

WESTSIDE SUBWAY EXTENSION PROJECT

Air Quality Memorandum

Metro

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1.0 INTRODUCTION

This memorandum supplements the *Westside Subway Extension Project Air Quality Technical Report (the Report)* dated August 2010 and supports the *Westside Subway Extension Final EIS/EIR*. This memorandum updates the analysis in the Environmental Impact/Environmental Consequences Section of the Report to incorporate modifications to the LPA (Alternative 2) since the release of the Draft EIS/EIR. The analysis has been revised to reflect modifications to the LPA operating plan and refinements to construction methods. The analysis was also revised to incorporate an assessment of existing conditions. Only the LPA (Alternative 2) is included in this memorandum.

The LPA could either be constructed as a single phase under the America Fast Forward (30/10) Scenario (Concurrent Construction), or as three consecutive phases under the Metro Long Range Transportation Plan (LRTP) Scenario (Phased Construction). The opening of the LPA as a single phase or in three sequential phases does not substantially change the air quality analysis that was presented in the Draft EIS/EIR.

Information on regulatory framework, analysis methodology and existing conditions/affected environment can be found in the *Westside Subway Extension Project Air Quality Technical Report*. The regulatory framework, analysis methodology and existing conditions/affected environment for the LPA are the same whether the LPA is constructed under the Concurrent Construction Scenario or the Phased Construction Scenario.

2.0 PROJECT DESCRIPTION

On October 28, 2010, the Metro Board selected the Westwood/VA Hospital Extension (Alternative 2 in the Draft EIS/EIR) as the Locally Preferred Alternative (LPA) and authorized the preparation of the *Westside Subway Extension Final EIS/EIR* (the Final EIS/EIR) to analyze the LPA. This alternative would extend HRT, in subway, approximately nine-miles from the existing Metro Purple Line Wilshire/Western Station to a Westwood/VA Hospital Station. The extension would include a total of seven new stations:

- Wilshire/La Brea
- Wilshire/Fairfax
- Wilshire/La Cienega
- Wilshire/Rodeo
- Century City (Century City Santa Monica or Century City Constellation)
- Westwood/UCLA (Westwood/UCLA On-Street or Westwood/UCLA Off-Street)
- Westwood/VA Hospital (Westwood/VA Hospital South or Westwood/VA Hospital North)

The estimated one-way running time for the project would be approximately 15 minutes from the Wilshire/Western Station to the Westwood/VA Hospital Station. The extension would operate at headways of 4 minutes during peak periods and 10 minutes during off-peak periods. As part of the project, Metro is also planning several enhancements to the Division 20 Maintenance and Storage Facility.

The construction schedule for the Project is partially dependent on the timing of Federal funding availability. Two LPA construction scenarios are considered. Both scenarios will contain the same elements with differences only in the timing of when they are built and operational. The first construction scenario assumes that under the America Fast Forward (30/10) Scenario (Concurrent Construction), the LPA would open in its entirety to the Westwood/VA Hospital Station in 2022 with the three construction segments built concurrently (Wilshire/Western to Wilshire/La Cienega, Wilshire/La Cienega to Century City and Century City to Westwood/VA Hospital). The second construction scenario assumes that under the Metro Long Range Transportation Plan (LRTP) Scenario (Phased Construction), the LPA would open in three consecutive phases (Phase 1 to Wilshire/La Cienega, Phase 2 to Century City, and Phase 3 to Westwood/VA Hospital), with the entire LPA operational to the Westwood/VA Hospital Station in 2036.

A detailed description of the LPA is provided in Chapter 2 of the Final EIS/EIR.

3.0 ENVIRONMENTAL IMPACT/ENVIRONMENTAL CONSEQUENCES

Pollutants that can be traced principally to motor vehicles are relevant to the evaluation of the project's impacts; these pollutants include CO, HC, NO_x, O_3, PM_{10}, $PM_{2.5}$, and MSAT. Transportation sources account for a small percentage of regional emissions of SO_x and Pb; thus, a detailed analysis is not required.

HC (VOC) and NO_x emissions from automotive sources are a concern primarily because they are precursors in the formation of ozone and particulate matter. Ozone is formed through a series of reactions that occur in the atmosphere in the presence of sunlight. Since the reactions are slow and occur as the pollutants are diffusing downwind, elevated ozone levels often are found many miles from the sources of the precursor pollutants. Therefore, the effects of HC and NO_x emissions generally are examined on a regional or "mesoscale" basis.

PM_{10} and $PM_{2.5}$ impacts are both regional and local. A significant portion of particulate matter, especially PM_{10}, comes from disturbed vacant land, construction activity, and paved road dust. $PM_{2.5}$ also comes from these sources. Motor vehicle exhaust, particularly from diesel vehicles, is also a source of PM_{10} and $PM_{2.5}$. PM_{10}, and especially $PM_{2.5}$, can also be created by secondary formation from precursor elements such as SO_2, NO_X, VOCs, and ammonia (NH_3). Secondary formation occurs due to chemical reaction in the atmosphere generally downwind some distance from the original emission source. Thus it is appropriate to predict concentrations of PM_{10} and $PM_{2.5}$ on both a regional and a localized basis.

CO impacts are generally localized. Even under the worst meteorological conditions and most congested traffic conditions, high concentrations are limited to a relatively short distance (300 to 600 feet) of heavily traveled roadways. Vehicle emissions are the major sources of CO. The Westside Subway Extension project could change traffic patterns within the project area. Consequently, it is appropriate to predict concentrations of CO on both a regional and a localized or "microscale" basis.

MSAT impacts are both regional and local. On February 3, 2006, the FHWA released "*Interim Guidance on Air Toxic Analysis in NEPA Documents."* This guidance was superseded on September 30, 2009 by FHWA's "*Interim Guidance Update on Air Toxic Analysis in NEPA Documents."* According to these documents, regardless of the alternative chosen, MSAT emissions will likely be lower than present levels in the design year as a result of EPA's national control programs that are projected to reduce annual MSAT emissions by 72 percent between 1999 and 2050. Local conditions may differ from these national projections in terms of fleet mix and turnover, vehicle miles traveled (VMT) growth rates, and local control measures. However, the magnitude of the EPA-projected reductions is so great (even after accounting for VMT growth) that MSAT emissions in the study area are likely to be lower in the future in nearly all cases.

3.1 Existing with Project

Per CEQA requirements, an EIR must include a description of the existing physical environmental conditions in the vicinity of the project. Those conditions, in turn, "will normally constitute the baseline physical conditions by which a lead agency determines whether an impact is significant." (CEQA Guidelines §15125[a])

For a project such as the Westside Subway project that would not commence operation for approximately 10 years and would not reach design year until 2035, use of only existing conditions as a baseline for energy impacts would be misleading. It is more likely that existing background traffic volumes (and background roadway changes from other programmed traffic improvement projects) and vehicle emission factors would change between today and 2035 than it is that existing conditions would remain unchanged over the next 25 years. For example, Regional Transportation Plans (RTP) include funded transportation projects that are programmed to be constructed by 2035. To ignore that these projects would be in place before the project reaches maturity (i.e., the point/year at which project-related traffic emissions reach their maximum) and to evaluate the project's impacts ignoring that these RTP improvements would change the underlying background conditions to which project traffic would be added, would be misleading because it would represent a hypothetical comparison.

Therefore, the analysis uses a dual baseline approach. That is, the project's impacts are evaluated both against existing conditions and against background (i.e., No Project) conditions as they are expected to be in 2035. This approach complies with CEQA. (See *Woodwark Park Homeowners Ass'n v. City of Fresno* (2007), 150 Cal.App.4th 683, 707 and *Sunnyvale West Neighborhood Assn. v. City of Sunnyvale* (2010), 190 Cal.App.4th 1351). Therefore, results for both baselines are presented.

3.2 Regional Emissions Analysis

The regional emission burden analysis of a project determines a project's overall impact on air quality levels. For this project, an analysis was conducted for the study area and for the entire region. The "region" is the 5 County Region which includes Los Angeles, Ventura, San Bernardino, Riverside and Orange Counties, and the "Study Area" is in western Los Angeles County and encompasses approximately 38 square miles. The Study Area, shown in Figure 3-1, is east-west oriented and includes portions of five jurisdictions: the cities of Los Angeles, West Hollywood, Beverly Hills, and Santa Monica, as well as portions of unincorporated Los Angeles County. The boundaries of the Study Area generally extend north to the base of the Santa Monica Mountains along Hollywood, Sunset and San Vicente Boulevards, east to the Metro Rail stations at Hollywood/Highland and Wilshire/Western, south to Pico Boulevard, and west to the Pacific Ocean.

The regional emissions analysis was conducted for Existing Conditions (2010), Existing with Project (2010), the No Build Alternative (2035), the Concurrent Construction Scenario (2035), and each phase of the Phased Construction Scenario (2035). The analysis was based on regional VMT estimates and vehicle hours traveled (VHT) estimates. Emission factors were obtained from CARB's emission factor program, EMFAC2007, the latest emission inventory model for the calculation of mobile source emission factors for vehicles operating on roads in California, using parameters set within the program for Los Angeles County. The results for the study area are shown in Table 3-1. The results for the region are shown in Table 3-2. As shown in the tables, in the existing year (2010), the Existing with Project scenario is predicted to have lower regional pollutant burden levels on both the regional and Study Area levels, as compared to Existing without the project. Similarly, in the design year (2035), all alternatives are predicted to have lower regional pollutant burden levels on both the regional and Study Area levels, as compared to the No Build Alternative. Project impacts are below the regional significance thresholds the SCAQMD developed.

Figure 3-1: Corridor Study Area



3.3 Local Impacts and Hot Spot Assessment

See Section 4.2 of the *Westside Subway Extension Project* Air Quality Technical Report.

3.3.1 Carbon Monoxide

See Section 4.2.1 of the *Westside Subway Extension Project* Air Quality Technical Report.

3.3.2 Analysis Results

Maximum one-hour and eight-hour CO levels were predicted at receptor sites along the proposed project. Maximum one-hour CO concentrations are shown in Table 3-3. Maximum eight-hour CO concentrations are shown in Table 3-4.

As shown in these tables, predicted CO concentrations in 2010 for Existing with Project conditions would be the same or slightly higher than those for Existing conditions without the project. Predicted CO concentrations in 2035 for the Concurrent Construction Scenario and all phases of the Phased Construction Scenario would be the same or slightly lower than those for the No Build Alternative. Predicted CO concentrations for the Concurrent Construction Scenario, all phases of the Phased Construction Scenario, and the No Build Alternative in 2035 are lower than Existing (with and without project) conditions in 2010.

No violations of the National Ambient Air Quality Standards are predicted under existing conditions (with and without the project), the No Build Alternative, the Concurrent Construction Scenario, or any phases of the Phased Construction Scenario.

Table 3-1: Study Area Emission Burden Assessment

Alternative	VMT		CO			TOG			NOx			PM10			PM2.5		
	Daily Vehicle Miles Traveled (millions)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build
Existing	4,348	—	16,746	—	—	1,117	—	—	4,242	—	—	297	—	—	220	—	—
Existing w/LPA	4,311	-0.9%	16,482	-265	-1.6%	1,093	-24	-2.2%	4,191	-51	-1.2%	292	-5	-1.7%	216	-4	-2.0%
No Build	5,185	—	5,405	—	—	348	—	—	1,198	—	—	292	—	—	206	—	—
Concurrent Construction Scenario																	
LPA with Century City Santa Monica	5,156	-0.6%	5,370	-35	-0.7%	345	-3	-0.7%	1,190	-8	-0.7%	291	-2	-0.7%	204	-2	-0.7%
LPA with Century City Constellation	5,152	-0.6%	5,365	-40	-0.7%	345	-3	-0.8%	1,189	-9	-0.7%	290	-2	-0.8%	204	-2	-0.8%
Phased Construction Scenario																	
Phase 1	5,178	-0.1%	5,393	-12	-0.2%	347	-1	-0.3%	1,195	-3	-0.2%	292	-1	-0.2%	205	-1	-0.3%
Phase 2 with Century City Santa Monica	5,172	-0.3%	5,387	-18	-0.3%	346	-1	-0.4%	1,194	-4	-0.3%	291	-1	-0.3%	205	-1	-0.4%
Phase 2 with Century City Constellation	5,166	-0.4%	5,380	-25	-0.5%	346	-2	-0.5%	1,192	-6	-0.5%	291	-1	-0.5%	205	-1	-0.5%
Phase 3 with Century City Santa Monica	5,156	-0.6%	5,370	-35	-0.7%	345	-3	-0.7%	1,190	-8	-0.7%	291	-2	-0.7%	204	-2	-0.7%
Phase 3 with Century City Constellation	5,152	-0.6%	5,365	-40	-0.7%	345	-3	-0.8%	1,189	-9	-0.7%	290	-2	-0.8%	204	-1	-0.8%

Alternative	VMT		CO			TOG			NOx			PM10			PM2.5		
	Daily Vehicle Miles Traveled (millions)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build
SCAQMD Significance Threshold			249 (550 lbs/day)			24.9 (55 lbs/day)			24.9 (55 lbs/day)			68 (150 lbs/day)			24.9 (55 lbs/day)		

Table 3-2: Regional Emission Burden Assessment

Alternative	VMT		CO			TOG			NOx			PM10			PM2.5		
	Daily Vehicle Miles Traveled (millions)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build
Existing	354.995	—	1,156,990	—	—	67,484	—	—	325,086	—	—	20,273	—	—	14,310	—	—
Existing w/LPA	354.719	-0.08%	1,156,010	-979	-0.1%	67,423	-60	-0.1%	324,830	-256	-0.1%	20,256	-17	-0.1%	14,298	-12	-0.1%
No Build	532.661	—	604,617	—	—	47,630	—	—	138,175	—	—	34,745	—	—	25,524	—	—
Concurrent Construction Scenario																	
LPA with Century City Santa Monica	532.343	-0.11%	602,210	-2,407	-0.4%	46,973	-657.2	-1.4%	137,463	-712	-0.5%	34,515	-231	-0.7%	25,299	-225	-0.9%
LPA with Century City Constellation	532.080	-0.11%	601,907	-2,710	-0.4%	46,949	-681.0	-1.4%	137,394	-782	-0.6%	34,497	-248	-0.7%	25,286	-238	-0.9%
Phased Construction Scenario																	
Phase 1	532.447	-0.04%	604,365	-251	0.0%	47,609	-21.3	0.0%	138,117	-58	0.0%	34,730	-15	0.0%	25,513	-11	0.0%
Phase 2 with Century City Santa Monica	532.514	-0.03%	604,453	-163	0.0%	47,618	-12.2	0.0%	138,138	-37	0.0%	34,736	-9	0.0%	25,517	-7	0.0%
Phase 2 with Century City Constellation	532.267	-0.07%	604,157	-459	-0.1%	47,592	-38.2	-0.1%	138,069	-106	-0.1%	34,718	-27	-0.1%	25,504	-20	-0.1%

Alternative	VMT		CO			TOG			NOx			PM10			PM2.5		
	Daily Vehicle Miles Traveled (millions)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build	Emission Burden (Kg/day)	Change from Existing/No Build (Kg/day)	Percent change from Existing/No Build
Phase 3 with Century City Santa Monica	532.343	-0.11%	602,210	-2,407	-0.4%	46,973	-657.2	-1.4%	137,463	-712	-0.5%	34,515	-231	-0.7%	25,299	-225	-0.9%
Phase 3 with Century City Constellation	532.080	-0.11%	601,907	-2,710	-0.4%	46,949	-681.3	-1.4%	137,394	-782	-0.6%	34,497	-248	-0.7%	25,286	-238	-0.9%
SCAQMD Significance Threshold			249 (550 lbs/day)			24.9 (55 lbs/day)			24.9 (55 lbs/day)			68 (150 lbs/day)			24.9 (55 lbs/day)		

Table 3-3: Predicted One-hour CO Concentrations (ppm)

No.	Site Description	Existing (2010)		Existing w/ Project (2010)		No Build (2035)		LPA (2035)		Phase 1		Phase 2		Phase 3	
		AM	PM	AM	PM	AM	PM	AM	PM	AM	PM	AM	PM	AM	PM
1	26th Street & Wilshire Boulevard	3.60	3.60	3.60	3.60	3.00	3.00	2.80	2.80	2.90	3.00	2.80	2.80	2.80	2.80
2	Veteran Avenue & Wilshire Boulevard	3.90	3.80	3.90	3.90	3.20	3.10	3.10	3.10	3.10	3.10	2.80	2.80	3.10	3.10
3	Glendon Avenue & Wilshire Boulevard	3.70	3.70	3.70	3.80	3.10	3.10	3.10	3.10	3.10	3.00	2.80	2.80	3.10	3.10
4	La Cienega Boulevard & Beverly Boulevard	3.60	3.70	3.70	3.70	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
5	La Brea Avenue and Olympic Boulevard	4.00	4.00	4.00	4.00	3.10	3.10	3.10	3.10	3.10	3.00	3.10	3.10	3.10	3.10

Concentrations include one-hour CO background = 2.8 ppm
One-hour NAAQS = 35 ppm
SAAQS = 20 ppm

Table 3-4: Predicted Eight-hour CO Concentrations (ppm)

No.	Site Description	Existing (2010)	Existing w/ Project (2010)	No Build (2035)	LPA (2035)	Phase 1	Phase 2	Phase 3
1	26th Street & Wilshire Boulevard	2.46	2.46	2.04	1.90	2.04	1.90	1.90
2	Veteran Avenue & Wilshire Boulevard	2.67	2.67	2.18	2.11	2.11	1.90	2.11
3	Glendon Avenue & Wilshire Boulevard	2.53	2.60	2.11	2.11	2.11	1.90	2.11
4	La Cienega Boulevard & Beverly Boulevard	2.53	2.53	2.04	2.04	2.04	2.04	2.04
5	La Brea Avenue and Olympic Boulevard	2.74	2.74	2.11	2.11	2.11	2.11	2.11

Concentrations include eight-hour CO background = 1.9 ppm
Eight-hour NAAQS = 9 ppm
SAAQS = 9.0 ppm

3.3.3 Particulate Matter (PM10 and PM2.5)

Because the project area is classified as a nonattainment area for PM_{10} and $PM_{2.5}$, a PM_{10} and $PM_{2.5}$ qualitative hotspot analysis following EPA's March 29, 2006 guidance "*Transportation Conformity Guidance for Qualitative Hot-spot Analyses in $PM_{2.5}$ and PM_{10} Nonattainment and Maintenance Areas* (EPA420-B-06-902) has been conducted, as recommended in EPA's Final Rule regarding the localized or "hot-spot" analysis of $PM_{2.5}$ and PM_{10} (40 CFR Part 93 – issued on March 10, 2006).

The proposed project will be electrically powered. Although the project does not specify additional bus service, any new buses servicing the project's stations will be powered by compressed natural gas. As such, the project is not anticipated to increase diesel traffic within the study area and is considered a project not of air quality concern. An interagency consultation, following SCAG procedures, is being scheduled to confirm this finding.

3.3.4 Mobile Source Air Toxics

See Section 4.2.4 of the *Westside Subway Extension Project* Air Quality Technical Report. The mobile source air toxics analysis is the same whether the LPA is constructed under the Concurrent Construction Scenario or the Phased Construction Scenario.

3.3.5 Odors

The project's operations are not expected to cause any objectionable odors, as the rail system's operations will operate on electric power and will not produce emissions. However, construction of the LPA under either the Concurrent Construction Scenario or the Phased Construction Scenario will generate emissions and objectionable odors, which could be significant but will be limited to the duration of construction.

3.4 Construction Assessments

An assessment of the air quality construction impacts was conducted. The assessment utilized CARB's Urban Emissions Model (URBEMIS), the Road Construction Emissions Model, Version 6.3.2 (RCEM) developed by the Sacramento Metropolitan Air Quality Management District (SMAQMD), and the SCAQMD OFFROAD 2007 emission factors. The RCEM model estimates emissions of fugitive dust PM_{10} based on a screening emission factor of 20 pounds per day per acre of unpaved activity, and applies an estimated 50% fugitive dust reduction if the user indicates that water trucks will be used for dust control. SCAQMD OFFROAD2007 was used to develop emission factors from off-road construction equipment. Worker and delivery trip emissions factors were estimated using the EMFAC2007 emission factor model. Using these various data sources, daily construction emission levels were developed. These values were compared to the air quality construction significance thresholds shown in Table 3-5 to determine if the project would meet or exceed these values. As the construction schedule is very preliminary at this time, construction emissions were estimated for each major activity.

America Fast Forward (30/10) Scenario (Concurrent Construction)

As shown in Table 3-6, for a typical station with a TBM entry/exit site, SCAQMD thresholds would be exceeded for VOCs, NOx and PM_{10}. For a typical station without a TBM entry/exit site, SCAQMD thresholds would be exceeded for NOx. For a maintenance facility, SCAQMD thresholds would be exceeded for NOx. For the entire project, the SCAQMD thresholds would be exceeded for all pollutants.

Metro Long Range Transportation Plan (LRTP) Scenario (Phased Construction)

As shown in Table 3-6, for a typical station with a TBM entry/exit site, SCAQMD thresholds would be exceeded for VOCs, NOx and PM_{10}. For a typical station without a TBM entry/exit site, SCAQMD thresholds would be exceeded for NOx. For a maintenance facility, SCAQMD thresholds would be exceeded for NOx. For Phase 1, the SCAQMD thresholds would be exceeded for all pollutants except for CO. For Phases 2 and 3, the SCAQMD thresholds would be exceeded for all pollutants.

Mitigation measures such as watering, the use of soil stabilizers, etc. will be applied to reduce the predicted PM_{10} levels to below the SCAQMD daily construction threshold levels. NOx levels would be elevated due partially to the proposed use of diesel locomotives to extract soil during the tunnel boring process. Mitigation measures could help to reduce these impacts, but it is unlikely, given the

current construction plan, that these levels would be below the SCAQMD threshold. Specific mitigation measures include:

All station exposed excavation and surface soil will be watered a certain amount of times a day/week.

- All station construction and cut and cover construction sites neighborhoods will have streets washed by watering trucks a certain amount of times a day/week.
- All tunnel locomotives will be powered by propane, not diesel.
- All electricity will be secured from the grid; generators will not be used
- The use of fugitive dust source controls is recommended. These controls include, but are not limited to:
  - Installing wind fencing and phase grading operations where appropriate
  - Operating water trucks for stabilization of surfaces under windy conditions
  - Prevent spillage and limit speed to 15 miles per hour when hauling material and operating non-earthmoving equipment.
  - Limit speed of earth-moving equipment to 10 miles per hour.
- Inventory all equipment before groundbreaking and determine suitability of mitigation measures on each piece of equipment.
- Identify when the use of mitigation measures is rejected due to economic feasibility,
- Insure that EPA diesel fuel requirements are met.
- Locating construction equipment and staging areas away from sensitive receptors and fresh air intake to buildings and air conditions.

Once a detailed construction schedule is developed, a more refined construction analysis will be conducted to determine the air quality impacts of construction.

3.5 Conformity Assessment

See Section 4. 4 of the *Westside Subway Extension Project* Air Quality Technical Report.

3.6 Cumulative Impacts

See Section 4.5 of the *Westside Subway Extension Project* Air Quality Technical Report.

Table 3-5: SCAQMD Air Quality Significance Thresholds

Mass Daily Thresholds[1]		
Pollutant	**Construction[2]**	**Operation[3]**
Nitrogen Oxides (NOx)	100 lbs/day	55 lbs/day
Volatile Organic Compounds (VOC)	75 lbs/day	55 lbs/day
Respirable Particulate Matter (PM10)	150 lbs/day	150 lbs/day
Fine Particulate Matter (PM2.5)	55 lbs/day	55 lbs/day
Sulfur Oxides (SOx)	150 lbs/day	150 lbs/day
Carbon Monoxide (CO)	550 lbs/day	550 lbs/day
Lead (Pb)	3 lbs/day	3 lbs/day
Carbon Dioxide equivalents (CO25)	Being developed at this time	Being developed at this time
Toxic Air Contaminants (TACs) and Odor Thresholds		
TACs (including carcinogens and non-carcinogens)	Maximum Incremental Cancer Risk ≥ 10 in 1 million Cancer Burden > 0.5 excess cancer cases (in areas ≥ 1 in 1 million) Hazard Index ≥ 1.0 (project increment)	
Odor	Project creates an odor nuisance pursuant to SCAQMD Rule 402	
Ambient Air Quality for Criteria Pollutants4		
NO2 1-hour average annual average	SCAQMD is in attainment; project is significant if it causes or contributes to an exceedance of the following attainment standards: 0.18 ppm (state) 0.03 ppm (state)	
PM10 24-hour average annual average	10.4 µg/m3 (construction)5 & 2.5 µg/m3 (operation) 1.0 µg/m3	
PM2.5 24-hour average	10.4 µg/m3 (construction)5 & 2.5 µg/m3 (operation)	
Sulfate 24-hour average	1 µg/m3	
CO 1-hour average 8-hour average	SCAQMD is in attainment; project is significant if it causes or contributes to an exceedance of the following attainment standards: 20 ppm (state) 9.0 ppm (state/federal)	

1Source: SCAQMD CEQA Handbook (SCAQMD, Rev. March 2009).
[2]Construction thresholds apply to both the South Coast Air Basin and Coachella Valley (Salton Sea and Mojave Desert Air Basins).
[3]For Coachella Valley, the mass daily thresholds for operation are the same as the construction thresholds.
[4]Ambient air quality thresholds for criteria pollutants based on SCAQMD Rule 1303, Table A-2 unless otherwise stated.
[5]Ambient air quality threshold based on SCAQMD Rule 403.
KEY:
lbs/day = pounds per day
ppm = parts per million
µg/m3 = microgram per cubic meter
≥ = greater than or equal to

Table 3-6: Estimated Construction Impacts for Concurrent Construction Scenario Project Design Elements (lbs/day)

Activity	VOC	CO	NOx	PM_{10}	$PM_{2.5}$
Typical Station with a TBM entry/exit site, such as La Brea Station					
Construction Equipment	74	164	406	18	18
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				138	29
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	5	48	50	3	3
Total	**77**	**194**	**436**	**195**	42
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Typical Station without a TBM entry/exit site, such as Fairfax Station					
Construction Equipment	28	102	137	7	7
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				64	
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	3	36	29	2	2
Total	31	135	162	72	22
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Maintenance Facility					
Construction Equipment	26	98	221	9	8
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				53	11
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	1	31	4	1	1
Total	27	129	225	63	20
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Concurrent Construction Scenario					
Total	236	1054	1679	709	203
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**

Note: Total construction emissions may not occur during the same peak period as each emission source, therefore the total construction emissions shown may not add up to the sum of the elements presented in this table.

Table 3-7: Estimated Construction Impacts for Phased Construction Scenario Project Design Elements (lbs/day)

Activity	VOC	CO	NOx	PM_{10}	$PM_{2.5}$
Typical Station with a TBM entry/exit site, such as Wilshire/La Brea Station					
Construction Equipment	74	164	406	18	18
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				138	29
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	5	48	50	3	3
Total	**77**	**194**	**436**	**195**	**42**
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Typical Station without a TBM entry/exit site, such as Wilshire/Fairfax Station					
Construction Equipment	28	102	137	7	7
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				64	
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	3	36	29	2	2
Total	**31**	**135**	**162**	**72**	**22**
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Maintenance Facility					
Construction Equipment	26	98	221	9	8
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				53	11
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	1	31	4	1	1
Total	**27**	**129**	**225**	**63**	**20**
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Phase 1					
Total	**134**	**544**	**809**	**198**	**94**
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Phase 2					
Total	**134**	**564**	**809**	**442**	**103**
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Phase 3					
Total	**134**	**564**	**809**	**442**	**103**
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**

Note: Total construction emissions may not occur during the same peak period as each emission source, therefore the total construction emissions shown may not add up to the sum of the elements presented in this table.

APPENDIX A
CAL3QHC Files Used for the Microscale Modeling

Site 1 – 26th & Wilshire
Input Files

```
Site 1 26th & Wilshire (S1EXAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Existing AM                      24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1111 3.3  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1071 3.3  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        58       2.0 1071   20.5 1287 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 3.3  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   40   20.5  180 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1198 3.3  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1302 3.3  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1181 3.3  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1181   20.5 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 3.3  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        50       2.0  121   20.5  168 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1248 3.3  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     723 3.3  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     591 3.3  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  591   20.5 1242 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     132 3.3  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  132   20.5  336 1 3
  1
SB        26 LT     AG   672.   845.  1384.   114.     688 3.3  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     563 3.3  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     485 3.3  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  485   20.5 1245 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 3.3  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        53       2.0   78   20.5  252 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     565 3.3  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1EXPM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Existing PM                      24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1229 3.3  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1142 3.3  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.       0.  24   2
        90        59       2.0 1142   20.5 1285 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 3.3  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.       0.  12   1
        90        54       2.0   87   20.5  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1326 3.3  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1384 3.3  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1181 3.3  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.       0.  36   3
        90        57       2.0 1181   20.5 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 3.3  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.       0.  12   1
```

```
        90        52       2.0  127   20.5  176 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1479 3.3  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     694 3.3  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     555 3.3  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  555   20.5 1236 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     139 3.3  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  139   20.5  252 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     656 3.3  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     727 3.3  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     616 3.3  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  616   20.5 1239 1 3
  1
NB        26 L      AG   818.   710.   705.   832.     111 3.3  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0  111   20.5  358 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     700 3.3  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1NBAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 No Build AM                      24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1288 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1248 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        59       2.0 1248   4.1 1290 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   40   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1363 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1617 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1496 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1496   4.1 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        51       2.0  121   4.1  170 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1515 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     817 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     715 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  715   4.1 1242 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     102 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        49       2.0  102   4.1  166 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     812 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     707 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     629 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        56       2.0  629   4.1 1245 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0   78   4.1  172 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     739 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1NBPM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 No Build PM                      24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1495 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1408 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        57       2.0 1408   4.1 1289 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   87   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1726 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1697 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1570 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1570   4.1 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        51       2.0  127   4.1  169 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1707 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     830 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     661 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        57       2.0  661   4.1 1236 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     169 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        51       2.0  169   4.1  174 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     762 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     921 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     810 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  810   4.1 1239 1 3
  1
NB        26 L      AG   818.   710.   705.   832.     111 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0  111   4.1  177 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     748 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B3AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt3 AM                   24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1275 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1235 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        59       2.0 1235   4.1 1288 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   40   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1352 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1613 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1492 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1492   4.1 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        51       2.0  121   4.1  170 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1491 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     822 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     714 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  714   4.1 1208 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     108 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  108   4.1  198 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     808 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     669 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     591 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  591   4.1 1210 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0   78   4.1  172 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     725 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B3PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt3 PM                    24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1509 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1422 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.       0.  24   2
        90        57       2.0 1422   4.1 1287 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.       0.  12   1
        90        53       2.0   87   4.1  175 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1766 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1713 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1586 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.       0.  36   3
        90        56       2.0 1586   4.1 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.       0.  12   1
```

```
        90        51       2.0  127   4.1  169 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1728 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     852 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     680 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        57       2.0  680   4.1 1200 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     169 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        52       2.0  169   4.1  174 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     765 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     974 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     863 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        58       2.0  863   4.1 1204 1 3
  1
NB        26 L      AG   818.   710.   705.   832.     111 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0  111   4.1  177 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     793 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B5AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt5 AM                   24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1254 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1214 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.       0.  24   2
        90        59       2.0 1214   4.1 1289 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.       0.  12   1
        90        55       2.0   40   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1331 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1560 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1439 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.       0.  36   3
        90        56       2.0 1439   4.1 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.       0.  12   1
```

```
        90        50       2.0  121   4.1  170 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1550 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     823 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     715 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  715   4.1 1196 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     108 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  108   4.1  198 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     812 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     669 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     591 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  591   4.1 1199 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0   78   4.1  172 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     707 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B5PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt5 PM                   24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1492 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1405 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        57       2.0 1405   4.1 1289 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        53       2.0   87   4.1  171 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1722 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1720 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1593 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        55       2.0 1593   4.1 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        50       2.0  127   4.1  164 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1718 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     846 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     677 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        57       2.0  677   4.1 1190 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     169 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        52       2.0  169   4.1  175 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     778 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     930 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     834 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        58       2.0  834   4.1 1193 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      96 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        54       2.0   96   4.1  180 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     770 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

Site 1 – 26th & Wilshire
Output Files

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 1 26th & Wilshire (S1EXAM.DAT) RUN: Site 1 Existing AM
DATE: 03/19/2010 TIME: 08:31:52.74

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	*	-15.0	139.0	583.0	699.0	*	819.	47.	AG	1111.	3.3	.0	44.0		
2.	EB Wil T+R	*	584.0	699.0	715.0	824.0	*	181.	46.	AG	1071.	3.3	.0	44.0		
3.	EB Wil T+R Q	*	672.0	783.0	-500.4	-348.0	*	1629.	226.	AG	71.	100.0	.0	24.0	1.34	82.8
4.	EB Wil LT	*	569.0	717.0	698.0	843.0	*	180.	46.	AG	40.	3.3	.0	32.0		
5.	EB Wil LT Q	*	654.0	800.0	643.5	789.8	*	15.	226.	AG	34.	100.0	.0	12.0	.65	.7
6.	EB Wil DP	*	715.0	824.0	1421.0	1528.0	*	997.	45.	AG	1198.	3.3	.0	44.0		
7.	WB Wil AP	*	1393.0	1557.0	810.0	982.0	*	819.	225.	AG	1302.	3.3	.0	44.0		
8.	WB Wil T+R	*	806.0	986.0	684.0	868.0	*	170.	226.	AG	1181.	3.3	.0	56.0		
9.	WB Wil T+R Q	*	717.0	900.0	868.0	1047.5	*	211.	46.	AG	103.	100.0	.0	36.0	.99	10.7
10.	WB Wil LT	*	824.0	966.0	707.0	850.0	*	165.	225.	AG	121.	3.3	.0	32.0		
11.	WB Wil LT Q	*	737.0	880.0	1187.5	1330.5	*	637.	45.	AG	31.	100.0	.0	12.0	1.81	32.4
12.	WB Wil DP	*	687.0	864.0	-35.0	163.0	*	1006.	226.	AG	1248.	3.3	.0	44.0		
13.	SB 26 AP	*	553.0	971.0	-6.0	1547.0	*	803.	316.	AG	723.	3.3	.0	32.0		
14.	SB 26 T+R	*	549.0	968.0	670.0	841.0	*	175.	136.	AG	591.	3.3	.0	44.0		
15.	SB 26 T+R Q	*	633.0	880.0	570.0	946.1	*	91.	316.	AG	68.	100.0	.0	24.0	.71	4.6
16.	SB 26 LT	*	563.0	978.0	679.0	856.0	*	168.	136.	AG	132.	3.3	.0	32.0		
17.	SB 26 LT Q	*	645.0	891.0	585.1	954.6	*	87.	317.	AG	31.	100.0	.0	12.0	.99	4.4
18.	SB 26 LT	*	672.0	845.0	1384.0	114.0	*	1020.	136.	AG	688.	3.3	.0	32.0		
19.	NB 26 AP	*	829.0	716.0	1410.0	138.0	*	820.	135.	AG	563.	3.3	.0	32.0		
20.	NB 26 T+R	*	832.0	719.0	715.0	846.0	*	173.	317.	AG	485.	3.3	.0	44.0		
21.	NB 26 T+R Q	*	759.0	798.0	810.1	742.5	*	75.	137.	AG	70.	100.0	.0	24.0	.60	3.8
22.	NB 26 L	*	818.0	710.0	705.0	832.0	*	166.	317.	AG	78.	3.3	.0	32.0		
23.	NB 26 L Q	*	747.0	787.0	773.7	758.0	*	39.	137.	AG	32.	100.0	.0	12.0	.85	2.0
24.	NB 26 DP	*	712.0	843.0	13.0	1565.0	*	1005.	316.	AG	565.	3.3	.0	32.0		

1 PAGE 2

JOB: Site 1 26th & Wilshire (S1EXAM.DAT) RUN: Site 1 Existing AM
DATE: 03/19/2010 TIME: 08:31:52.74

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Wil T+R Q	*	90	58	2.0	1071	1287	20.50	1	3
5.	EB Wil LT Q	*	90	55	2.0	40	180	20.50	1	3
9.	WB Wil T+R Q	*	90	56	2.0	1181	1190	20.50	1	3
11.	WB Wil LT Q	*	90	50	2.0	121	168	20.50	1	3
15.	SB 26 T+R Q	*	90	56	2.0	591	1242	20.50	1	3
17.	SB 26 LT Q	*	90	50	2.0	132	336	20.50	1	3
21.	NB 26 T+R Q	*	90	57	2.0	485	1245	20.50	1	3
23.	NB 26 L Q	*	90	53	2.0	78	252	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	967.0	615.0	5.0	*
2.	SE 164 S	*	874.0	710.0	5.0	*
3.	SE 82 S	*	816.0	771.0	5.0	*
4.	SE CNR	*	768.0	826.0	5.0	*
5.	SE 82 E	*	819.0	886.0	5.0	*
6.	SE 164 E	*	877.0	944.0	5.0	*
7.	SE MID E	*	996.0	1059.0	5.0	*
8.	NE MID E	*	916.0	1134.0	5.0	*
9.	NE 164 E	*	800.0	1020.0	5.0	*
10.	NE 82 E	*	741.0	962.0	5.0	*
11.	NE CNR	*	680.0	915.0	5.0	*
12.	NE 82 N	*	628.0	964.0	5.0	*
13.	NE 164 N	*	570.0	1023.0	5.0	*
14.	NE MID N	*	454.0	1143.0	5.0	*
15.	NW MID N	*	391.0	1100.0	5.0	*
16.	NW 164 N	*	514.0	974.0	5.0	*
17.	NW 82 N	*	571.0	914.0	5.0	*
18.	NW CNR	*	621.0	855.0	5.0	*
19.	NW 82 W	*	570.0	797.0	5.0	*
20.	NW 164 W	*	512.0	740.0	5.0	*
21.	NW MID W	*	412.0	643.0	5.0	*
22.	SW MID W	*	484.0	558.0	5.0	*
23.	SW 164 W	*	589.0	658.0	5.0	*
24.	SW 82 W	*	649.0	715.0	5.0	*
25.	SW CNR	*	707.0	765.0	5.0	*
26.	SW 82 S	*	763.0	714.0	5.0	*
27.	SW 164 S	*	820.0	656.0	5.0	*
28.	SW MID S	*	919.0	554.0	5.0	*

1 PAGE 3

JOB: Site 1 26th & Wilshire (S1EXAM.DAT) RUN: Site 1 Existing AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.2	.4	.2	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
5.	.0	.0	.2	.4	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.0
10.	.0	.0	.2	.2	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
15.	.0	.0	.1	.2	.5	.3	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
20.	.0	.0	.1	.3	.5	.4	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
25.	.0	.0	.1	.4	.5	.4	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
30.	.0	.0	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.0	.0
35.	.0	.0	.1	.2	.3	.3	.3	.1	.1	.2	.1	.0	.0	.0	.1	.1	.3	.3	.0	.0
40.	.0	.0	.0	.2	.3	.3	.2	.1	.1	.3	.1	.0	.0	.0	.1	.1	.3	.2	.1	.0
45.	.0	.0	.0	.1	.1	.1	.1	.1	.2	.4	.3	.0	.0	.0	.1	.1	.3	.3	.1	.2
50.	.0	.0	.0	.1	.1	.1	.1	.1	.3	.5	.5	.0	.0	.0	.1	.1	.3	.5	.3	.2
55.	.0	.0	.0	.1	.1	.1	.1	.3	.5	.6	.5	.0	.0	.0	.1	.1	.3	.5	.3	.3
60.	.0	.0	.0	.0	.0	.0	.0	.3	.5	.6	.6	.1	.0	.0	.1	.1	.4	.4	.3	.2
65.	.0	.0	.0	.0	.0	.0	.0	.3	.5	.8	.6	.2	.0	.0	.1	.1	.4	.4	.3	.1
70.	.0	.0	.0	.0	.0	.0	.0	.3	.7	.8	.5	.2	.0	.0	.1	.1	.4	.4	.2	.1
75.	.0	.0	.0	.0	.0	.0	.0	.3	.6	.7	.5	.1	.0	.0	.1	.1	.4	.5	.1	.3
80.	.0	.0	.0	.0	.0	.0	.0	.3	.6	.7	.5	.1	.0	.0	.1	.2	.4	.5	.1	.3
85.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.6	.5	.1	.0	.0	.1	.2	.4	.3	.1	.3
90.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.1	.1	.0	.1	.1	.4	.3	.1	.3
95.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.1	.1	.0	.1	.1	.4	.2	.2	.3
100.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.1	.1	.3	.2	.3	.2
105.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.1	.2	.3	.1	.3	.2
110.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.3	.2	.3	.2
115.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.3	.2	.3	.2
120.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.3	.2	.3	.2
125.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.2	.2	.3	.2
130.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.2	.1	.0	.0	.1	.2	.2	.2	.3	.2
135.	.1	.1	.0	.1	.0	.0	.0	.2	.5	.5	.2	.0	.0	.1	.0	.2	.2	.3	.3	.2
140.	.1	.1	.1	.1	.0	.0	.0	.2	.5	.5	.2	.0	.1	.1	.0	.1	.1	.2	.3	.3
145.	.1	.2	.2	.2	.0	.0	.0	.2	.5	.5	.2	.1	.1	.1	.0	.0	.1	.2	.3	.3
150.	.2	.2	.2	.3	.0	.0	.0	.2	.5	.5	.2	.1	.2	.1	.0	.0	.1	.3	.3	.3
155.	.2	.2	.1	.3	.0	.0	.0	.2	.5	.5	.2	.1	.2	.1	.0	.0	.0	.3	.2	.3
160.	.2	.2	.1	.4	.0	.0	.0	.2	.5	.5	.2	.1	.2	.1	.0	.0	.2	.3	.2	.3
165.	.2	.2	.1	.4	.0	.0	.0	.2	.6	.5	.2	.1	.2	.2	.0	.0	.2	.3	.2	.3
170.	.2	.2	.1	.4	.0	.0	.0	.2	.6	.5	.2	.2	.2	.2	.0	.0	.2	.3	.2	.3
175.	.2	.2	.3	.3	.0	.0	.0	.2	.5	.5	.3	.3	.2	.2	.0	.0	.2	.2	.2	.3
180.	.1	.2	.2	.3	.0	.0	.0	.2	.5	.5	.3	.4	.2	.2	.0	.0	.2	.2	.2	.3
185.	.1	.1	.2	.2	.0	.0	.0	.2	.6	.4	.5	.4	.2	.2	.0	.1	.2	.2	.2	.3
190.	.1	.1	.2	.2	.1	.0	.0	.2	.6	.4	.3	.4	.2	.1	.0	.1	.2	.2	.3	.3
195.	.1	.1	.2	.2	.1	.0	.0	.3	.6	.4	.3	.4	.2	.1	.0	.1	.2	.2	.4	.4
200.	.1	.1	.2	.2	.1	.0	.0	.3	.5	.5	.3	.4	.2	.1	.0	.1	.2	.2	.4	.4
205.	.1	.1	.1	.1	.1	.0	.0	.3	.4	.5	.3	.4	.2	.1	.0	.1	.2	.3	.4	.4

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.2	.1	.0	.0	.0	.3	.5	.5	.3	.4	.2	.1	.0	.0	.2	.3	.4	.4
215.	.1	.1	.3	.1	.1	.0	.0	.4	.6	.5	.3	.4	.1	.1	.0	.0	.2	.3	.4	.4
220.	.1	.1	.3	.2	.1	.2	.1	.3	.5	.4	.3	.3	.1	.1	.0	.0	.1	.2	.4	.4
225.	.1	.1	.4	.2	.2	.2	.2	.3	.5	.4	.3	.2	.1	.1	.0	.0	.0	.2	.2	.2
230.	.1	.1	.4	.5	.3	.3	.3	.1	.4	.3	.3	.2	.1	.1	.0	.0	.0	.2	.2	.2
235.	.1	.2	.4	.5	.3	.3	.2	.1	.2	.2	.3	.2	.1	.1	.0	.0	.0	.1	.1	.1
240.	.1	.2	.4	.3	.3	.3	.3	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
245.	.1	.1	.4	.3	.3	.3	.3	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
250.	.1	.1	.4	.3	.2	.4	.4	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
255.	.1	.1	.4	.3	.2	.4	.3	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
260.	.1	.1	.4	.3	.1	.3	.3	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0
265.	.1	.1	.4	.4	.1	.3	.3	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
270.	.1	.1	.4	.3	.3	.3	.3	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
275.	.2	.1	.3	.2	.3	.4	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
280.	.2	.1	.3	.2	.3	.4	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
285.	.2	.1	.3	.1	.3	.4	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
290.	.2	.1	.3	.1	.3	.3	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
295.	.2	.1	.2	.1	.3	.3	.2	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0
300.	.1	.1	.2	.2	.3	.3	.2	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0
305.	.1	.1	.2	.2	.3	.3	.2	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0
310.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.1	.2	.2	.1	.0	.1	.0	.0	.0	.0
315.	.0	.1	.0	.3	.4	.4	.2	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.0	.0
320.	.0	.0	.0	.3	.4	.4	.2	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.2	.0	.0
325.	.0	.0	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0
330.	.0	.1	.2	.3	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0
335.	.0	.1	.2	.3	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.3	.0	.0
340.	.0	.1	.2	.3	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
345.	.0	.1	.2	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
350.	.0	.1	.2	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
355.	.0	.0	.2	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
360.	.0	.0	.2	.4	.2	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
MAX DEGR.	.2 150	.2 145	.4 225	.5 230	.5 15	.4 20	.4 250	.4 215	.7 70	.8 65	.6 60	.4 180	.2 150	.2 165	.1 0	.2 80	.4 60	.5 50	.4 195	.4 195

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.4	.4	.4	.3	.4	.2	.1
5. *	.0	.4	.4	.3	.5	.4	.1	.1
10. *	.0	.4	.4	.2	.5	.4	.1	.1
15. *	.0	.4	.4	.3	.5	.4	.1	.1
20. *	.0	.4	.4	.3	.3	.4	.1	.1
25. *	.0	.4	.3	.4	.3	.3	.1	.1
30. *	.0	.4	.3	.4	.3	.3	.1	.1
35. *	.0	.3	.4	.3	.4	.3	.1	.1
40. *	.1	.3	.3	.3	.2	.2	.1	.1
45. *	.1	.2	.3	.1	.2	.2	.1	.1
50. *	.1	.1	.0	.1	.2	.2	.1	.1
55. *	.1	.1	.0	.0	.2	.2	.1	.1
60. *	.3	.0	.0	.0	.2	.2	.1	.1
65. *	.3	.0	.0	.0	.2	.1	.1	.1
70. *	.3	.0	.0	.0	.2	.1	.1	.1
75. *	.3	.0	.0	.0	.2	.1	.1	.1
80. *	.3	.0	.0	.0	.2	.1	.1	.1
85. *	.3	.0	.0	.0	.2	.1	.1	.1
90. *	.3	.0	.0	.0	.2	.1	.1	.1
95. *	.3	.0	.0	.0	.2	.1	.1	.1
100. *	.3	.0	.0	.0	.2	.1	.1	.1
105. *	.3	.0	.0	.0	.2	.1	.1	.1
110. *	.3	.0	.0	.0	.1	.1	.1	.1
115. *	.3	.0	.0	.0	.1	.1	.1	.1
120. *	.3	.0	.0	.0	.1	.1	.1	.1
125. *	.3	.0	.0	.0	.1	.1	.1	.1
130. *	.3	.0	.0	.0	.1	.1	.1	.1
135. *	.3	.0	.0	.0	.1	.1	.1	.1
140. *	.3	.0	.0	.0	.0	.1	.1	.1
145. *	.3	.0	.0	.0	.0	.0	.0	.0
150. *	.3	.0	.0	.0	.0	.0	.0	.0
155. *	.3	.0	.0	.0	.0	.0	.0	.0
160. *	.3	.0	.0	.0	.0	.0	.0	.0
165. *	.3	.0	.0	.0	.0	.0	.0	.0
170. *	.3	.0	.0	.0	.0	.0	.0	.0
175. *	.3	.0	.0	.0	.0	.0	.0	.0
180. *	.3	.0	.0	.0	.0	.0	.0	.0
185. *	.3	.0	.0	.0	.0	.0	.0	.0
190. *	.3	.0	.0	.0	.0	.0	.0	.0
195. *	.4	.0	.0	.0	.0	.0	.0	.0
200. *	.4	.0	.0	.0	.0	.0	.0	.0
205. *	.4	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 1 26th & Wilshire (S1EXAM.DAT) RUN: Site 1 Existing AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.4	.0	.0	.0	.0	.0	.0	.0
215. *	.4	.1	.1	.1	.1	.0	.0	.0
220. *	.3	.2	.2	.2	.1	.0	.0	.0
225. *	.2	.3	.3	.3	.3	.1	.0	.0
230. *	.2	.3	.4	.4	.4	.1	.0	.0
235. *	.1	.4	.4	.4	.5	.1	.1	.0
240. *	.0	.4	.4	.4	.5	.1	.1	.0
245. *	.0	.4	.5	.5	.5	.2	.1	.0
250. *	.0	.4	.4	.5	.4	.1	.1	.0
255. *	.0	.4	.4	.5	.4	.1	.1	.0
260. *	.0	.4	.4	.5	.4	.1	.1	.0
265. *	.0	.4	.4	.4	.4	.1	.1	.0
270. *	.0	.4	.4	.4	.4	.1	.1	.0
275. *	.0	.4	.4	.4	.3	.1	.1	.0
280. *	.0	.4	.4	.4	.3	.1	.1	.0
285. *	.0	.4	.4	.4	.3	.1	.1	.0
290. *	.0	.4	.4	.4	.3	.1	.0	.0
295. *	.0	.4	.4	.4	.3	.1	.0	.0
300. *	.0	.4	.4	.4	.3	.0	.0	.0
305. *	.0	.4	.4	.4	.3	.0	.0	.0
310. *	.0	.4	.4	.4	.2	.0	.0	.0
315. *	.0	.4	.4	.4	.2	.0	.0	.1
320. *	.0	.4	.4	.4	.2	.0	.1	.1
325. *	.0	.4	.4	.4	.2	.1	.1	.1
330. *	.0	.4	.4	.4	.2	.1	.1	.1
335. *	.0	.4	.4	.4	.2	.1	.2	.1
340. *	.0	.4	.4	.4	.2	.1	.2	.1
345. *	.0	.4	.4	.4	.2	.1	.2	.1
350. *	.0	.4	.4	.4	.2	.2	.3	.1
355. *	.0	.4	.5	.4	.2	.3	.3	.1
360. *	.0	.4	.4	.4	.3	.4	.2	.1
MAX *	.4	.4	.5	.5	.5	.4	.3	.1
DEGR. *	195	0	245	245	5	0	350	0

THE HIGHEST CONCENTRATION IS .80 PPM AT 65 DEGREES FROM REC10.
THE 2ND HIGHEST CONCENTRATION IS .70 PPM AT 70 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .60 PPM AT 60 DEGREES FROM REC11.

JOB: Site 1 26th & Wilshire (S1EXPM.DAT) RUN: Site 1 Existing PM
DATE: 03/19/2010 TIME: 08:32:40.36

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Wil AP	-15.0	139.0	583.0	699.0	819.	47.	AG	1229.	3.3	.0	44.0		
2.	EB	Wil T+R	584.0	699.0	715.0	824.0	181.	46.	AG	1142.	3.3	.0	44.0		
3.	EB	Wil T+R Q	672.0	783.0	-880.4	-714.6	2157.	226.	AG	72.	100.0	.0	24.0	1.48	109.6
4.	EB	Wil LT	569.0	717.0	698.0	843.0	180.	46.	AG	87.	3.3	.0	32.0		
5.	EB	Wil LT Q	654.0	800.0	435.3	586.8	305.	226.	AG	33.	100.0	.0	12.0	1.36	15.5
6.	EB	Wil DP	715.0	824.0	1421.0	1528.0	997.	45.	AG	1326.	3.3	.0	44.0		
7.	WB	Wil AP	1393.0	1557.0	810.0	982.0	819.	225.	AG	1384.	3.3	.0	44.0		
8.	WB	Wil T+R	806.0	986.0	684.0	868.0	170.	226.	AG	1181.	3.3	.0	56.0		
9.	WB	Wil T+R Q	717.0	900.0	930.9	1108.9	299.	46.	AG	104.	100.0	.0	36.0	1.02	15.2
10.	WB	Wil LT	824.0	966.0	707.0	850.0	165.	225.	AG	127.	3.3	.0	32.0		
11.	WB	Wil LT Q	737.0	880.0	1241.3	1384.3	713.	45.	AG	32.	100.0	.0	12.0	1.92	36.2
12.	WB	Wil DP	687.0	864.0	-35.0	163.0	1006.	226.	AG	1479.	3.3	.0	44.0		
13.	SB	26 AP	553.0	971.0	-6.0	1547.0	803.	316.	AG	694.	3.3	.0	32.0		
14.	SB	26 T+R	549.0	968.0	670.0	841.0	175.	136.	AG	555.	3.3	.0	44.0		
15.	SB	26 T+R Q	633.0	880.0	574.5	941.4	85.	316.	AG	68.	100.0	.0	24.0	.67	4.3
16.	SB	26 LT	563.0	978.0	679.0	856.0	168.	136.	AG	139.	3.3	.0	32.0		
17.	SB	26 LT Q	645.0	891.0	309.2	1247.8	490.	317.	AG	31.	100.0	.0	12.0	1.39	24.9
18.	SB	26 DP	672.0	845.0	1384.0	114.0	1020.	136.	AG	656.	3.3	.0	32.0		
19.	NB	26 AP	829.0	716.0	1410.0	138.0	820.	135.	AG	727.	3.3	.0	32.0		
20.	NB	26 T+R	832.0	719.0	715.0	846.0	173.	317.	AG	616.	3.3	.0	44.0		
21.	NB	26 T+R Q	759.0	798.0	829.1	721.9	103.	137.	AG	70.	100.0	.0	24.0	.77	5.3
22.	NB	26 L	818.0	710.0	705.0	832.0	166.	317.	AG	111.	3.3	.0	32.0		
23.	NB	26 L Q	747.0	787.0	778.4	752.9	46.	137.	AG	32.	100.0	.0	12.0	.82	2.4
24.	NB	26 DP	712.0	843.0	13.0	1565.0	1005.	316.	AG	700.	3.3	.0	32.0		

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JOB: Site 1 26th & Wilshire (S1EXPM.DAT) RUN: Site 1 Existing PM
DATE: 03/19/2010 TIME: 08:32:40.36

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB	Wil T+R Q	90	59	2.0	1142	1285	20.50	1	3
5.	EB	Wil LT Q	90	54	2.0	87	182	20.50	1	3
9.	WB	Wil T+R Q	90	57	2.0	1181	1196	20.50	1	3
11.	WB	Wil LT Q	90	52	2.0	127	176	20.50	1	3
15.	SB	26 T+R Q	90	56	2.0	555	1236	20.50	1	3
17.	SB	26 LT Q	90	50	2.0	139	252	20.50	1	3
21.	NB	26 T+R Q	90	57	2.0	616	1239	20.50	1	3
23.	NB	26 L Q	90	52	2.0	111	358	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	967.0	615.0	5.0
2.	SE 164 S	874.0	710.0	5.0
3.	SE 82 S	816.0	771.0	5.0
4.	SE CNR	768.0	826.0	5.0
5.	SE 82 E	819.0	886.0	5.0
6.	SE 164 E	877.0	944.0	5.0
7.	SE MID E	996.0	1059.0	5.0
8.	NE MID E	916.0	1134.0	5.0
9.	NE 164 E	800.0	1020.0	5.0
10.	NE 82 E	741.0	962.0	5.0
11.	NE CNR	680.0	915.0	5.0
12.	NE 82 N	628.0	964.0	5.0
13.	NE 164 N	570.0	1023.0	5.0
14.	NE MID N	454.0	1143.0	5.0
15.	NW MID N	391.0	1100.0	5.0
16.	NW 164 N	514.0	974.0	5.0
17.	NW 82 N	571.0	914.0	5.0
18.	NW CNR	621.0	855.0	5.0
19.	NW 82 W	570.0	797.0	5.0
20.	NW 164 W	512.0	740.0	5.0
21.	NW MID W	412.0	643.0	5.0
22.	SW MID W	484.0	558.0	5.0
23.	SW 164 W	589.0	658.0	5.0
24.	SW 82 W	649.0	715.0	5.0
25.	SW CNR	707.0	765.0	5.0
26.	SW 82 S	763.0	714.0	5.0
27.	SW 164 S	820.0	656.0	5.0
28.	SW MID S	919.0	554.0	5.0

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JOB: Site 1 26th & Wilshire (S1EXPM.DAT) RUN: Site 1 Existing PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.1	.2	.4	.5	.5	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.0	.0
5.	.0	.0	.2	.4	.5	.4	.3	.0	.0	.0	.0	.0	.0	.0	.2	.2	.3	.3	.0	.0
10.	.0	.0	.2	.3	.6	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
15.	.0	.0	.2	.4	.6	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
20.	.0	.0	.3	.5	.5	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.2	.4	.2	.1	.0
25.	.0	.0	.2	.5	.5	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.4	.2	.1	.0
30.	.0	.0	.1	.4	.5	.4	.3	.0	.0	.1	.0	.0	.0	.0	.1	.1	.3	.2	.0	.0
35.	.0	.0	.1	.4	.4	.3	.3	.1	.2	.2	.1	.0	.0	.0	.1	.1	.3	.3	.1	.0
40.	.0	.0	.0	.3	.3	.3	.3	.1	.2	.4	.2	.0	.0	.0	.1	.1	.3	.2	.1	.2
45.	.0	.0	.0	.1	.3	.3	.1	.1	.3	.4	.4	.0	.0	.0	.1	.1	.3	.4	.2	.2
50.	.0	.0	.0	.1	.1	.1	.1	.2	.5	.6	.5	.0	.0	.0	.1	.1	.3	.6	.3	.3
55.	.0	.0	.0	.1	.1	.1	.1	.3	.6	.6	.6	.1	.0	.0	.1	.1	.4	.6	.3	.3
60.	.0	.0	.0	.0	.1	.1	.0	.3	.7	.8	.6	.2	.0	.0	.1	.1	.5	.5	.3	.4
65.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.8	.6	.2	.0	.0	.1	.1	.4	.4	.3	.2
70.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.8	.5	.3	.0	.0	.1	.1	.5	.5	.2	.2
75.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.8	.5	.2	.0	.0	.1	.3	.5	.5	.2	.4
80.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.7	.5	.2	.1	.0	.1	.3	.4	.5	.2	.4
85.	.0	.0	.0	.0	.0	.0	.0	.3	.7	.6	.5	.1	.1	.0	.2	.3	.4	.3	.2	.4
90.	.0	.0	.0	.0	.0	.0	.0	.2	.6	.6	.4	.1	.1	.0	.2	.2	.4	.3	.3	.4
95.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.1	.1	.0	.3	.3	.4	.3	.3	.4
100.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.3	.3	.3	.1	.3	.3
105.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.3	.3	.3	.1	.3	.2
110.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.1	.3	.2	.3	.2	.3	.2
115.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.1	.3	.2	.3	.2	.3	.2
120.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.2	.2	.3	.2	.3	.2
125.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.2	.2	.3	.2
130.	.1	.1	.0	.0	.0	.0	.0	.3	.5	.5	.2	.1	.0	.1	.1	.2	.3	.3	.3	.2
135.	.1	.1	.1	.1	.0	.0	.0	.3	.5	.5	.2	.0	.1	.1	.0	.1	.3	.3	.3	.3
140.	.1	.1	.1	.2	.0	.0	.0	.3	.5	.5	.2	.1	.1	.1	.0	.1	.2	.2	.3	.3
145.	.1	.1	.2	.2	.0	.0	.0	.3	.5	.5	.2	.1	.1	.2	.0	.0	.1	.2	.3	.3
150.	.2	.2	.3	.4	.0	.0	.0	.4	.5	.5	.2	.1	.1	.2	.0	.0	.1	.3	.3	.3
155.	.2	.2	.4	.4	.0	.0	.0	.4	.5	.5	.3	.1	.2	.2	.0	.0	.1	.3	.3	.3
160.	.2	.2	.4	.4	.0	.0	.0	.4	.5	.5	.2	.1	.3	.2	.0	.0	.2	.3	.2	.3
165.	.2	.2	.3	.3	.0	.0	.0	.4	.6	.5	.2	.2	.3	.2	.0	.0	.2	.3	.2	.3
170.	.2	.2	.4	.3	.0	.0	.0	.5	.6	.5	.3	.3	.3	.3	.0	.0	.2	.3	.2	.3
175.	.1	.1	.3	.3	.0	.0	.0	.5	.6	.5	.3	.3	.3	.3	.0	.0	.2	.3	.3	.4
180.	.1	.1	.3	.3	.1	.0	.0	.5	.5	.5	.4	.4	.2	.3	.0	.0	.2	.3	.3	.4
185.	.1	.1	.3	.2	.1	.0	.0	.5	.6	.5	.5	.4	.3	.2	.0	.1	.2	.2	.4	.4
190.	.1	.1	.3	.2	.1	.0	.0	.6	.6	.4	.4	.4	.3	.2	.0	.1	.2	.3	.4	.4
195.	.1	.1	.3	.2	.1	.0	.0	.7	.6	.4	.3	.4	.3	.2	.0	.1	.2	.3	.4	.4
200.	.1	.1	.3	.2	.1	.0	.0	.7	.6	.6	.3	.4	.3	.2	.0	.1	.2	.3	.4	.4
205.	.1	.1	.3	.2	.1	.0	.0	.6	.6	.5	.3	.4	.3	.2	.0	.1	.2	.4	.4	.4

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.3	.2	.0	.0	.0	.6	.6	.5	.4	.4	.2	.2	.0	.1	.2	.4	.4	.4
215.	.1	.1	.3	.2	.1	.1	.1	.6	.6	.5	.4	.4	.2	.2	.0	.0	.2	.4	.4	.4
220.	.1	.1	.3	.2	.1	.2	.2	.5	.5	.4	.3	.4	.2	.2	.0	.0	.1	.3	.4	.4
225.	.1	.1	.4	.3	.3	.3	.2	.5	.5	.4	.3	.2	.2	.2	.0	.0	.0	.2	.2	.2
230.	.1	.1	.4	.6	.3	.3	.3	.3	.4	.3	.3	.2	.2	.2	.0	.0	.0	.2	.2	.2
235.	.1	.2	.4	.6	.3	.3	.4	.1	.2	.2	.3	.2	.2	.2	.0	.0	.0	.1	.1	.1
240.	.1	.2	.5	.4	.3	.4	.3	.1	.0	.0	.2	.2	.1	.2	.0	.0	.0	.0	.0	.0
245.	.1	.2	.5	.4	.3	.4	.3	.0	.0	.0	.2	.2	.1	.2	.0	.0	.0	.0	.0	.0
250.	.1	.2	.5	.4	.2	.4	.5	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0
255.	.1	.2	.5	.5	.3	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
260.	.1	.2	.5	.4	.2	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
265.	.1	.2	.5	.4	.2	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
270.	.1	.2	.5	.3	.3	.4	.4	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
275.	.1	.1	.4	.3	.3	.4	.4	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
280.	.1	.1	.4	.3	.3	.4	.4	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
285.	.2	.1	.3	.3	.3	.4	.3	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
290.	.2	.1	.3	.2	.3	.3	.3	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
295.	.1	.2	.2	.3	.3	.3	.3	.0	.0	.0	.2	.3	.3	.3	.0	.0	.0	.0	.0	.0
300.	.1	.2	.2	.2	.3	.3	.3	.0	.0	.0	.2	.3	.3	.3	.0	.0	.0	.0	.0	.0
305.	.1	.2	.2	.2	.4	.3	.3	.0	.0	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0
310.	.1	.2	.2	.3	.4	.4	.3	.0	.0	.0	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0
315.	.0	.1	.1	.3	.4	.4	.3	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.0	.0
320.	.0	.1	.2	.4	.4	.4	.2	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.2	.0	.0
325.	.0	.0	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.0	.0
330.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.2	.3	.4	.0	.0
335.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.2	.3	.4	.5	.0	.0
340.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.5	.0	.0
345.	.0	.1	.2	.3	.3	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.2	.3	.4	.5	.0	.0
350.	.0	.1	.2	.3	.3	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.5	.0	.0
355.	.0	.1	.2	.3	.3	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.0	.0
360.	.0	.1	.2	.4	.5	.5	.2	.0	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.0	.0
MAX DEGR.	.2 150	.2 150	.5 240	.6 230	.6 10	.5 0	.5 250	.7 195	.8 65	.8 60	.6 55	.4 180	.3 160	.3 170	.3 0	.3 0	.5 60	.6 50	.4 185	.4 60

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.4	.5	.4	.3	.4	.3	.2
5. *	.0	.4	.4	.4	.5	.4	.3	.1
10. *	.0	.5	.4	.3	.5	.4	.3	.1
15. *	.0	.5	.4	.3	.5	.4	.1	.1
20. *	.0	.4	.4	.3	.3	.4	.1	.1
25. *	.0	.4	.5	.4	.3	.4	.1	.1
30. *	.0	.4	.3	.4	.4	.3	.1	.1
35. *	.0	.4	.4	.3	.4	.3	.1	.1
40. *	.1	.3	.4	.3	.4	.2	.1	.1
45. *	.1	.2	.3	.2	.2	.2	.1	.1
50. *	.1	.1	.1	.1	.2	.2	.1	.1
55. *	.2	.1	.0	.0	.2	.2	.1	.1
60. *	.3	.0	.0	.0	.2	.2	.1	.1
65. *	.3	.0	.0	.0	.2	.2	.1	.1
70. *	.3	.0	.0	.0	.2	.2	.1	.1
75. *	.4	.0	.0	.0	.2	.2	.1	.1
80. *	.4	.0	.0	.0	.2	.2	.2	.1
85. *	.4	.0	.0	.0	.2	.2	.2	.2
90. *	.4	.0	.0	.0	.2	.1	.2	.2
95. *	.4	.0	.0	.0	.2	.1	.2	.2
100. *	.3	.0	.0	.0	.2	.1	.2	.2
105. *	.3	.0	.0	.0	.2	.1	.2	.2
110. *	.3	.0	.0	.0	.2	.2	.2	.2
115. *	.3	.0	.0	.0	.2	.2	.2	.2
120. *	.3	.0	.0	.0	.1	.2	.2	.2
125. *	.3	.0	.0	.0	.1	.2	.2	.2
130. *	.3	.0	.0	.0	.1	.2	.1	.1
135. *	.3	.0	.0	.0	.1	.1	.1	.1
140. *	.3	.0	.0	.0	.0	.1	.1	.1
145. *	.3	.0	.0	.0	.0	.0	.0	.0
150. *	.3	.0	.0	.0	.0	.0	.0	.0
155. *	.3	.0	.0	.0	.0	.0	.0	.0
160. *	.3	.0	.0	.0	.0	.0	.0	.0
165. *	.3	.0	.0	.0	.0	.0	.0	.0
170. *	.3	.0	.0	.0	.0	.0	.0	.0
175. *	.4	.0	.0	.0	.0	.0	.0	.0
180. *	.4	.0	.0	.0	.0	.0	.0	.0
185. *	.4	.0	.0	.0	.0	.0	.0	.0
190. *	.4	.0	.0	.0	.0	.0	.0	.0
195. *	.4	.0	.0	.0	.0	.0	.0	.0
200. *	.4	.0	.0	.0	.0	.0	.0	.0
205. *	.4	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 1 26th & Wilshire (S1EXPM.DAT) RUN: Site 1 Existing PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.4	.0	.0	.0	.0	.0	.0	.0
215. *	.4	.1	.1	.1	.1	.0	.0	.0
220. *	.4	.2	.2	.2	.1	.0	.0	.0
225. *	.2	.3	.3	.3	.3	.1	.0	.0
230. *	.2	.4	.4	.4	.4	.1	.0	.0
235. *	.1	.4	.5	.4	.5	.1	.1	.0
240. *	.0	.5	.5	.4	.5	.2	.1	.0
245. *	.0	.5	.5	.5	.5	.3	.1	.0
250. *	.0	.5	.5	.5	.4	.3	.1	.0
255. *	.0	.4	.5	.5	.4	.2	.1	.0
260. *	.0	.4	.4	.5	.4	.2	.1	.0
265. *	.0	.4	.4	.4	.4	.2	.1	.0
270. *	.0	.4	.4	.4	.4	.2	.1	.0
275. *	.0	.4	.4	.4	.3	.2	.1	.0
280. *	.0	.4	.4	.4	.3	.2	.1	.0
285. *	.0	.4	.4	.4	.3	.2	.1	.0
290. *	.0	.4	.4	.4	.3	.2	.1	.0
295. *	.0	.4	.4	.4	.3	.1	.0	.0
300. *	.0	.4	.4	.4	.3	.1	.0	.0
305. *	.0	.4	.4	.4	.3	.0	.0	.0
310. *	.0	.4	.4	.4	.2	.0	.0	.0
315. *	.0	.4	.4	.4	.2	.0	.0	.1
320. *	.0	.4	.4	.4	.2	.0	.1	.1
325. *	.0	.4	.4	.4	.2	.1	.1	.1
330. *	.0	.4	.4	.4	.3	.1	.2	.1
335. *	.0	.4	.4	.4	.3	.1	.2	.1
340. *	.0	.4	.4	.4	.2	.1	.2	.1
345. *	.0	.4	.4	.4	.2	.1	.3	.1
350. *	.0	.4	.4	.4	.2	.2	.3	.2
355. *	.0	.4	.5	.4	.2	.4	.3	.2
360. *	.0	.4	.5	.4	.3	.4	.3	.2
MAX *	.4	.5	.5	.5	.5	.4	.3	.2
DEGR. *	75	10	0	245	5	0	0	0

THE HIGHEST CONCENTRATION IS .80 PPM AT 65 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 60 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .70 PPM AT 195 DEGREES FROM REC8 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 1 26th & Wilshire (S1NBAM.DAT) RUN: Site 1 No Build AM
DATE: 03/19/2010 TIME: 08:37:14.44

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	*	-15.0	139.0	583.0	699.0	*	819.	47.	AG	1288.	.8	.0	44.0		
2.	EB Wil T+R	*	584.0	699.0	715.0	824.0	*	181.	46.	AG	1248.	.8	.0	44.0		
3.	EB Wil T+R Q	*	672.0	783.0	-3512.7	-3254.0	*	5815.	226.	AG	14.	100.0	.0	24.0	7.17	295.4
4.	EB Wil LT	*	569.0	717.0	698.0	843.0	*	180.	46.	AG	40.	.8	.0	32.0		
5.	EB Wil LT Q	*	654.0	800.0	643.5	789.8	*	15.	226.	AG	7.	100.0	.0	12.0	.65	.7
6.	EB Wil DP	*	715.0	824.0	1421.0	1528.0	*	997.	45.	AG	1363.	.8	.0	44.0		
7.	WB Wil AP	*	1393.0	1557.0	810.0	982.0	*	819.	225.	AG	1617.	.8	.0	44.0		
8.	WB Wil T+R	*	806.0	986.0	684.0	868.0	*	170.	226.	AG	1496.	.8	.0	56.0		
9.	WB Wil T+R Q	*	717.0	900.0	4109.1	4213.2	*	4742.	46.	AG	21.	100.0	.0	36.0	7.90	240.9
10.	WB Wil LT	*	824.0	966.0	707.0	850.0	*	165.	225.	AG	121.	.8	.0	32.0		
11.	WB Wil LT Q	*	737.0	880.0	1195.3	1338.3	*	648.	45.	AG	6.	100.0	.0	12.0	1.83	32.9
12.	WB Wil DP	*	687.0	864.0	-35.0	163.0	*	1006.	226.	AG	1515.	.8	.0	44.0		
13.	SB 26 AP	*	553.0	971.0	-6.0	1547.0	*	803.	316.	AG	817.	.8	.0	32.0		
14.	SB 26 T+R	*	549.0	968.0	670.0	841.0	*	175.	136.	AG	715.	.8	.0	44.0		
15.	SB 26 T+R Q	*	633.0	880.0	-1458.9	3073.9	*	3031.	316.	AG	14.	100.0	.0	24.0	4.46	154.0
16.	SB 26 LT	*	563.0	978.0	679.0	856.0	*	168.	136.	AG	102.	.8	.0	32.0		
17.	SB 26 LT Q	*	645.0	891.0	355.3	1198.8	*	423.	317.	AG	6.	100.0	.0	12.0	1.50	21.5
18.	SB 26 DP	*	672.0	845.0	1384.0	114.0	*	1020.	136.	AG	812.	.8	.0	32.0		
19.	NB 26 AP	*	829.0	716.0	1410.0	138.0	*	820.	135.	AG	707.	.8	.0	32.0		
20.	NB 26 T+R	*	832.0	719.0	715.0	846.0	*	173.	317.	AG	629.	.8	.0	44.0		
21.	NB 26 T+R Q	*	759.0	798.0	2493.7	-1085.4	*	2561.	137.	AG	14.	100.0	.0	24.0	3.88	130.1
22.	NB 26 L	*	818.0	710.0	705.0	832.0	*	166.	317.	AG	78.	.8	.0	32.0		
23.	NB 26 L Q	*	747.0	787.0	887.8	634.2	*	208.	137.	AG	6.	100.0	.0	12.0	1.22	10.6
24.	NB 26 DP	*	712.0	843.0	13.0	1565.0	*	1005.	316.	AG	739.	.8	.0	32.0		

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JOB: Site 1 26th & Wilshire (S1NBAM.DAT) RUN: Site 1 No Build AM
DATE: 03/19/2010 TIME: 08:37:14.44

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Wil T+R Q	*	90	59	2.0	1248	290	4.10	1	3
5.	EB Wil LT Q	*	90	55	2.0	40	182	4.10	1	3
9.	WB Wil T+R Q	*	90	56	2.0	1496	190	4.10	1	3
11.	WB Wil LT Q	*	90	51	2.0	121	170	4.10	1	3
15.	SB 26 T+R Q	*	90	56	2.0	715	242	4.10	1	3
17.	SB 26 LT Q	*	90	49	2.0	102	166	4.10	1	3
21.	NB 26 T+R Q	*	90	56	2.0	629	245	4.10	1	3
23.	NB 26 L Q	*	90	52	2.0	78	172	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	967.0	615.0	5.0	*
2.	SE 164 S	*	874.0	710.0	5.0	*
3.	SE 82 S	*	816.0	771.0	5.0	*
4.	SE CNR	*	768.0	826.0	5.0	*
5.	SE 82 E	*	819.0	886.0	5.0	*
6.	SE 164 E	*	877.0	944.0	5.0	*
7.	SE MID E	*	996.0	1059.0	5.0	*
8.	NE MID E	*	916.0	1134.0	5.0	*
9.	NE 164 E	*	800.0	1020.0	5.0	*
10.	NE 82 E	*	741.0	962.0	5.0	*
11.	NE CNR	*	680.0	915.0	5.0	*
12.	NE 82 N	*	628.0	964.0	5.0	*
13.	NE 164 N	*	570.0	1023.0	5.0	*
14.	NE MID N	*	454.0	1143.0	5.0	*
15.	NW MID N	*	391.0	1100.0	5.0	*
16.	NW 164 N	*	514.0	974.0	5.0	*
17.	NW 82 N	*	571.0	914.0	5.0	*
18.	NW CNR	*	621.0	855.0	5.0	*
19.	NW 82 W	*	570.0	797.0	5.0	*
20.	NW 164 W	*	512.0	740.0	5.0	*
21.	NW MID W	*	412.0	643.0	5.0	*
22.	SW MID W	*	484.0	558.0	5.0	*
23.	SW 164 W	*	589.0	658.0	5.0	*
24.	SW 82 W	*	649.0	715.0	5.0	*
25.	SW CNR	*	707.0	765.0	5.0	*
26.	SW 82 S	*	763.0	714.0	5.0	*
27.	SW 164 S	*	820.0	656.0	5.0	*
28.	SW MID S	*	919.0	554.0	5.0	*

1 PAGE 3

JOB: Site 1 26th & Wilshire (S1NBAM.DAT) RUN: Site 1 No Build AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
50.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
55.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
60.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
140.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
145.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
150.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
155.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
160.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
165.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
180.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
215.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX	.1	.1	.1	.1	.1	.1	.0	.2	.2	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.1
DEGR.	150	145	140	145	30	30	0	60	60	40	45	0	0	0	110	105	320	45	210	210

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.0	.0	.0	.0	.0
75. *	.0	.0	.0	.0	.0	.0	.0	.0
80. *	.0	.0	.0	.0	.0	.0	.0	.0
85. *	.0	.0	.0	.0	.0	.0	.0	.0
90. *	.0	.0	.0	.0	.0	.0	.0	.0
95. *	.0	.0	.0	.0	.0	.0	.0	.0
100. *	.0	.0	.0	.0	.0	.0	.0	.0
105. *	.0	.0	.0	.0	.0	.0	.0	.0
110. *	.0	.0	.0	.0	.0	.0	.0	.0
115. *	.0	.0	.0	.0	.0	.0	.0	.0
120. *	.0	.0	.0	.0	.0	.0	.0	.0
125. *	.0	.0	.0	.0	.0	.0	.0	.0
130. *	.0	.0	.0	.0	.0	.0	.0	.0
135. *	.0	.0	.0	.0	.0	.0	.0	.0
140. *	.0	.0	.0	.0	.0	.0	.0	.0
145. *	.0	.0	.0	.0	.0	.0	.0	.0
150. *	.0	.0	.0	.0	.0	.0	.0	.0
155. *	.0	.0	.0	.0	.0	.0	.0	.0
160. *	.0	.0	.0	.0	.0	.0	.0	.0
165. *	.0	.0	.0	.0	.0	.0	.0	.0
170. *	.0	.0	.0	.0	.0	.0	.0	.0
175. *	.0	.0	.0	.0	.0	.0	.0	.0
180. *	.0	.0	.0	.0	.0	.0	.0	.0
185. *	.0	.0	.0	.0	.0	.0	.0	.0
190. *	.0	.0	.0	.0	.0	.0	.0	.0
195. *	.0	.0	.0	.0	.0	.0	.0	.0
200. *	.0	.0	.0	.0	.0	.0	.0	.0
205. *	.0	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 1 26th & Wilshire (S1NBAM.DAT) RUN: Site 1 No Build AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.1	.0	.0	.0	.0	.0	.0	.0
215. *	.0	.0	.0	.0	.0	.0	.0	.0
220. *	.0	.0	.0	.0	.0	.0	.0	.0
225. *	.0	.0	.0	.0	.0	.0	.0	.0
230. *	.0	.0	.0	.0	.0	.0	.0	.0
235. *	.0	.1	.1	.0	.0	.0	.0	.0
240. *	.0	.1	.1	.0	.0	.0	.0	.0
245. *	.0	.0	.0	.0	.0	.0	.0	.0
250. *	.0	.0	.0	.0	.0	.0	.0	.0
255. *	.0	.0	.0	.0	.0	.0	.0	.0
260. *	.0	.0	.0	.0	.0	.0	.0	.0
265. *	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.1	.1	.1	.0	.0	.0	.0	.0
DEGR. *	210	235	235	0	0	0	0	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 60 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 60 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 150 DEGREES FROM REC1 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 1 26th & Wilshire (S1NBPM.DAT) RUN: Site 1 No Build PM
DATE: 03/19/2010 TIME: 08:36:37.97

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	*	-15.0	139.0	583.0	699.0	*	819.	47.	AG	1495.	.8	.0	44.0		
2.	EB Wil T+R	*	584.0	699.0	715.0	824.0	*	181.	46.	AG	1408.	.8	.0	44.0		
3.	EB Wil T+R Q	*	672.0	783.0	-4071.5	-3793.1	*	6591.	226.	AG	14.	100.0	.0	24.0	7.57	334.8
4.	EB Wil LT	*	569.0	717.0	698.0	843.0	*	180.	46.	AG	87.	.8	.0	32.0		
5.	EB Wil LT Q	*	654.0	800.0	420.3	572.1	*	326.	226.	AG	7.	100.0	.0	12.0	1.40	16.6
6.	EB Wil DP	*	715.0	824.0	1421.0	1528.0	*	997.	45.	AG	1726.	.8	.0	44.0		
7.	WB Wil AP	*	1393.0	1557.0	810.0	982.0	*	819.	225.	AG	1697.	.8	.0	44.0		
8.	WB Wil T+R	*	806.0	986.0	684.0	868.0	*	170.	226.	AG	1570.	.8	.0	56.0		
9.	WB Wil T+R Q	*	717.0	900.0	4284.0	4384.0	*	4986.	46.	AG	21.	100.0	.0	36.0	8.05	253.3
10.	WB Wil LT	*	824.0	966.0	707.0	850.0	*	165.	225.	AG	127.	.8	.0	32.0		
11.	WB Wil LT Q	*	737.0	880.0	1248.2	1391.2	*	723.	45.	AG	6.	100.0	.0	12.0	1.95	36.7
12.	WB Wil DP	*	687.0	864.0	-35.0	163.0	*	1006.	226.	AG	1707.	.8	.0	44.0		
13.	SB 26 AP	*	553.0	971.0	-6.0	1547.0	*	803.	316.	AG	830.	.8	.0	32.0		
14.	SB 26 T+R	*	549.0	968.0	670.0	841.0	*	175.	136.	AG	661.	.8	.0	44.0		
15.	SB 26 T+R Q	*	633.0	880.0	-1291.2	2898.1	*	2788.	316.	AG	14.	100.0	.0	24.0	4.34	141.7
16.	SB 26 LT	*	563.0	978.0	679.0	856.0	*	168.	136.	AG	169.	.8	.0	32.0		
17.	SB 26 LT Q	*	645.0	891.0	-144.8	1730.1	*	1152.	317.	AG	6.	100.0	.0	12.0	2.52	58.5
18.	SB 26 DP	*	672.0	845.0	1384.0	114.0	*	1020.	136.	AG	762.	.8	.0	32.0		
19.	NB 26 AP	*	829.0	716.0	1410.0	138.0	*	820.	135.	AG	921.	.8	.0	32.0		
20.	NB 26 T+R	*	832.0	719.0	715.0	846.0	*	173.	317.	AG	810.	.8	.0	44.0		
21.	NB 26 T+R Q	*	759.0	798.0	3184.9	-1835.9	*	3581.	137.	AG	14.	100.0	.0	24.0	5.26	181.9
22.	NB 26 L	*	818.0	710.0	705.0	832.0	*	166.	317.	AG	111.	.8	.0	32.0		
23.	NB 26 L Q	*	747.0	787.0	1113.9	388.7	*	541.	137.	AG	6.	100.0	.0	12.0	1.68	27.5
24.	NB 26 DP	*	712.0	843.0	13.0	1565.0	*	1005.	316.	AG	748.	.8	.0	32.0		

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JOB: Site 1 26th & Wilshire (S1NBPM.DAT) RUN: Site 1 No Build PM
DATE: 03/19/2010 TIME: 08:36:37.97

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Wil T+R Q	*	90	57	2.0	1408	289	4.10	1	3
5.	EB Wil LT Q	*	90	55	2.0	87	182	4.10	1	3
9.	WB Wil T+R Q	*	90	56	2.0	1570	196	4.10	1	3
11.	WB Wil LT Q	*	90	51	2.0	127	169	4.10	1	3
15.	SB 26 T+R Q	*	90	57	2.0	661	236	4.10	1	3
17.	SB 26 LT Q	*	90	51	2.0	169	174	4.10	1	3
21.	NB 26 T+R Q	*	90	57	2.0	810	239	4.10	1	3
23.	NB 26 L Q	*	90	52	2.0	111	177	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	967.0	615.0	5.0	*
2.	SE 164 S	*	874.0	710.0	5.0	*
3.	SE 82 S	*	816.0	771.0	5.0	*
4.	SE CNR	*	768.0	826.0	5.0	*
5.	SE 82 E	*	819.0	886.0	5.0	*
6.	SE 164 E	*	877.0	944.0	5.0	*
7.	SE MID E	*	996.0	1059.0	5.0	*
8.	NE MID E	*	916.0	1134.0	5.0	*
9.	NE 164 E	*	800.0	1020.0	5.0	*
10.	NE 82 E	*	741.0	962.0	5.0	*
11.	NE CNR	*	680.0	915.0	5.0	*
12.	NE 82 N	*	628.0	964.0	5.0	*
13.	NE 164 N	*	570.0	1023.0	5.0	*
14.	NE MID N	*	454.0	1143.0	5.0	*
15.	NW MID N	*	391.0	1100.0	5.0	*
16.	NW 164 N	*	514.0	974.0	5.0	*
17.	NW 82 N	*	571.0	914.0	5.0	*
18.	NW CNR	*	621.0	855.0	5.0	*
19.	NW 82 W	*	570.0	797.0	5.0	*
20.	NW 164 W	*	512.0	740.0	5.0	*
21.	NW MID W	*	412.0	643.0	5.0	*
22.	SW MID W	*	484.0	558.0	5.0	*
23.	SW 164 W	*	589.0	658.0	5.0	*
24.	SW 82 W	*	649.0	715.0	5.0	*
25.	SW CNR	*	707.0	765.0	5.0	*
26.	SW 82 S	*	763.0	714.0	5.0	*
27.	SW 164 S	*	820.0	656.0	5.0	*
28.	SW MID S	*	919.0	554.0	5.0	*

1 PAGE 3

JOB: Site 1 26th & Wilshire (S1NBPM.DAT) RUN: Site 1 No Build PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.0	.1	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
50.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
55.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
60.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
140.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
145.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
150.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
155.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
160.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
165.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
170.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
180.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
200.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
205.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1

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JOB: Site 1 26th & Wilshire (S1NBPM.DAT) RUN: Site 1 No Build PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
215.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
220.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX DEGR.	.1	.1	.1	.1	.1	.1	.1	.2	.2	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.1
	145	140	140	20	5	5	10	55	55	40	45	0	0	0	105	100	320	45	195	195

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JOB: Site 1 26th & Wilshire (S1NBPM.DAT) RUN: Site 1 No Build PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	* CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.1	.0	.0	.0	.0	.0	.0	.0
65. *	.1	.0	.0	.0	.0	.0	.0	.0
70. *	.1	.0	.0	.0	.0	.0	.0	.0
75. *	.1	.0	.0	.0	.0	.0	.0	.0
80. *	.0	.0	.0	.0	.0	.0	.0	.0
85. *	.0	.0	.0	.0	.0	.0	.0	.0
90. *	.0	.0	.0	.0	.0	.0	.0	.0
95. *	.0	.0	.0	.0	.0	.0	.0	.0
100. *	.0	.0	.0	.0	.0	.0	.0	.0
105. *	.0	.0	.0	.0	.0	.0	.0	.0
110. *	.0	.0	.0	.0	.0	.0	.0	.0
115. *	.0	.0	.0	.0	.0	.0	.0	.0
120. *	.0	.0	.0	.0	.0	.0	.0	.0
125. *	.0	.0	.0	.0	.0	.0	.0	.0
130. *	.0	.0	.0	.0	.0	.0	.0	.0
135. *	.0	.0	.0	.0	.0	.0	.0	.0
140. *	.0	.0	.0	.0	.0	.0	.0	.0
145. *	.0	.0	.0	.0	.0	.0	.0	.0
150. *	.0	.0	.0	.0	.0	.0	.0	.0
155. *	.0	.0	.0	.0	.0	.0	.0	.0
160. *	.0	.0	.0	.0	.0	.0	.0	.0
165. *	.0	.0	.0	.0	.0	.0	.0	.0
170. *	.0	.0	.0	.0	.0	.0	.0	.0
175. *	.0	.0	.0	.0	.0	.0	.0	.0
180. *	.0	.0	.0	.0	.0	.0	.0	.0
185. *	.0	.0	.0	.0	.0	.0	.0	.0
190. *	.0	.0	.0	.0	.0	.0	.0	.0
195. *	.1	.0	.0	.0	.0	.0	.0	.0
200. *	.1	.0	.0	.0	.0	.0	.0	.0
205. *	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 1 26th & Wilshire (S1NBPM.DAT) RUN: Site 1 No Build PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.1	.0	.0	.0	.0	.0	.0	.0
215. *	.1	.0	.0	.0	.0	.0	.0	.0
220. *	.0	.0	.0	.0	.0	.0	.0	.0
225. *	.0	.0	.0	.0	.0	.0	.0	.0
230. *	.0	.0	.0	.0	.0	.0	.0	.0
235. *	.0	.0	.0	.0	.0	.0	.0	.0
240. *	.0	.0	.0	.0	.0	.0	.0	.0
245. *	.0	.0	.0	.0	.0	.0	.0	.0
250. *	.0	.0	.0	.0	.0	.0	.0	.0
255. *	.0	.0	.0	.0	.0	.0	.0	.0
260. *	.0	.0	.0	.0	.0	.0	.0	.0
265. *	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.1	.0	.0	.0	.0	.0	.0	.0
DEGR. *	60	0	0	0	0	0	0	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 55 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 55 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 145 DEGREES FROM REC1 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 1 26th & Wilshire (S1B3AM.DAT) RUN: Site 1 Build Alt3 AM
DATE: 03/19/2010 TIME: 08:42:35.42

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-15.0	139.0	583.0	699.0	819.	47.	AG	1275.	.8	.0	44.0		
2.	EB Wil T+R	584.0	699.0	715.0	824.0	181.	46.	AG	1235.	.8	.0	44.0		
3.	EB Wil T+R Q	672.0	783.0	-3467.3	-3210.2	5752.	226.	AG	14.	100.0	.0	24.0	7.17	292.2
4.	EB Wil LT	569.0	717.0	698.0	843.0	180.	46.	AG	40.	.8	.0	32.0		
5.	EB Wil LT Q	654.0	800.0	643.5	789.8	15.	226.	AG	7.	100.0	.0	12.0	.65	.7
6.	EB Wil DP	715.0	824.0	1421.0	1528.0	997.	45.	AG	1352.	.8	.0	44.0		
7.	WB Wil AP	1393.0	1557.0	810.0	982.0	819.	225.	AG	1613.	.8	.0	44.0		
8.	WB Wil T+R	806.0	986.0	684.0	868.0	170.	226.	AG	1492.	.8	.0	56.0		
9.	WB Wil T+R Q	717.0	900.0	4101.4	4205.7	4731.	46.	AG	21.	100.0	.0	36.0	7.89	240.3
10.	WB Wil LT	824.0	966.0	707.0	850.0	165.	225.	AG	121.	.8	.0	32.0		
11.	WB Wil LT Q	737.0	880.0	1195.3	1338.3	648.	45.	AG	6.	100.0	.0	12.0	1.83	32.9
12.	WB Wil DP	687.0	864.0	-35.0	163.0	1006.	226.	AG	1491.	.8	.0	44.0		
13.	SB 26 AP	553.0	971.0	-6.0	1547.0	803.	316.	AG	822.	.8	.0	32.0		
14.	SB 26 T+R	549.0	968.0	670.0	841.0	175.	136.	AG	714.	.8	.0	44.0		
15.	SB 26 T+R Q	633.0	880.0	-1544.0	3163.2	3155.	316.	AG	14.	100.0	.0	24.0	5.17	160.3
16.	SB 26 LT	563.0	978.0	679.0	856.0	168.	136.	AG	108.	.8	.0	32.0		
17.	SB 26 LT Q	645.0	891.0	388.3	1163.8	375.	317.	AG	6.	100.0	.0	12.0	1.37	19.0
18.	SB 26 DP	672.0	845.0	1384.0	114.0	1020.	136.	AG	808.	.8	.0	32.0		
19.	NB 26 AP	829.0	716.0	1410.0	138.0	820.	135.	AG	669.	.8	.0	32.0		
20.	NB 26 T+R	832.0	719.0	715.0	846.0	173.	317.	AG	591.	.8	.0	44.0		
21.	NB 26 T+R Q	759.0	798.0	2461.3	-1050.3	2513.	137.	AG	14.	100.0	.0	24.0	4.40	127.6
22.	NB 26 L	818.0	710.0	705.0	832.0	166.	317.	AG	78.	.8	.0	32.0		
23.	NB 26 L Q	747.0	787.0	887.8	634.2	208.	137.	AG	6.	100.0	.0	12.0	1.22	10.6
24.	NB 26 DP	712.0	843.0	13.0	1565.0	1005.	316.	AG	725.	.8	.0	32.0		

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JOB: Site 1 26th & Wilshire (S1B3AM.DAT) RUN: Site 1 Build Alt3 AM
DATE: 03/19/2010 TIME: 08:42:35.42

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Wil T+R Q	90	59	2.0	1235	288	4.10	1	3
5.	EB Wil LT Q	90	55	2.0	40	182	4.10	1	3
9.	WB Wil T+R Q	90	56	2.0	1492	190	4.10	1	3
11.	WB Wil LT Q	90	51	2.0	121	170	4.10	1	3
15.	SB 26 T+R Q	90	56	2.0	714	208	4.10	1	3
17.	SB 26 LT Q	90	50	2.0	108	198	4.10	1	3
21.	NB 26 T+R Q	90	57	2.0	591	210	4.10	1	3
23.	NB 26 L Q	90	52	2.0	78	172	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	967.0	615.0	5.0
2.	SE 164 S	874.0	710.0	5.0
3.	SE 82 S	816.0	771.0	5.0
4.	SE CNR	768.0	826.0	5.0
5.	SE 82 E	819.0	886.0	5.0
6.	SE 164 E	877.0	944.0	5.0
7.	SE MID E	996.0	1059.0	5.0
8.	NE MID E	916.0	1134.0	5.0
9.	NE 164 E	800.0	1020.0	5.0
10.	NE 82 E	741.0	962.0	5.0
11.	NE CNR	680.0	915.0	5.0
12.	NE 82 N	628.0	964.0	5.0
13.	NE 164 N	570.0	1023.0	5.0
14.	NE MID N	454.0	1143.0	5.0
15.	NW MID N	391.0	1100.0	5.0
16.	NW 164 N	514.0	974.0	5.0
17.	NW 82 N	571.0	914.0	5.0
18.	NW CNR	621.0	855.0	5.0
19.	NW 82 W	570.0	797.0	5.0
20.	NW 164 W	512.0	740.0	5.0
21.	NW MID W	412.0	643.0	5.0
22.	SW MID W	484.0	558.0	5.0
23.	SW 164 W	589.0	658.0	5.0
24.	SW 82 W	649.0	715.0	5.0
25.	SW CNR	707.0	765.0	5.0
26.	SW 82 S	763.0	714.0	5.0
27.	SW 164 S	820.0	656.0	5.0
28.	SW MID S	919.0	554.0	5.0

1 PAGE 3

JOB: Site 1 26th & Wilshire (S1B3AM.DAT) RUN: Site 1 Build Alt3 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
140.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
145.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
150.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
155.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
160.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
165.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
170.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
180.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
215.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX DEGR.	.1 150	.1 145	.1 140	.1 145	.1 30	.1 30	.0 0	.2 60	.2 60	.1 40	.1 45	.0 0	.0 0	.0 0	.1 110	.1 105	.1 320	.1 45	.1 210	.1 210

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.0	.0	.0	.0	.0
75. *	.0	.0	.0	.0	.0	.0	.0	.0
80. *	.0	.0	.0	.0	.0	.0	.0	.0
85. *	.0	.0	.0	.0	.0	.0	.0	.0
90. *	.0	.0	.0	.0	.0	.0	.0	.0
95. *	.0	.0	.0	.0	.0	.0	.0	.0
100. *	.0	.0	.0	.0	.0	.0	.0	.0
105. *	.0	.0	.0	.0	.0	.0	.0	.0
110. *	.0	.0	.0	.0	.0	.0	.0	.0
115. *	.0	.0	.0	.0	.0	.0	.0	.0
120. *	.0	.0	.0	.0	.0	.0	.0	.0
125. *	.0	.0	.0	.0	.0	.0	.0	.0
130. *	.0	.0	.0	.0	.0	.0	.0	.0
135. *	.0	.0	.0	.0	.0	.0	.0	.0
140. *	.0	.0	.0	.0	.0	.0	.0	.0
145. *	.0	.0	.0	.0	.0	.0	.0	.0
150. *	.0	.0	.0	.0	.0	.0	.0	.0
155. *	.0	.0	.0	.0	.0	.0	.0	.0
160. *	.0	.0	.0	.0	.0	.0	.0	.0
165. *	.0	.0	.0	.0	.0	.0	.0	.0
170. *	.0	.0	.0	.0	.0	.0	.0	.0
175. *	.0	.0	.0	.0	.0	.0	.0	.0
180. *	.0	.0	.0	.0	.0	.0	.0	.0
185. *	.0	.0	.0	.0	.0	.0	.0	.0
190. *	.0	.0	.0	.0	.0	.0	.0	.0
195. *	.0	.0	.0	.0	.0	.0	.0	.0
200. *	.0	.0	.0	.0	.0	.0	.0	.0
205. *	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 1 26th & Wilshire (S1B3AM.DAT) RUN: Site 1 Build Alt3 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.0	.0	.0	.0	.0	.0	.0	.0
215. *	.0	.0	.0	.0	.0	.0	.0	.0
220. *	.0	.0	.0	.0	.0	.0	.0	.0
225. *	.0	.0	.0	.0	.0	.0	.0	.0
230. *	.0	.0	.0	.0	.0	.0	.0	.0
235. *	.0	.1	.1	.0	.0	.0	.0	.0
240. *	.0	.1	.1	.0	.0	.0	.0	.0
245. *	.0	.0	.0	.0	.0	.0	.0	.0
250. *	.0	.0	.0	.0	.0	.0	.0	.0
255. *	.0	.0	.0	.0	.0	.0	.0	.0
260. *	.0	.0	.0	.0	.0	.0	.0	.0
265. *	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.1	.1	.0	.0	.0	.0	.0
DEGR. *	0	235	235	0	0	0	0	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 60 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 60 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 150 DEGREES FROM REC1 .

JOB: Site 1 26th & Wilshire (S1B3PM.DAT) RUN: Site 1 Build Alt3 PM
DATE: 03/19/2010 TIME: 08:42:55.91

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Wil AP	-15.0	139.0	583.0	699.0	819.	47.	AG	1509.	.8	.0	44.0		
2.	EB	Wil T+R	584.0	699.0	715.0	824.0	181.	46.	AG	1422.	.8	.0	44.0		
3.	EB	Wil T+R Q	672.0	783.0	-4133.7	-3853.1	6677.	226.	AG	14.	100.0	.0	24.0	7.73	339.2
4.	EB	Wil LT	569.0	717.0	698.0	843.0	180.	46.	AG	87.	.8	.0	32.0		
5.	EB	Wil LT Q	654.0	800.0	435.7	587.1	305.	226.	AG	6.	100.0	.0	12.0	1.36	15.5
6.	EB	Wil DP	715.0	824.0	1421.0	1528.0	997.	45.	AG	1766.	.8	.0	44.0		
7.	WB	Wil AP	1393.0	1557.0	810.0	982.0	819.	225.	AG	1713.	.8	.0	44.0		
8.	WB	Wil T+R	806.0	986.0	684.0	868.0	170.	226.	AG	1586.	.8	.0	56.0		
9.	WB	Wil T+R Q	717.0	900.0	4322.5	4421.6	5040.	46.	AG	21.	100.0	.0	36.0	8.12	256.0
10.	WB	Wil LT	824.0	966.0	707.0	850.0	165.	225.	AG	127.	.8	.0	32.0		
11.	WB	Wil LT Q	737.0	880.0	1248.2	1391.2	723.	45.	AG	6.	100.0	.0	12.0	1.95	36.7
12.	WB	Wil DP	687.0	864.0	-35.0	163.0	1006.	226.	AG	1728.	.8	.0	44.0		
13.	SB	26 AP	553.0	971.0	-6.0	1547.0	803.	316.	AG	852.	.8	.0	32.0		
14.	SB	26 T+R	549.0	968.0	670.0	841.0	175.	136.	AG	680.	.8	.0	44.0		
15.	SB	26 T+R Q	633.0	880.0	-1458.6	3073.6	3031.	316.	AG	14.	100.0	.0	24.0	5.31	154.0
16.	SB	26 LT	563.0	978.0	679.0	856.0	168.	136.	AG	169.	.8	.0	32.0		
17.	SB	26 LT Q	645.0	891.0	-160.0	1746.3	1175.	317.	AG	6.	100.0	.0	12.0	2.60	59.7
18.	SB	26 DP	672.0	845.0	1384.0	114.0	1020.	136.	AG	765.	.8	.0	32.0		
19.	NB	26 AP	829.0	716.0	1410.0	138.0	820.	135.	AG	974.	.8	.0	32.0		
20.	NB	26 T+R	832.0	719.0	715.0	846.0	173.	317.	AG	863.	.8	.0	44.0		
21.	NB	26 T+R Q	759.0	798.0	3485.9	-2162.6	4025.	137.	AG	14.	100.0	.0	24.0	6.84	204.5
22.	NB	26 L	818.0	710.0	705.0	832.0	166.	317.	AG	111.	.8	.0	32.0		
23.	NB	26 L Q	747.0	787.0	1113.9	388.7	541.	137.	AG	6.	100.0	.0	12.0	1.68	27.5
24.	NB	26 DP	712.0	843.0	13.0	1565.0	1005.	316.	AG	793.	.8	.0	32.0		

JOB: Site 1 26th & Wilshire (S1B3PM.DAT) RUN: Site 1 Build Alt3 PM
DATE: 03/19/2010 TIME: 08:42:55.91

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB	Wil T+R Q	90	57	2.0	1422	287	4.10	1	3
5.	EB	Wil LT Q	90	53	2.0	87	175	4.10	1	3
9.	WB	Wil T+R Q	90	56	2.0	1586	196	4.10	1	3
11.	WB	Wil LT Q	90	51	2.0	127	169	4.10	1	3
15.	SB	26 T+R Q	90	57	2.0	680	200	4.10	1	3
17.	SB	26 LT Q	90	52	2.0	169	174	4.10	1	3
21.	NB	26 T+R Q	90	58	2.0	863	204	4.10	1	3
23.	NB	26 L Q	90	52	2.0	111	177	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	967.0	615.0	5.0
2.	SE 164 S	874.0	710.0	5.0
3.	SE 82 S	816.0	771.0	5.0
4.	SE CNR	768.0	826.0	5.0
5.	SE 82 E	819.0	886.0	5.0
6.	SE 164 E	877.0	944.0	5.0
7.	SE MID E	996.0	1059.0	5.0
8.	NE MID E	916.0	1134.0	5.0
9.	NE 164 E	800.0	1020.0	5.0
10.	NE 82 E	741.0	962.0	5.0
11.	NE CNR	680.0	915.0	5.0
12.	NE 82 N	628.0	964.0	5.0
13.	NE 164 N	570.0	1023.0	5.0
14.	NE MID N	454.0	1143.0	5.0
15.	NW MID N	391.0	1100.0	5.0
16.	NW 164 N	514.0	974.0	5.0
17.	NW 82 N	571.0	914.0	5.0
18.	NW CNR	621.0	855.0	5.0
19.	NW 82 W	570.0	797.0	5.0
20.	NW 164 W	512.0	740.0	5.0
21.	NW MID W	412.0	643.0	5.0
22.	SW MID W	484.0	558.0	5.0
23.	SW 164 W	589.0	658.0	5.0
24.	SW 82 W	649.0	715.0	5.0
25.	SW CNR	707.0	765.0	5.0
26.	SW 82 S	763.0	714.0	5.0
27.	SW 164 S	820.0	656.0	5.0
28.	SW MID S	919.0	554.0	5.0

JOB: Site 1 26th & Wilshire (S1B3PM.DAT) RUN: Site 1 Build Alt3 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
50.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
55.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
60.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
140.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
145.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
150.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
155.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
160.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
165.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
170.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
180.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
200.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
205.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
215.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
220.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX DEGR.	.1 145	.1 140	.1 140	.1 15	.1 5	.1 5	.1 10	.2 55	.2 55	.1 40	.1 45	.0 0	.0 0	.0 0	.1 105	.1 100	.1 320	.1 45	.1 195	.1 195

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.1	.0	.0	.0	.0	.0	.0	.0
65. *	.1	.0	.0	.0	.0	.0	.0	.0
70. *	.1	.0	.0	.0	.0	.0	.0	.0
75. *	.1	.0	.0	.0	.0	.0	.0	.0
80. *	.0	.0	.0	.0	.0	.0	.0	.0
85. *	.0	.0	.0	.0	.0	.0	.0	.0
90. *	.0	.0	.0	.0	.0	.0	.0	.0
95. *	.0	.0	.0	.0	.0	.0	.0	.0
100. *	.0	.0	.0	.0	.0	.0	.0	.0
105. *	.0	.0	.0	.0	.0	.0	.0	.0
110. *	.0	.0	.0	.0	.0	.0	.0	.0
115. *	.0	.0	.0	.0	.0	.0	.0	.0
120. *	.0	.0	.0	.0	.0	.0	.0	.0
125. *	.0	.0	.0	.0	.0	.0	.0	.0
130. *	.0	.0	.0	.0	.0	.0	.0	.0
135. *	.0	.0	.0	.0	.0	.0	.0	.0
140. *	.0	.0	.0	.0	.0	.0	.0	.0
145. *	.0	.0	.0	.0	.0	.0	.0	.0
150. *	.0	.0	.0	.0	.0	.0	.0	.0
155. *	.0	.0	.0	.0	.0	.0	.0	.0
160. *	.0	.0	.0	.0	.0	.0	.0	.0
165. *	.0	.0	.0	.0	.0	.0	.0	.0
170. *	.0	.0	.0	.0	.0	.0	.0	.0
175. *	.0	.0	.0	.0	.0	.0	.0	.0
180. *	.0	.0	.0	.0	.0	.0	.0	.0
185. *	.0	.0	.0	.0	.0	.0	.0	.0
190. *	.0	.0	.0	.0	.0	.0	.0	.0
195. *	.1	.0	.0	.0	.0	.0	.0	.0
200. *	.1	.0	.0	.0	.0	.0	.0	.0
205. *	.1	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 1 26th & Wilshire (S1B3PM.DAT) RUN: Site 1 Build Alt3 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.1	.0	.0	.0	.0	.0	.0	.0
215. *	.1	.0	.0	.0	.0	.0	.0	.0
220. *	.0	.0	.0	.0	.0	.0	.0	.0
225. *	.0	.0	.0	.0	.0	.0	.0	.0
230. *	.0	.0	.0	.0	.0	.0	.0	.0
235. *	.0	.0	.0	.0	.0	.0	.0	.0
240. *	.0	.0	.0	.0	.0	.0	.0	.0
245. *	.0	.0	.0	.0	.0	.0	.0	.0
250. *	.0	.0	.0	.0	.0	.0	.0	.0
255. *	.0	.0	.0	.0	.0	.0	.0	.0
260. *	.0	.0	.0	.0	.0	.0	.0	.0
265. *	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.1	.0	.0	.0	.0	.0	.0	.0
DEGR. *	60	0	0	0	0	0	0	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 55 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 55 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 145 DEGREES FROM REC1 .

JOB: Site 1 26th & Wilshire (S1B5AM.DAT) RUN: Site 1 Build Alt5 AM
DATE: 03/19/2010 TIME: 08:43:23.32

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Wil AP	-15.0	139.0	583.0	699.0	819.	47.	AG	1254.	.8	.0	44.0		
2.	EB	Wil T+R	584.0	699.0	715.0	824.0	181.	46.	AG	1214.	.8	.0	44.0		
3.	EB	Wil T+R Q	672.0	783.0	-3390.4	-3136.0	5645.	226.	AG	14.	100.0	.0	24.0	7.06	286.7
4.	EB	Wil LT	569.0	717.0	698.0	843.0	180.	46.	AG	40.	.8	.0	32.0		
5.	EB	Wil LT Q	654.0	800.0	643.5	789.8	15.	226.	AG	7.	100.0	.0	12.0	.65	.7
6.	EB	Wil DP	715.0	824.0	1421.0	1528.0	997.	45.	AG	1331.	.8	.0	44.0		
7.	WB	Wil AP	1393.0	1557.0	810.0	982.0	819.	225.	AG	1560.	.8	.0	44.0		
8.	WB	Wil T+R	806.0	986.0	684.0	868.0	170.	226.	AG	1439.	.8	.0	56.0		
9.	WB	Wil T+R Q	717.0	900.0	3962.8	4070.3	4537.	46.	AG	21.	100.0	.0	36.0	7.60	230.5
10.	WB	Wil LT	824.0	966.0	707.0	850.0	165.	225.	AG	121.	.8	.0	32.0		
11.	WB	Wil LT Q	737.0	880.0	1187.5	1330.5	637.	45.	AG	6.	100.0	.0	12.0	1.81	32.4
12.	WB	Wil DP	687.0	864.0	-35.0	163.0	1006.	226.	AG	1550.	.8	.0	44.0		
13.	SB	26 AP	553.0	971.0	-6.0	1547.0	803.	316.	AG	823.	.8	.0	32.0		
14.	SB	26 T+R	549.0	968.0	670.0	841.0	175.	136.	AG	715.	.8	.0	44.0		
15.	SB	26 T+R Q	633.0	880.0	-1575.6	3196.3	3200.	316.	AG	14.	100.0	.0	24.0	5.49	162.6
16.	SB	26 LT	563.0	978.0	679.0	856.0	168.	136.	AG	108.	.8	.0	32.0		
17.	SB	26 LT Q	645.0	891.0	388.3	1163.8	375.	317.	AG	6.	100.0	.0	12.0	1.37	19.0
18.	SB	26 DP	672.0	845.0	1384.0	114.0	1020.	136.	AG	812.	.8	.0	32.0		
19.	NB	26 AP	829.0	716.0	1410.0	138.0	820.	135.	AG	669.	.8	.0	32.0		
20.	NB	26 T+R	832.0	719.0	715.0	846.0	173.	317.	AG	591.	.8	.0	44.0		
21.	NB	26 T+R Q	759.0	798.0	2484.1	-1075.0	2546.	137.	AG	14.	100.0	.0	24.0	4.61	129.4
22.	NB	26 L	818.0	710.0	705.0	832.0	166.	317.	AG	78.	.8	.0	32.0		
23.	NB	26 L Q	747.0	787.0	887.8	634.2	208.	137.	AG	6.	100.0	.0	12.0	1.22	10.6
24.	NB	26 DP	712.0	843.0	13.0	1565.0	1005.	316.	AG	707.	.8	.0	32.0		

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JOB: Site 1 26th & Wilshire (S1B5AM.DAT) RUN: Site 1 Build Alt5 AM
DATE: 03/19/2010 TIME: 08:43:23.32

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB	Wil T+R Q	90	59	2.0	1214	289	4.10	1	3
5.	EB	Wil LT Q	90	55	2.0	40	182	4.10	1	3
9.	WB	Wil T+R Q	90	56	2.0	1439	190	4.10	1	3
11.	WB	Wil LT Q	90	50	2.0	121	170	4.10	1	3
15.	SB	26 T+R Q	90	56	2.0	715	196	4.10	1	3
17.	SB	26 LT Q	90	50	2.0	108	198	4.10	1	3
21.	NB	26 T+R Q	90	57	2.0	591	199	4.10	1	3
23.	NB	26 L Q	90	52	2.0	78	172	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	967.0	615.0	5.0
2.	SE 164 S	874.0	710.0	5.0
3.	SE 82 S	816.0	771.0	5.0
4.	SE CNR	768.0	826.0	5.0
5.	SE 82 E	819.0	886.0	5.0
6.	SE 164 E	877.0	944.0	5.0
7.	SE MID E	996.0	1059.0	5.0
8.	NE MID E	916.0	1134.0	5.0
9.	NE 164 E	800.0	1020.0	5.0
10.	NE 82 E	741.0	962.0	5.0
11.	NE CNR	680.0	915.0	5.0
12.	NE 82 N	628.0	964.0	5.0
13.	NE 164 N	570.0	1023.0	5.0
14.	NE MID N	454.0	1143.0	5.0
15.	NW MID N	391.0	1100.0	5.0
16.	NW 164 N	514.0	974.0	5.0
17.	NW 82 N	571.0	914.0	5.0
18.	NW CNR	621.0	855.0	5.0
19.	NW 82 W	570.0	797.0	5.0
20.	NW 164 W	512.0	740.0	5.0
21.	NW MID W	412.0	643.0	5.0
22.	SW MID W	484.0	558.0	5.0
23.	SW 164 W	589.0	658.0	5.0
24.	SW 82 W	649.0	715.0	5.0
25.	SW CNR	707.0	765.0	5.0
26.	SW 82 S	763.0	714.0	5.0
27.	SW 164 S	820.0	656.0	5.0
28.	SW MID S	919.0	554.0	5.0

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JOB: Site 1 26th & Wilshire (S1B5AM.DAT) RUN: Site 1 Build Alt5 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
55.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
60.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
140.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
145.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
150.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
155.	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
160.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
165.	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
170.	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
180.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
215.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
220.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.1
DEGR.	150	145	140	145	0	0	0	60	60	40	45	0	0	0	110	105	320	50	205	205

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.0	.0	.0	.0	.0
75. *	.0	.0	.0	.0	.0	.0	.0	.0
80. *	.0	.0	.0	.0	.0	.0	.0	.0
85. *	.0	.0	.0	.0	.0	.0	.0	.0
90. *	.0	.0	.0	.0	.0	.0	.0	.0
95. *	.0	.0	.0	.0	.0	.0	.0	.0
100. *	.0	.0	.0	.0	.0	.0	.0	.0
105. *	.0	.0	.0	.0	.0	.0	.0	.0
110. *	.0	.0	.0	.0	.0	.0	.0	.0
115. *	.0	.0	.0	.0	.0	.0	.0	.0
120. *	.0	.0	.0	.0	.0	.0	.0	.0
125. *	.0	.0	.0	.0	.0	.0	.0	.0
130. *	.0	.0	.0	.0	.0	.0	.0	.0
135. *	.0	.0	.0	.0	.0	.0	.0	.0
140. *	.0	.0	.0	.0	.0	.0	.0	.0
145. *	.0	.0	.0	.0	.0	.0	.0	.0
150. *	.0	.0	.0	.0	.0	.0	.0	.0
155. *	.0	.0	.0	.0	.0	.0	.0	.0
160. *	.0	.0	.0	.0	.0	.0	.0	.0
165. *	.0	.0	.0	.0	.0	.0	.0	.0
170. *	.0	.0	.0	.0	.0	.0	.0	.0
175. *	.0	.0	.0	.0	.0	.0	.0	.0
180. *	.0	.0	.0	.0	.0	.0	.0	.0
185. *	.0	.0	.0	.0	.0	.0	.0	.0
190. *	.0	.0	.0	.0	.0	.0	.0	.0
195. *	.0	.0	.0	.0	.0	.0	.0	.0
200. *	.0	.0	.0	.0	.0	.0	.0	.0
205. *	.1	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 1 26th & Wilshire (S1B5AM.DAT) RUN: Site 1 Build Alt5 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.1	.0	.0	.0	.0	.0	.0	.0
215. *	.0	.0	.0	.0	.0	.0	.0	.0
220. *	.0	.0	.0	.0	.0	.0	.0	.0
225. *	.0	.0	.0	.0	.0	.0	.0	.0
230. *	.0	.0	.0	.0	.0	.0	.0	.0
235. *	.0	.1	.1	.0	.0	.0	.0	.0
240. *	.0	.1	.1	.0	.0	.0	.0	.0
245. *	.0	.0	.0	.0	.0	.0	.0	.0
250. *	.0	.0	.0	.0	.0	.0	.0	.0
255. *	.0	.0	.0	.0	.0	.0	.0	.0
260. *	.0	.0	.0	.0	.0	.0	.0	.0
265. *	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.1	.1	.1	.0	.0	.0	.0	.0
DEGR. *	205	235	235	0	0	0	0	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 60 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 60 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 150 DEGREES FROM REC1 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 1 26th & Wilshire (S1B5PM.DAT) RUN: Site 1 Build Alt5 PM
DATE: 03/19/2010 TIME: 08:43:42.60

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	*	-15.0	139.0	583.0	699.0	*	819.	47.	AG	1492.	.8	.0	44.0		
2.	EB Wil T+R	*	584.0	699.0	715.0	824.0	*	181.	46.	AG	1405.	.8	.0	44.0		
3.	EB Wil T+R Q	*	672.0	783.0	-4056.1	-3778.3	*	6570.	226.	AG	14.	100.0	.0	24.0	7.55	333.7
4.	EB Wil LT	*	569.0	717.0	698.0	843.0	*	180.	46.	AG	87.	.8	.0	32.0		
5.	EB Wil LT Q	*	654.0	800.0	421.0	572.8	*	325.	226.	AG	6.	100.0	.0	12.0	1.40	16.5
6.	EB Wil DP	*	715.0	824.0	1421.0	1528.0	*	997.	45.	AG	1722.	.8	.0	44.0		
7.	WB Wil AP	*	1393.0	1557.0	810.0	982.0	*	819.	225.	AG	1720.	.8	.0	44.0		
8.	WB Wil T+R	*	806.0	986.0	684.0	868.0	*	170.	226.	AG	1593.	.8	.0	56.0		
9.	WB Wil T+R Q	*	717.0	900.0	4325.9	4425.0	*	5045.	46.	AG	20.	100.0	.0	36.0	7.93	256.3
10.	WB Wil LT	*	824.0	966.0	707.0	850.0	*	165.	225.	AG	127.	.8	.0	32.0		
11.	WB Wil LT Q	*	737.0	880.0	1247.7	1390.7	*	722.	45.	AG	6.	100.0	.0	12.0	1.95	36.7
12.	WB Wil DP	*	687.0	864.0	-35.0	163.0	*	1006.	226.	AG	1718.	.8	.0	44.0		
13.	SB 26 AP	*	553.0	971.0	-6.0	1547.0	*	803.	316.	AG	846.	.8	.0	32.0		
14.	SB 26 T+R	*	549.0	968.0	670.0	841.0	*	175.	136.	AG	677.	.8	.0	44.0		
15.	SB 26 T+R Q	*	633.0	880.0	-1467.6	3083.0	*	3044.	316.	AG	14.	100.0	.0	24.0	5.54	154.6
16.	SB 26 LT	*	563.0	978.0	679.0	856.0	*	168.	136.	AG	169.	.8	.0	32.0		
17.	SB 26 LT Q	*	645.0	891.0	-152.7	1738.5	*	1164.	317.	AG	6.	100.0	.0	12.0	2.56	59.1
18.	SB 26 DP	*	672.0	845.0	1384.0	114.0	*	1020.	136.	AG	778.	.8	.0	32.0		
19.	NB 26 AP	*	829.0	716.0	1410.0	138.0	*	820.	135.	AG	930.	.8	.0	32.0		
20.	NB 26 T+R	*	832.0	719.0	715.0	846.0	*	173.	317.	AG	834.	.8	.0	44.0		
21.	NB 26 T+R Q	*	759.0	798.0	3408.0	-2078.0	*	3910.	137.	AG	14.	100.0	.0	24.0	6.95	198.6
22.	NB 26 L	*	818.0	710.0	705.0	832.0	*	166.	317.	AG	96.	.8	.0	32.0		
23.	NB 26 L Q	*	747.0	787.0	1019.5	491.2	*	402.	137.	AG	7.	100.0	.0	12.0	1.50	20.4
24.	NB 26 DP	*	712.0	843.0	13.0	1565.0	*	1005.	316.	AG	770.	.8	.0	32.0		

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JOB: Site 1 26th & Wilshire (S1B5PM.DAT) RUN: Site 1 Build Alt5 PM
DATE: 03/19/2010 TIME: 08:43:42.60

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Wil T+R Q	*	90	57	2.0	1405	289	4.10	1	3
5.	EB Wil LT Q	*	90	53	2.0	87	171	4.10	1	3
9.	WB Wil T+R Q	*	90	55	2.0	1593	196	4.10	1	3
11.	WB Wil LT Q	*	90	50	2.0	127	164	4.10	1	3
15.	SB 26 T+R Q	*	90	57	2.0	677	190	4.10	1	3
17.	SB 26 LT Q	*	90	52	2.0	169	175	4.10	1	3
21.	NB 26 T+R Q	*	90	58	2.0	834	193	4.10	1	3
23.	NB 26 L Q	*	90	54	2.0	96	180	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	967.0	615.0	5.0	*
2.	SE 164 S	*	874.0	710.0	5.0	*
3.	SE 82 S	*	816.0	771.0	5.0	*
4.	SE CNR	*	768.0	826.0	5.0	*
5.	SE 82 E	*	819.0	886.0	5.0	*
6.	SE 164 E	*	877.0	944.0	5.0	*
7.	SE MID E	*	996.0	1059.0	5.0	*
8.	NE MID E	*	916.0	1134.0	5.0	*
9.	NE 164 E	*	800.0	1020.0	5.0	*
10.	NE 82 E	*	741.0	962.0	5.0	*
11.	NE CNR	*	680.0	915.0	5.0	*
12.	NE 82 N	*	628.0	964.0	5.0	*
13.	NE 164 N	*	570.0	1023.0	5.0	*
14.	NE MID N	*	454.0	1143.0	5.0	*
15.	NW MID N	*	391.0	1100.0	5.0	*
16.	NW 164 N	*	514.0	974.0	5.0	*
17.	NW 82 N	*	571.0	914.0	5.0	*
18.	NW CNR	*	621.0	855.0	5.0	*
19.	NW 82 W	*	570.0	797.0	5.0	*
20.	NW 164 W	*	512.0	740.0	5.0	*
21.	NW MID W	*	412.0	643.0	5.0	*
22.	SW MID W	*	484.0	558.0	5.0	*
23.	SW 164 W	*	589.0	658.0	5.0	*
24.	SW 82 W	*	649.0	715.0	5.0	*
25.	SW CNR	*	707.0	765.0	5.0	*
26.	SW 82 S	*	763.0	714.0	5.0	*
27.	SW 164 S	*	820.0	656.0	5.0	*
28.	SW MID S	*	919.0	554.0	5.0	*

1 PAGE 3

JOB: Site 1 26th & Wilshire (S1B5PM.DAT) RUN: Site 1 Build Alt5 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5.	* .0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10.	* .0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	* .0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	* .0	.0	.0	.0	.1	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
55.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0
60.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
75.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
80.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
85.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
90.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
95.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
100.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
105.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
110.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
115.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
120.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
125.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
130.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
135.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
140.	* .0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
145.	* .1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
150.	* .1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
155.	* .1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
160.	* .0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
165.	* .0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
170.	* .0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
175.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
180.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
200.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
205.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1

1

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
215.	* .0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
220.	* .0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
225.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	* .0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	* .0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	* .0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	* .0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	* .0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0
320.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
325.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
330.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
335.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
340.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
360.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX	* .1	.1	.1	.1	.1	.1	.1	.2	.2	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.1
DEGR.	* 145	140	140	20	5	5	10	55	55	40	45	0	0	0	105	100	320	50	195	195

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.1	.0	.0	.0	.0	.0	.0	.0
65.	.1	.0	.0	.0	.0	.0	.0	.0
70.	.1	.0	.0	.0	.0	.0	.0	.0
75.	.1	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0
180.	.0	.0	.0	.0	.0	.0	.0	.0
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 1 26th & Wilshire (S1B5PM.DAT) RUN: Site 1 Build Alt5 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0
MAX DEGR.	.1 60	.0 0	.0 0	.0 0	.0 0	.0 0	.0 0	.0 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 55 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 55 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 145 DEGREES FROM REC1 .

Site 1

Existing with Project

Input & Output Files

```
Site 1 26th & Wilshire (S1EXWPAM.DAT)   60.0321.0.0000.000280.30480000
1    1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Existing WITH PROJ AM            24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1111 3.3  0.  44
30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1071 3.3  0.  44
30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.       0.  24   2
       90        58       2.0 1071   20.5 1287 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 3.3  0.  32
30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.       0.  12   1
       90        55       2.0   40   20.5  180 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1198 3.3  0.  44
30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1302 3.3  0.  44
30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1181 3.3  0.  56
30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.       0.  36   3
       90        56       2.0 1181   20.5 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 3.3  0.  32
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30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
        90        50       2.0  121   20.5  168 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1248 3.3  0.  44
30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     723 3.3  0.  32
30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     591 3.3  0.  44
30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  591   20.5 1242 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     132 3.3  0.  32
30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  132   20.5  336 1 3
  1
SB        26 LT     AG   672.   845.  1384.   114.     688 3.3  0.  32
30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     563 3.3  0.  32
30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     485 3.3  0.  44
30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  485   20.5 1245 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 3.3  0.  32
30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        53       2.0   78   20.5  252 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     565 3.3  0.  32
30.
1.0   04 1000.   0Y  5  0 72
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1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 1 26th & Wilshire (S1EXWPAM.DAT) RUN: Site 1 Existing WITH PROJ AM
DATE: 07/12/2011 TIME: 14:43:26.06

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-15.0	139.0	583.0	699.0	819.	47.	AG	1111.	3.3	.0	44.0		
2.	EB Wil T+R	584.0	699.0	715.0	824.0	181.	46.	AG	1071.	3.3	.0	44.0		
3.	EB Wil T+R Q	672.0	783.0	-500.4	-348.0	1629.	226.	AG	71.	100.0	.0	24.0	1.34	82.8
4.	EB Wil LT	569.0	717.0	698.0	843.0	180.	46.	AG	40.	3.3	.0	32.0		
5.	EB Wil LT Q	654.0	800.0	643.5	789.8	15.	226.	AG	34.	100.0	.0	12.0	.65	.7
6.	EB Wil DP	715.0	824.0	1421.0	1528.0	997.	45.	AG	1198.	3.3	.0	44.0		
7.	WB Wil AP	1393.0	1557.0	810.0	982.0	819.	225.	AG	1302.	3.3	.0	44.0		
8.	WB Wil T+R	806.0	986.0	684.0	868.0	170.	226.	AG	1181.	3.3	.0	56.0		
9.	WB Wil T+R Q	717.0	900.0	868.0	1047.5	211.	46.	AG	103.	100.0	.0	36.0	.99	10.7
10.	WB Wil LT	824.0	966.0	707.0	850.0	165.	225.	AG	121.	3.3	.0	32.0		
11.	WB Wil LT Q	737.0	880.0	1187.5	1330.5	637.	45.	AG	31.	100.0	.0	12.0	1.81	32.4
12.	WB Wil DP	687.0	864.0	-35.0	163.0	1006.	226.	AG	1248.	3.3	.0	44.0		
13.	SB 26 AP	553.0	971.0	-6.0	1547.0	803.	316.	AG	723.	3.3	.0	32.0		
14.	SB 26 T+R	549.0	968.0	670.0	841.0	175.	136.	AG	591.	3.3	.0	44.0		
15.	SB 26 T+R Q	633.0	880.0	570.0	946.1	91.	316.	AG	68.	100.0	.0	24.0	.71	4.6
16.	SB 26 LT	563.0	978.0	679.0	856.0	168.	136.	AG	132.	3.3	.0	32.0		
17.	SB 26 LT Q	645.0	891.0	585.1	954.6	87.	317.	AG	31.	100.0	.0	12.0	.99	4.4
18.	SB 26 LT	672.0	845.0	1384.0	114.0	1020.	136.	AG	688.	3.3	.0	32.0		
19.	NB 26 AP	829.0	716.0	1410.0	138.0	820.	135.	AG	563.	3.3	.0	32.0		
20.	NB 26 T+R	832.0	719.0	715.0	846.0	173.	317.	AG	485.	3.3	.0	44.0		
21.	NB 26 T+R Q	759.0	798.0	810.1	742.5	75.	137.	AG	70.	100.0	.0	24.0	.60	3.8
22.	NB 26 L	818.0	710.0	705.0	832.0	166.	317.	AG	78.	3.3	.0	32.0		
23.	NB 26 L Q	747.0	787.0	773.7	758.0	39.	137.	AG	32.	100.0	.0	12.0	.85	2.0
24.	NB 26 DP	712.0	843.0	13.0	1565.0	1005.	316.	AG	565.	3.3	.0	32.0		

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JOB: Site 1 26th & Wilshire (S1EXWPAM.DAT) RUN: Site 1 Existing WITH PROJ AM
DATE: 07/12/2011 TIME: 14:43:26.06

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Wil T+R Q	90	58	2.0	1071	1287	20.50	1	3
5.	EB Wil LT Q	90	55	2.0	40	180	20.50	1	3
9.	WB Wil T+R Q	90	56	2.0	1181	1190	20.50	1	3
11.	WB Wil LT Q	90	50	2.0	121	168	20.50	1	3
15.	SB 26 T+R Q	90	56	2.0	591	1242	20.50	1	3
17.	SB 26 LT Q	90	50	2.0	132	336	20.50	1	3
21.	NB 26 T+R Q	90	57	2.0	485	1245	20.50	1	3
23.	NB 26 L Q	90	53	2.0	78	252	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	967.0	615.0	5.0
2.	SE 164 S	874.0	710.0	5.0
3.	SE 82 S	816.0	771.0	5.0
4.	SE CNR	768.0	826.0	5.0
5.	SE 82 E	819.0	886.0	5.0
6.	SE 164 E	877.0	944.0	5.0
7.	SE MID E	996.0	1059.0	5.0
8.	NE MID E	916.0	1134.0	5.0
9.	NE 164 E	800.0	1020.0	5.0
10.	NE 82 E	741.0	962.0	5.0
11.	NE CNR	680.0	915.0	5.0
12.	NE 82 N	628.0	964.0	5.0
13.	NE 164 N	570.0	1023.0	5.0
14.	NE MID N	454.0	1143.0	5.0
15.	NW MID N	391.0	1100.0	5.0
16.	NW 164 N	514.0	974.0	5.0
17.	NW 82 N	571.0	914.0	5.0
18.	NW CNR	621.0	855.0	5.0
19.	NW 82 W	570.0	797.0	5.0
20.	NW 164 W	512.0	740.0	5.0
21.	NW MID W	412.0	643.0	5.0
22.	SW MID W	484.0	558.0	5.0
23.	SW 164 W	589.0	658.0	5.0
24.	SW 82 W	649.0	715.0	5.0
25.	SW CNR	707.0	765.0	5.0
26.	SW 82 S	763.0	714.0	5.0
27.	SW 164 S	820.0	656.0	5.0
28.	SW MID S	919.0	554.0	5.0

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JOB: Site 1 26th & Wilshire (S1EXWPAM.DAT) RUN: Site 1 Existing WITH PROJ AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.2	.4	.2	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
5.	.0	.0	.2	.4	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.0
10.	.0	.0	.2	.2	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
15.	.0	.0	.1	.2	.5	.3	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
20.	.0	.0	.1	.3	.5	.4	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
25.	.0	.0	.1	.4	.5	.4	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.1	.0
30.	.0	.0	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.2	.0	.0
35.	.0	.0	.1	.2	.3	.3	.3	.1	.1	.2	.1	.0	.0	.0	.1	.1	.3	.3	.0	.0
40.	.0	.0	.0	.2	.3	.3	.2	.1	.1	.3	.1	.0	.0	.0	.1	.1	.3	.2	.1	.0
45.	.0	.0	.0	.1	.1	.1	.1	.1	.2	.4	.3	.0	.0	.0	.1	.1	.3	.3	.1	.2
50.	.0	.0	.0	.1	.1	.1	.1	.1	.3	.5	.5	.0	.0	.0	.1	.1	.3	.5	.3	.2
55.	.0	.0	.0	.1	.1	.1	.1	.3	.5	.6	.5	.0	.0	.0	.1	.1	.3	.5	.3	.3
60.	.0	.0	.0	.0	.0	.0	.0	.3	.5	.6	.6	.1	.0	.0	.1	.1	.4	.4	.3	.2
65.	.0	.0	.0	.0	.0	.0	.0	.3	.5	.8	.6	.2	.0	.0	.1	.1	.4	.4	.3	.1
70.	.0	.0	.0	.0	.0	.0	.0	.3	.7	.8	.5	.2	.0	.0	.1	.1	.4	.4	.2	.1
75.	.0	.0	.0	.0	.0	.0	.0	.3	.6	.7	.5	.1	.0	.0	.1	.1	.4	.5	.1	.3
80.	.0	.0	.0	.0	.0	.0	.0	.3	.6	.7	.5	.1	.0	.0	.1	.2	.4	.5	.1	.3
85.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.6	.5	.1	.0	.0	.1	.2	.4	.3	.1	.3
90.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.1	.1	.0	.1	.1	.4	.3	.1	.3
95.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.1	.1	.0	.1	.1	.4	.2	.2	.3
100.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.1	.1	.3	.2	.3	.2
105.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.1	.2	.3	.1	.3	.2
110.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.3	.2	.3	.2
115.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.3	.2	.3	.2
120.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.3	.2	.3	.2
125.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.2	.2	.3	.2
130.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.2	.1	.0	.0	.1	.2	.2	.2	.3	.2
135.	.1	.1	.0	.1	.0	.0	.0	.2	.5	.5	.2	.0	.0	.1	.0	.2	.2	.3	.3	.2
140.	.1	.1	.1	.1	.0	.0	.0	.2	.5	.5	.2	.0	.1	.1	.0	.1	.1	.2	.3	.3
145.	.1	.2	.2	.2	.0	.0	.0	.2	.5	.5	.2	.1	.1	.1	.0	.0	.1	.2	.3	.3
150.	.2	.2	.2	.3	.0	.0	.0	.2	.5	.5	.2	.1	.2	.1	.0	.0	.1	.3	.3	.3
155.	.2	.2	.1	.3	.0	.0	.0	.2	.5	.5	.2	.1	.2	.1	.0	.0	.0	.3	.2	.3
160.	.2	.2	.1	.4	.0	.0	.0	.2	.5	.5	.2	.1	.2	.1	.0	.0	.2	.3	.2	.3
165.	.2	.2	.1	.4	.0	.0	.0	.2	.6	.5	.2	.1	.2	.2	.0	.0	.2	.3	.2	.3
170.	.2	.2	.1	.4	.0	.0	.0	.2	.6	.5	.2	.2	.2	.2	.0	.0	.2	.3	.2	.3
175.	.2	.2	.3	.3	.0	.0	.0	.2	.5	.5	.3	.3	.2	.2	.0	.0	.2	.2	.2	.3
180.	.1	.2	.2	.3	.0	.0	.0	.2	.5	.5	.3	.4	.2	.2	.0	.0	.2	.2	.2	.3
185.	.1	.1	.2	.2	.0	.0	.0	.2	.6	.4	.5	.4	.2	.2	.0	.1	.2	.2	.2	.3
190.	.1	.1	.2	.2	.1	.0	.0	.2	.6	.4	.3	.4	.2	.1	.0	.1	.2	.2	.3	.3
195.	.1	.1	.2	.2	.1	.0	.0	.3	.6	.4	.3	.4	.2	.1	.0	.1	.2	.2	.4	.4
200.	.1	.1	.2	.2	.1	.0	.0	.3	.5	.5	.3	.4	.2	.1	.0	.1	.2	.2	.4	.4
205.	.1	.1	.1	.1	.1	.0	.0	.3	.4	.5	.3	.4	.2	.1	.0	.1	.2	.3	.4	.4

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.2	.1	.0	.0	.0	.3	.5	.5	.3	.4	.2	.1	.0	.0	.2	.3	.4	.4
215.	.1	.1	.3	.1	.1	.0	.0	.4	.6	.5	.3	.4	.1	.1	.0	.0	.2	.3	.4	.4
220.	.1	.1	.3	.2	.1	.2	.1	.3	.5	.4	.3	.3	.1	.1	.0	.0	.1	.2	.4	.4
225.	.1	.1	.4	.2	.2	.2	.2	.3	.5	.4	.3	.2	.1	.1	.0	.0	.0	.2	.2	.2
230.	.1	.1	.4	.5	.3	.3	.3	.1	.4	.3	.3	.2	.1	.1	.0	.0	.0	.2	.2	.2
235.	.1	.2	.4	.5	.3	.3	.2	.1	.2	.2	.3	.2	.1	.1	.0	.0	.0	.1	.1	.1
240.	.1	.2	.4	.3	.3	.3	.3	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
245.	.1	.1	.4	.3	.3	.3	.3	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
250.	.1	.1	.4	.3	.2	.4	.4	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
255.	.1	.1	.4	.3	.2	.4	.3	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
260.	.1	.1	.4	.3	.1	.3	.3	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0
265.	.1	.1	.4	.4	.1	.3	.3	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
270.	.1	.1	.4	.3	.3	.3	.3	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
275.	.2	.1	.3	.2	.3	.4	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
280.	.2	.1	.3	.2	.3	.4	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
285.	.2	.1	.3	.1	.3	.4	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
290.	.2	.1	.3	.1	.3	.3	.2	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.0	.0	.0
295.	.2	.1	.2	.1	.3	.3	.2	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0
300.	.1	.1	.2	.2	.3	.3	.2	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0
305.	.1	.1	.2	.2	.3	.3	.2	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0
310.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.1	.2	.2	.1	.0	.1	.0	.0	.0	.0
315.	.0	.1	.0	.3	.4	.4	.2	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.0	.0
320.	.0	.0	.0	.3	.4	.4	.2	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.2	.0	.0
325.	.0	.0	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0
330.	.0	.1	.2	.3	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0
335.	.0	.1	.2	.3	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.3	.0	.0
340.	.0	.1	.2	.3	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
345.	.0	.1	.2	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
350.	.0	.1	.2	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
355.	.0	.0	.2	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
360.	.0	.0	.2	.4	.2	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.3	.0	.0
MAX	.2	.2	.4	.5	.5	.4	.4	.4	.7	.8	.6	.4	.2	.2	.1	.2	.4	.5	.4	.4
DEGR.	150	145	225	230	15	20	250	215	70	65	60	180	150	165	0	80	60	50	195	195

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR) * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.4	.4	.4	.3	.4	.2	.1
5. *	.0	.4	.4	.3	.5	.4	.1	.1
10. *	.0	.4	.4	.2	.5	.4	.1	.1
15. *	.0	.4	.4	.3	.5	.4	.1	.1
20. *	.0	.4	.4	.3	.3	.4	.1	.1
25. *	.0	.4	.3	.4	.3	.3	.1	.1
30. *	.0	.4	.3	.4	.3	.3	.1	.1
35. *	.0	.3	.4	.3	.4	.3	.1	.1
40. *	.1	.3	.3	.3	.2	.2	.1	.1
45. *	.1	.2	.3	.1	.2	.2	.1	.1
50. *	.1	.1	.0	.1	.2	.2	.1	.1
55. *	.1	.1	.0	.0	.2	.2	.1	.1
60. *	.3	.0	.0	.0	.2	.2	.1	.1
65. *	.3	.0	.0	.0	.2	.1	.1	.1
70. *	.3	.0	.0	.0	.2	.1	.1	.1
75. *	.3	.0	.0	.0	.2	.1	.1	.1
80. *	.3	.0	.0	.0	.2	.1	.1	.1
85. *	.3	.0	.0	.0	.2	.1	.1	.1
90. *	.3	.0	.0	.0	.2	.1	.1	.1
95. *	.3	.0	.0	.0	.2	.1	.1	.1
100. *	.3	.0	.0	.0	.2	.1	.1	.1
105. *	.3	.0	.0	.0	.2	.1	.1	.1
110. *	.3	.0	.0	.0	.1	.1	.1	.1
115. *	.3	.0	.0	.0	.1	.1	.1	.1
120. *	.3	.0	.0	.0	.1	.1	.1	.1
125. *	.3	.0	.0	.0	.1	.1	.1	.1
130. *	.3	.0	.0	.0	.1	.1	.1	.1
135. *	.3	.0	.0	.0	.1	.1	.1	.1
140. *	.3	.0	.0	.0	.0	.1	.1	.1
145. *	.3	.0	.0	.0	.0	.0	.0	.0
150. *	.3	.0	.0	.0	.0	.0	.0	.0
155. *	.3	.0	.0	.0	.0	.0	.0	.0
160. *	.3	.0	.0	.0	.0	.0	.0	.0
165. *	.3	.0	.0	.0	.0	.0	.0	.0
170. *	.3	.0	.0	.0	.0	.0	.0	.0
175. *	.3	.0	.0	.0	.0	.0	.0	.0
180. *	.3	.0	.0	.0	.0	.0	.0	.0
185. *	.3	.0	.0	.0	.0	.0	.0	.0
190. *	.3	.0	.0	.0	.0	.0	.0	.0
195. *	.4	.0	.0	.0	.0	.0	.0	.0
200. *	.4	.0	.0	.0	.0	.0	.0	.0
205. *	.4	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.4	.0	.0	.0	.0	.0	.0	.0
215. *	.4	.1	.1	.1	.1	.0	.0	.0
220. *	.3	.2	.2	.2	.1	.0	.0	.0
225. *	.2	.3	.3	.3	.3	.1	.0	.0
230. *	.2	.3	.4	.4	.4	.1	.0	.0
235. *	.1	.4	.4	.4	.5	.1	.1	.0
240. *	.0	.4	.4	.4	.5	.1	.1	.0
245. *	.0	.4	.5	.5	.5	.2	.1	.0
250. *	.0	.4	.4	.5	.4	.1	.1	.0
255. *	.0	.4	.4	.5	.4	.1	.1	.0
260. *	.0	.4	.4	.5	.4	.1	.1	.0
265. *	.0	.4	.4	.4	.4	.1	.1	.0
270. *	.0	.4	.4	.4	.4	.1	.1	.0
275. *	.0	.4	.4	.4	.3	.1	.1	.0
280. *	.0	.4	.4	.4	.3	.1	.1	.0
285. *	.0	.4	.4	.4	.3	.1	.1	.0
290. *	.0	.4	.4	.4	.3	.1	.0	.0
295. *	.0	.4	.4	.4	.3	.1	.0	.0
300. *	.0	.4	.4	.4	.3	.0	.0	.0
305. *	.0	.4	.4	.4	.3	.0	.0	.0
310. *	.0	.4	.4	.4	.2	.0	.0	.0
315. *	.0	.4	.4	.4	.2	.0	.0	.1
320. *	.0	.4	.4	.4	.2	.0	.1	.1
325. *	.0	.4	.4	.4	.2	.1	.1	.1
330. *	.0	.4	.4	.4	.2	.1	.1	.1
335. *	.0	.4	.4	.4	.2	.1	.2	.1
340. *	.0	.4	.4	.4	.2	.1	.2	.1
345. *	.0	.4	.4	.4	.2	.1	.2	.1
350. *	.0	.4	.4	.4	.2	.2	.3	.1
355. *	.0	.4	.5	.4	.2	.3	.3	.1
360. *	.0	.4	.4	.4	.3	.4	.2	.1
MAX *	.4	.4	.5	.5	.5	.4	.3	.1
DEGR. *	195	0	245	245	5	0	350	0

THE HIGHEST CONCENTRATION IS .80 PPM AT 65 DEGREES FROM REC10.
THE 2ND HIGHEST CONCENTRATION IS .70 PPM AT 70 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .60 PPM AT 60 DEGREES FROM REC11.

```
Site 1 26th & Wilshire (S1EXWPPM.DAT)   60.0321.0.0000.000280.30480000
1    1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Existing WITH PROJ PM            24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1229 3.3  0.  44
30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1142 3.3  0.  44
30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.       0.  24   2
       90        59       2.0 1142   20.5 1285 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 3.3  0.  32
30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.       0.  12   1
       90        54       2.0   87   20.5  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1326 3.3  0.  44
30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1384 3.3  0.  44
30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1181 3.3  0.  56
30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.       0.  36   3
       90        57       2.0 1181   20.5 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 3.3  0.  32
```

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30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
        90        52       2.0  127   20.5  176 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1479 3.3  0.  44
30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     694 3.3  0.  32
30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     555 3.3  0.  44
30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  555   20.5 1236 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     139 3.3  0.  32
30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  139   20.5  252 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     656 3.3  0.  32
30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     727 3.3  0.  32
30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     616 3.3  0.  44
30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  616   20.5 1239 1 3
  1
NB        26 L      AG   818.   710.   705.   832.     111 3.3  0.  32
30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0  111   20.5  358 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     700 3.3  0.  32
30.
1.0   04 1000.   0Y  5  0 72
```

JOB: Site 1 26th & Wilshire (S1EXWPPM.DAT) RUN: Site 1 Existing WITH PROJ PM
DATE: 07/12/2011 TIME: 14:43:51.82

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-15.0	139.0	583.0	699.0	819.	47.	AG	1229.	3.3	.0	44.0		
2.	EB Wil T+R	584.0	699.0	715.0	824.0	181.	46.	AG	1142.	3.3	.0	44.0		
3.	EB Wil T+R Q	672.0	783.0	-880.4	-714.6	2157.	226.	AG	72.	100.0	.0	24.0	1.48	109.6
4.	EB Wil LT	569.0	717.0	698.0	843.0	180.	46.	AG	87.	3.3	.0	32.0		
5.	EB Wil LT Q	654.0	800.0	435.3	586.8	305.	226.	AG	33.	100.0	.0	12.0	1.36	15.5
6.	EB Wil DP	715.0	824.0	1421.0	1528.0	997.	45.	AG	1326.	3.3	.0	44.0		
7.	WB Wil AP	1393.0	1557.0	810.0	982.0	819.	225.	AG	1384.	3.3	.0	44.0		
8.	WB Wil T+R	806.0	986.0	684.0	868.0	170.	226.	AG	1181.	3.3	.0	56.0		
9.	WB Wil T+R Q	717.0	900.0	930.9	1108.9	299.	46.	AG	104.	100.0	.0	36.0	1.02	15.2
10.	WB Wil LT	824.0	966.0	707.0	850.0	165.	225.	AG	127.	3.3	.0	32.0		
11.	WB Wil LT Q	737.0	880.0	1241.3	1384.3	713.	45.	AG	32.	100.0	.0	12.0	1.92	36.2
12.	WB Wil DP	687.0	864.0	-35.0	163.0	1006.	226.	AG	1479.	3.3	.0	44.0		
13.	SB 26 AP	553.0	971.0	-6.0	1547.0	803.	316.	AG	694.	3.3	.0	32.0		
14.	SB 26 T+R	549.0	968.0	670.0	841.0	175.	136.	AG	555.	3.3	.0	44.0		
15.	SB 26 T+R Q	633.0	880.0	574.5	941.4	85.	316.	AG	68.	100.0	.0	24.0	.67	4.3
16.	SB 26 LT	563.0	978.0	679.0	856.0	168.	136.	AG	139.	3.3	.0	32.0		
17.	SB 26 LT Q	645.0	891.0	309.2	1247.8	490.	317.	AG	31.	100.0	.0	12.0	1.39	24.9
18.	SB 26 DP	672.0	845.0	1384.0	114.0	1020.	136.	AG	656.	3.3	.0	32.0		
19.	NB 26 AP	829.0	716.0	1410.0	138.0	820.	135.	AG	727.	3.3	.0	32.0		
20.	NB 26 T+R	832.0	719.0	715.0	846.0	173.	317.	AG	616.	3.3	.0	44.0		
21.	NB 26 T+R Q	759.0	798.0	829.1	721.9	103.	137.	AG	70.	100.0	.0	24.0	.77	5.3
22.	NB 26 L	818.0	710.0	705.0	832.0	166.	317.	AG	111.	3.3	.0	32.0		
23.	NB 26 L Q	747.0	787.0	778.4	752.9	46.	137.	AG	32.	100.0	.0	12.0	.82	2.4
24.	NB 26 DP	712.0	843.0	13.0	1565.0	1005.	316.	AG	700.	3.3	.0	32.0		

1

JOB: Site 1 26th & Wilshire (S1EXWPPM.DAT) RUN: Site 1 Existing WITH PROJ PM
DATE: 07/12/2011 TIME: 14:43:51.82

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Wil T+R Q	90	59	2.0	1142	1285	20.50	1	3
5.	EB Wil LT Q	90	54	2.0	87	182	20.50	1	3
9.	WB Wil T+R Q	90	57	2.0	1181	1196	20.50	1	3
11.	WB Wil LT Q	90	52	2.0	127	176	20.50	1	3
15.	SB 26 T+R Q	90	56	2.0	555	1236	20.50	1	3
17.	SB 26 LT Q	90	50	2.0	139	252	20.50	1	3
21.	NB 26 T+R Q	90	57	2.0	616	1239	20.50	1	3
23.	NB 26 L Q	90	52	2.0	111	358	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	967.0	615.0	5.0
2.	SE 164 S	874.0	710.0	5.0
3.	SE 82 S	816.0	771.0	5.0
4.	SE CNR	768.0	826.0	5.0
5.	SE 82 E	819.0	886.0	5.0
6.	SE 164 E	877.0	944.0	5.0
7.	SE MID E	996.0	1059.0	5.0
8.	NE MID E	916.0	1134.0	5.0
9.	NE 164 E	800.0	1020.0	5.0
10.	NE 82 E	741.0	962.0	5.0
11.	NE CNR	680.0	915.0	5.0
12.	NE 82 N	628.0	964.0	5.0
13.	NE 164 N	570.0	1023.0	5.0
14.	NE MID N	454.0	1143.0	5.0
15.	NW MID N	391.0	1100.0	5.0
16.	NW 164 N	514.0	974.0	5.0
17.	NW 82 N	571.0	914.0	5.0
18.	NW CNR	621.0	855.0	5.0
19.	NW 82 W	570.0	797.0	5.0
20.	NW 164 W	512.0	740.0	5.0
21.	NW MID W	412.0	643.0	5.0
22.	SW MID W	484.0	558.0	5.0
23.	SW 164 W	589.0	658.0	5.0
24.	SW 82 W	649.0	715.0	5.0
25.	SW CNR	707.0	765.0	5.0
26.	SW 82 S	763.0	714.0	5.0
27.	SW 164 S	820.0	656.0	5.0
28.	SW MID S	919.0	554.0	5.0

1

JOB: Site 1 26th & Wilshire (S1EXWPPM.DAT) RUN: Site 1 Existing WITH PROJ PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.1	.2	.4	.5	.5	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.0	.0
5.	.0	.0	.2	.4	.5	.4	.3	.0	.0	.0	.0	.0	.0	.0	.2	.2	.3	.3	.0	.0
10.	.0	.0	.2	.3	.6	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
15.	.0	.0	.2	.4	.6	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
20.	.0	.0	.3	.5	.5	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.2	.4	.2	.1	.0
25.	.0	.0	.2	.5	.5	.5	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.4	.2	.1	.0
30.	.0	.0	.1	.4	.5	.4	.3	.0	.0	.1	.0	.0	.0	.0	.1	.1	.3	.2	.0	.0
35.	.0	.0	.1	.4	.4	.3	.3	.1	.2	.2	.1	.0	.0	.0	.1	.1	.3	.3	.1	.0
40.	.0	.0	.0	.3	.3	.3	.3	.1	.2	.4	.2	.0	.0	.0	.1	.1	.3	.2	.1	.2
45.	.0	.0	.0	.1	.3	.3	.1	.1	.3	.4	.4	.0	.0	.0	.1	.1	.3	.4	.2	.2
50.	.0	.0	.0	.1	.1	.1	.1	.2	.5	.6	.5	.0	.0	.0	.1	.1	.3	.6	.3	.3
55.	.0	.0	.0	.1	.1	.1	.1	.3	.6	.6	.6	.1	.0	.0	.1	.1	.4	.6	.3	.3
60.	.0	.0	.0	.0	.1	.1	.0	.3	.7	.8	.6	.2	.0	.0	.1	.1	.5	.5	.3	.4
65.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.8	.6	.2	.0	.0	.1	.1	.4	.4	.3	.2
70.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.8	.5	.3	.0	.0	.1	.1	.5	.5	.2	.2
75.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.8	.5	.2	.0	.0	.1	.3	.5	.5	.2	.4
80.	.0	.0	.0	.0	.0	.0	.0	.4	.8	.7	.5	.2	.1	.0	.1	.3	.4	.5	.2	.4
85.	.0	.0	.0	.0	.0	.0	.0	.3	.7	.6	.5	.1	.1	.0	.2	.3	.4	.3	.2	.4
90.	.0	.0	.0	.0	.0	.0	.0	.2	.6	.6	.4	.1	.1	.0	.2	.2	.4	.3	.3	.4
95.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.1	.1	.0	.3	.3	.4	.3	.3	.4
100.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.3	.3	.3	.1	.3	.3
105.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.1	.0	.3	.3	.3	.1	.3	.2
110.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.1	.3	.2	.3	.2	.3	.2
115.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.1	.3	.2	.3	.2	.3	.2
120.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.2	.2	.3	.2	.3	.2
125.	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.3	.2	.1	.0	.1	.2	.2	.2	.3	.2
130.	.1	.1	.0	.0	.0	.0	.0	.3	.5	.5	.2	.1	.0	.1	.1	.2	.3	.3	.3	.2
135.	.1	.1	.1	.1	.0	.0	.0	.3	.5	.5	.2	.0	.1	.1	.0	.1	.3	.3	.3	.3
140.	.1	.1	.1	.2	.0	.0	.0	.3	.5	.5	.2	.1	.1	.1	.0	.1	.2	.2	.3	.3
145.	.1	.1	.2	.2	.0	.0	.0	.3	.5	.5	.2	.1	.1	.2	.0	.0	.1	.2	.3	.3
150.	.2	.2	.3	.4	.0	.0	.0	.4	.5	.5	.2	.1	.1	.2	.0	.0	.1	.3	.3	.3
155.	.2	.2	.4	.4	.0	.0	.0	.4	.5	.5	.3	.1	.2	.2	.0	.0	.1	.3	.3	.3
160.	.2	.2	.4	.4	.0	.0	.0	.4	.5	.5	.2	.1	.3	.2	.0	.0	.2	.3	.2	.3
165.	.2	.2	.3	.3	.0	.0	.0	.4	.6	.5	.2	.2	.3	.2	.0	.0	.2	.3	.2	.3
170.	.2	.2	.4	.3	.0	.0	.0	.5	.6	.5	.3	.3	.3	.3	.0	.0	.2	.3	.2	.3
175.	.1	.1	.3	.3	.0	.0	.0	.5	.6	.5	.3	.3	.3	.3	.0	.0	.2	.3	.3	.4
180.	.1	.1	.3	.3	.1	.0	.0	.5	.5	.5	.4	.4	.2	.3	.0	.0	.2	.3	.3	.4
185.	.1	.1	.3	.2	.1	.0	.0	.5	.6	.5	.5	.4	.3	.2	.0	.1	.2	.2	.4	.4
190.	.1	.1	.3	.2	.1	.0	.0	.6	.6	.4	.4	.4	.3	.2	.0	.1	.2	.3	.4	.4
195.	.1	.1	.3	.2	.1	.0	.0	.7	.6	.4	.3	.4	.3	.2	.0	.1	.2	.3	.4	.4
200.	.1	.1	.3	.2	.1	.0	.0	.7	.6	.6	.3	.4	.3	.2	.0	.1	.2	.3	.4	.4
205.	.1	.1	.3	.2	.1	.0	.0	.6	.6	.5	.3	.4	.3	.2	.0	.1	.2	.4	.4	.4

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.3	.2	.0	.0	.0	.6	.6	.5	.4	.4	.2	.2	.0	.1	.2	.4	.4	.4
215.	.1	.1	.3	.2	.1	.1	.1	.6	.6	.5	.4	.4	.2	.2	.0	.0	.2	.4	.4	.4
220.	.1	.1	.3	.2	.1	.2	.2	.5	.5	.4	.3	.4	.2	.2	.0	.0	.1	.3	.4	.4
225.	.1	.1	.4	.3	.3	.3	.2	.5	.5	.4	.3	.2	.2	.2	.0	.0	.0	.2	.2	.2
230.	.1	.1	.4	.6	.3	.3	.3	.3	.4	.3	.3	.2	.2	.2	.0	.0	.0	.2	.2	.2
235.	.1	.2	.4	.6	.3	.3	.4	.1	.2	.2	.3	.2	.2	.2	.0	.0	.0	.1	.1	.1
240.	.1	.2	.5	.4	.3	.4	.3	.1	.0	.0	.2	.2	.1	.2	.0	.0	.0	.0	.0	.0
245.	.1	.2	.5	.4	.3	.4	.3	.0	.0	.0	.2	.2	.1	.2	.0	.0	.0	.0	.0	.0
250.	.1	.2	.5	.4	.2	.4	.5	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0
255.	.1	.2	.5	.5	.3	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
260.	.1	.2	.5	.4	.2	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
265.	.1	.2	.5	.4	.2	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
270.	.1	.2	.5	.3	.3	.4	.4	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
275.	.1	.1	.4	.3	.3	.4	.4	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
280.	.1	.1	.4	.3	.3	.4	.4	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
285.	.2	.1	.3	.3	.3	.4	.3	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
290.	.2	.1	.3	.2	.3	.3	.3	.0	.0	.0	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
295.	.1	.2	.2	.3	.3	.3	.3	.0	.0	.0	.2	.3	.3	.3	.0	.0	.0	.0	.0	.0
300.	.1	.2	.2	.2	.3	.3	.3	.0	.0	.0	.2	.3	.3	.3	.0	.0	.0	.0	.0	.0
305.	.1	.2	.2	.2	.4	.3	.3	.0	.0	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0
310.	.1	.2	.2	.3	.4	.4	.3	.0	.0	.0	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0
315.	.0	.1	.1	.3	.4	.4	.3	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.0	.0
320.	.0	.1	.2	.4	.4	.4	.2	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.2	.0	.0
325.	.0	.0	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.3	.0	.0
330.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.2	.3	.4	.4	.0	.0
335.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.2	.3	.4	.5	.0	.0
340.	.0	.1	.2	.3	.4	.4	.2	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.5	.0	.0
345.	.0	.1	.2	.3	.3	.4	.2	.0	.0	.0	.0	.0	.0	.0	.2	.3	.4	.5	.0	.0
350.	.0	.1	.2	.3	.3	.4	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.5	.0	.0
355.	.0	.1	.2	.3	.3	.4	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.0	.0
360.	.0	.1	.2	.4	.5	.5	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.0	.0
MAX DEGR.	.2 150	.2 150	.5 240	.6 230	.6 10	.5 0	.5 250	.7 195	.8 65	.8 60	.6 55	.4 180	.3 160	.3 170	.3 0	.3 0	.5 60	.6 50	.4 185	.4 60

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR) | CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.4	.5	.4	.3	.4	.3	.2
5. *	.0	.4	.4	.4	.5	.4	.3	.1
10. *	.0	.5	.4	.3	.5	.4	.3	.1
15. *	.0	.5	.4	.3	.5	.4	.1	.1
20. *	.0	.4	.4	.3	.3	.4	.1	.1
25. *	.0	.4	.5	.4	.3	.4	.1	.1
30. *	.0	.4	.3	.4	.4	.3	.1	.1
35. *	.0	.4	.4	.3	.4	.3	.1	.1
40. *	.1	.3	.4	.3	.4	.2	.1	.1
45. *	.1	.2	.3	.2	.2	.2	.1	.1
50. *	.1	.1	.1	.1	.2	.2	.1	.1
55. *	.2	.1	.0	.0	.2	.2	.1	.1
60. *	.3	.0	.0	.0	.2	.2	.1	.1
65. *	.3	.0	.0	.0	.2	.2	.1	.1
70. *	.3	.0	.0	.0	.2	.2	.1	.1
75. *	.4	.0	.0	.0	.2	.2	.1	.1
80. *	.4	.0	.0	.0	.2	.2	.2	.1
85. *	.4	.0	.0	.0	.2	.2	.2	.2
90. *	.4	.0	.0	.0	.2	.1	.2	.2
95. *	.4	.0	.0	.0	.2	.1	.2	.2
100. *	.3	.0	.0	.0	.2	.1	.2	.2
105. *	.3	.0	.0	.0	.2	.1	.2	.2
110. *	.3	.0	.0	.0	.2	.2	.2	.2
115. *	.3	.0	.0	.0	.2	.2	.2	.2
120. *	.3	.0	.0	.0	.1	.2	.2	.2
125. *	.3	.0	.0	.0	.1	.2	.2	.2
130. *	.3	.0	.0	.0	.1	.2	.1	.1
135. *	.3	.0	.0	.0	.1	.1	.1	.1
140. *	.3	.0	.0	.0	.0	.1	.1	.1
145. *	.3	.0	.0	.0	.0	.0	.0	.0
150. *	.3	.0	.0	.0	.0	.0	.0	.0
155. *	.3	.0	.0	.0	.0	.0	.0	.0
160. *	.3	.0	.0	.0	.0	.0	.0	.0
165. *	.3	.0	.0	.0	.0	.0	.0	.0
170. *	.3	.0	.0	.0	.0	.0	.0	.0
175. *	.4	.0	.0	.0	.0	.0	.0	.0
180. *	.4	.0	.0	.0	.0	.0	.0	.0
185. *	.4	.0	.0	.0	.0	.0	.0	.0
190. *	.4	.0	.0	.0	.0	.0	.0	.0
195. *	.4	.0	.0	.0	.0	.0	.0	.0
200. *	.4	.0	.0	.0	.0	.0	.0	.0
205. *	.4	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 1 26th & Wilshire (S1EXWPPM.DAT) RUN: Site 1 Existing WITH PROJ PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210. *	.4	.0	.0	.0	.0	.0	.0	.0
215. *	.4	.1	.1	.1	.1	.0	.0	.0
220. *	.4	.2	.2	.2	.1	.0	.0	.0
225. *	.2	.3	.3	.3	.3	.1	.0	.0
230. *	.2	.4	.4	.4	.4	.1	.0	.0
235. *	.1	.4	.5	.4	.5	.1	.1	.0
240. *	.0	.5	.5	.4	.5	.2	.1	.0
245. *	.0	.5	.5	.5	.5	.3	.1	.0
250. *	.0	.5	.5	.5	.4	.3	.1	.0
255. *	.0	.4	.5	.5	.4	.2	.1	.0
260. *	.0	.4	.4	.5	.4	.2	.1	.0
265. *	.0	.4	.4	.4	.4	.2	.1	.0
270. *	.0	.4	.4	.4	.4	.2	.1	.0
275. *	.0	.4	.4	.4	.3	.2	.1	.0
280. *	.0	.4	.4	.4	.3	.2	.1	.0
285. *	.0	.4	.4	.4	.3	.2	.1	.0
290. *	.0	.4	.4	.4	.3	.2	.1	.0
295. *	.0	.4	.4	.4	.3	.1	.0	.0
300. *	.0	.4	.4	.4	.3	.1	.0	.0
305. *	.0	.4	.4	.4	.3	.0	.0	.0
310. *	.0	.4	.4	.4	.2	.0	.0	.0
315. *	.0	.4	.4	.4	.2	.0	.0	.1
320. *	.0	.4	.4	.4	.2	.0	.1	.1
325. *	.0	.4	.4	.4	.2	.1	.1	.1
330. *	.0	.4	.4	.4	.3	.1	.2	.1
335. *	.0	.4	.4	.4	.3	.1	.2	.1
340. *	.0	.4	.4	.4	.2	.1	.2	.1
345. *	.0	.4	.4	.4	.2	.1	.3	.1
350. *	.0	.4	.4	.4	.2	.2	.3	.2
355. *	.0	.4	.5	.4	.2	.4	.3	.2
360. *	.0	.4	.5	.4	.3	.4	.3	.2
MAX *	.4	.5	.5	.5	.5	.4	.3	.2
DEGR. *	75	10	0	245	5	0	0	0

THE HIGHEST CONCENTRATION IS .80 PPM AT 65 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 60 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .70 PPM AT 195 DEGREES FROM REC8 .

Site 2 – Veterans & Wilshire
Input Files

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Site 2 Veteran & Wilshire (S2EXAM.DAT)  60.0321.0.0000.000280.30480000
1    1
SE MID S                1066.      492.       5.0
SE 164 S                 942.      686.       5.0
SE 82 S                  892.      756.       5.0
SE CNR                   869.      821.       5.0
SE 82 E                  925.      853.       5.0
SE 164 E                1005.      880.       5.0
SE MID E                1219.      947.       5.0
NE MID E                1144.     1099.       5.0
NE 164 E                 918.     1026.       5.0
NE 82 E                  838.     1000.       5.0
NE CNR                   759.      983.       5.0
NE 82 N                  716.     1047.       5.0
NE 164 N                 676.     1120.       5.0
NE MID N                 595.     1269.       5.0
NW MID N                 464.     1209.       5.0
NW 164 N                 546.     1079.       5.0
NW 82 N                  589.     1010.       5.0
NW CNR                   611.      945.       5.0
NW 82 W                  552.      910.       5.0
NW 164 W                 475.      884.       5.0
NW MID W                 273.      815.       5.0
SW MID W                 305.      649.       5.0
SW 164 W                 565.      737.       5.0
SW 82 W                  645.      764.       5.0
SW CNR                   718.      779.       5.0
SW 82 S                  774.      718.       5.0
SW 164 S                 824.      646.       5.0
SW MID S                 957.      459.       5.0
Site 2 Existing AM                      27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    4350 3.3   0  68
30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    4350 3.3   0  68
30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3824 3.3   0  68
30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        56       2.0 3824   20.5  999 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     526 3.3   0  44
30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       118       2.0  526   20.5 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3918 3.3   0  68
30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    2511 3.3   0  68
30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    2443 3.3   0  68
30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
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      150        82       2.0 2443   20.5 1009 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      68 3.3   0  44
30.
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       142       2.0   68   20.5 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    2828 3.3   0  68
30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    2828 3.3   0  68
30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     992 3.5   0  32
30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     842 3.5   0  56
30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       111       2.0  842   20.5  964 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     150 3.5   0  32
30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       106       2.0  150   20.5  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1188 3.5   0  44
30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1188 3.5   0  44
30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.     440 3.5   0  44
30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     235 3.5   0  56
30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  235   20.5  829 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     205 3.5   0  44
30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  205   20.5  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     359 3.5   0  44
30.
1.0   04 1000.   0Y  5  0 72
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Site 2 Veteran & Wilshire (S2EXPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 Existing PM                       27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    2564 3.3   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    2564 3.3   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    2293 3.3   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
      150         60       2.0 2293   20.5  999 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     271 3.3   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
      150        126       2.0  271   20.5 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    2453 3.3   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    2853 3.3   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    2778 3.3   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
      150         77       2.0 2778   20.5 1010 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      75 3.3   0  44   30.
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  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   75   20.5 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3732 3.3   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3732 3.3   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1155 3.5   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     957 3.5   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       107       2.0  957   20.5  860 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     198 3.5   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       102       2.0  198   20.5  927 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.     984 3.5   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.     984 3.5   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1132 3.5   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     422 3.5   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       116       2.0  422   20.5  817 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     710 3.5   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        94       2.0  710   20.5  808 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     535 3.5   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2NBAM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 NO BUILD AM                        27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5619 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5619 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4678 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        57       2.0 4678   4.1  983 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     941 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       118       2.0  941   4.1  995 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4869 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3164 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3147 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
      150        82       2.0 3147   4.1 1084 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3437 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3437 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     946 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     814 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       111       2.0  814   4.1  875 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       106       2.0  132   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1787 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1787 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1155 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     833 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  833   4.1  852 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     322 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  322   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     791 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2NBPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 NO BUILD PM                        27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3358 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3358 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3073 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        68       2.0 3073   4.1  982 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     285 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       126       2.0  285   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3305 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4295 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4276 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
      150        85       2.0 4276   4.1  982 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      19 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   19   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4969 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4969 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1351 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1028 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150        97       2.0 1028   4.1  790 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     323 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150        95       2.0  323   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1719 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1719 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1987 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     858 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       109       2.0  858   4.1  810 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1129 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        87       2.0 1129   4.1  804 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     968 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B1AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT1 AM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5595 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5595 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4672 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
       150        59       2.0 4672   4.1  981 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     923 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
       150       118       2.0  923   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4826 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3179 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3160 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
       150        84       2.0 3160   4.1  997 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      19 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   19   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3487 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3487 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     959 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     827 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       109       2.0  827   4.1  877 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       104       2.0  132   4.1  885 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1751 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1751 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1151 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     820 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  820   4.1  858 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     331 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  331   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     817 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B1PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT1 PM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3430 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3430 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3138 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
       150        65       2.0 3138   4.1  984 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     292 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
       150       128       2.0  292   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3339 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4302 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4286 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
       150        82       2.0 4286   4.1  979 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      16 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   16   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4930 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4930 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1373 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1090 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       100       2.0 1090   4.1  782 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     283 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150        95       2.0  283   4.1  885 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1841 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1841 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1997 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     894 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       109       2.0  800   4.1  858 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1103 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0 1103   4.1  800 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     992 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B2AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT2 AM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5509 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5509 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4596 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        57       2.0 4596   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     913 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       118       2.0  913   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4761 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3138 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3121 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
      150        82       2.0 3121   4.1  995 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3409 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3409 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     947 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     815 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       111       2.0  815   4.1  888 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       106       2.0  132   4.1  967 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1755 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1755 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1085 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     767 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  767   4.1  852 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     318 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  318   4.1  837 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     751 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B2PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT2 PM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3358 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3358 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3074 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        70       2.0 3074   4.1  971 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     284 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       131       2.0  284   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3319 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4364 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4346 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 4346   4.1  981 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      18 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   18   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    5006 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    5006 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1384 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1053 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150        95       2.0 1053   4.1  784 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     331 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150        93       2.0  331   4.1  929 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1795 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1795 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    2004 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     886 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       109       2.0  886   4.1  812 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1118 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        89       2.0 1118   4.1  797 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     990 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B3AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT3 AM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5495 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5495 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4593 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
      150        57       2.0 4593   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     902 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
      150       118       2.0  902   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4799 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3158 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3142 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
      150        82       2.0 3142   4.1  995 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      16 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   16   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3429 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3429 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     932 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     800 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       108       2.0  800   4.1  885 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       106       2.0  132   4.1  959 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1754 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1754 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1134 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     795 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  795   4.1  853 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     339 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  339   4.1  859 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     737 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B3PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT3 PM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3401 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3401 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3112 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        68       2.0 3112   4.1  977 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     289 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       127       2.0  289   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3325 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4274 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4256 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        83       2.0 4256   4.1  982 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      18 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   18   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4918 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4918 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1362 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1091 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       100       2.0 1091   4.1  776 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     271 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150        95       2.0  271   4.1  933 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1792 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1792 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1983 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     912 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       109       2.0  912   4.1  800 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1074 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        88       2.0 1074   4.1  804 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     985 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B4AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT4 AM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5553 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5553 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4635 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        57       2.0 4635   4.1  968 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     918 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       118       2.0  918   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4832 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3177 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3161 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
      150        82       2.0 3161   4.1  994 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      16 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   16   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3438 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3438 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     949 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     817 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       111       2.0  817   4.1  859 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       106       2.0  132   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1787 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1787 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1182 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     853 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  853   4.1  834 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     329 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  329   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     807 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B4PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT4 PM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3310 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3310 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3031 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
      150        68       2.0 3031   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     279 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
      150       126       2.0  279   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3239 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4265 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4246 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
      150        85       2.0 4246   4.1  984 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      19 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   19   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    5001 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    5001 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1387 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1067 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       100       2.0 1067   4.1  782 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     320 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150        95       2.0  320   4.1  928 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1703 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1703 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1982 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     871 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       111       2.0  871   4.1  806 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1111 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        87       2.0 1111   4.1  804 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     999 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
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```
Site 2 Veteran & Wilshire (S2B5AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT5 AM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5547 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5547 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4619 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        57       2.0 4619   4.1  966 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     928 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       118       2.0  928   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4794 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3154 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3137 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
      150        81       2.0 3137   4.1  994 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
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  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3424 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3424 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     931 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     799 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       111       2.0  799   4.1  887 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       106       2.0  132   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1771 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1771 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1108 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     777 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  777   4.1  834 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     331 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  331   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     748 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
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Site 2 Veteran & Wilshire (S2B5PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  1066.      492.       5.0
SE 164 S                   942.      686.       5.0
SE 82 S                    892.      756.       5.0
SE CNR                     869.      821.       5.0
SE 82 E                    925.      853.       5.0
SE 164 E                  1005.      880.       5.0
SE MID E                  1219.      947.       5.0
NE MID E                  1144.     1099.       5.0
NE 164 E                   918.     1026.       5.0
NE 82 E                    838.     1000.       5.0
NE CNR                     759.      983.       5.0
NE 82 N                    716.     1047.       5.0
NE 164 N                   676.     1120.       5.0
NE MID N                   595.     1269.       5.0
NW MID N                   464.     1209.       5.0
NW 164 N                   546.     1079.       5.0
NW 82 N                    589.     1010.       5.0
NW CNR                     611.      945.       5.0
NW 82 W                    552.      910.       5.0
NW 164 W                   475.      884.       5.0
NW MID W                   273.      815.       5.0
SW MID W                   305.      649.       5.0
SW 164 W                   565.      737.       5.0
SW 82 W                    645.      764.       5.0
SW CNR                     718.      779.       5.0
SW 82 S                    774.      718.       5.0
SW 164 S                   824.      646.       5.0
SW MID S                   957.      459.       5.0
Site 2 BUILD ALT5 PM                    27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3396 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3396 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3109 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        71       2.0 3109   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     287 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       132       2.0  287   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3318 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4322 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4305 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
      150        82       2.0 4305   4.1  981 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
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  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4984 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4984 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1370 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1075 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150        97       2.0 1075   4.1  795 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     295 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150        92       2.0  295   4.1  929 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1793 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1793 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1986 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     876 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       108       2.0  876   4.1  812 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1110 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0 1110   4.1  794 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     979 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

Site 2 – Veterans & Wilshire
Output Files

JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT) RUN: Site 2 Existing AM
DATE: 07/12/2011 TIME: 15:40:48.13

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	4350.	3.3	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	4350.	3.3	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	3824.	3.3	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-3100.5	-481.3	3997.	251.	AG	82.	100.0	.0	48.0	1.60	203.0
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	526.	3.3	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-158.3	587.1	860.	252.	AG	87.	100.0	.0	24.0	1.30	43.7
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	3918.	3.3	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	2511.	3.3	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	2443.	3.3	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	2882.1	1612.9	2188.	72.	AG	120.	100.0	.0	48.0	1.42	111.2
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	68.	3.3	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	935.8	942.2	117.	73.	AG	104.	100.0	.0	24.0	1.21	5.9
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	2828.	3.3	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	2828.	3.3	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	992.	3.5	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	842.	3.5	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1279.0	113.0	812.	146.	AG	122.	100.0	.0	36.0	1.25	41.3
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	150.	3.5	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	896.3	719.4	87.	145.	AG	39.	100.0	.0	12.0	.59	4.4
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1188.	3.5	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1188.	3.5	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	440.	3.5	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	235.	3.5	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	652.0	1024.5	51.	328.	AG	132.	100.0	.0	36.0	.55	2.6
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	205.	3.5	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	616.5	1014.7	50.	328.	AG	66.	100.0	.0	24.0	.33	2.6
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	359.	3.5	.0	44.0		

1 PAGE 2

JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT) RUN: Site 2 Existing AM
DATE: 07/12/2011 TIME: 15:40:48.13

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	56	2.0	3824	999	20.50	1	3
6.	EB Wil LT Q	150	118	2.0	526	1084	20.50	1	3
10.	WB Wil T+R Q	150	82	2.0	2443	1009	20.50	1	3
12.	WB Wil LT Q	150	142	2.0	68	1084	20.50	1	3
17.	NB Vet T+LT Q	150	111	2.0	842	964	20.50	1	3
19.	NB Vet RT Q	150	106	2.0	150	955	20.50	1	3
24.	SB Vet T+LT Q	150	120	2.0	235	829	20.50	1	3
26.	SB Vet RT Q	150	90	2.0	205	834	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

1 PAGE 3

JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT) RUN: Site 2 Existing AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .2	.3	.5	.6	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
5.	* .2	.2	.5	.6	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
10.	* .2	.2	.5	.6	.7	.7	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
15.	* .2	.2	.4	.6	.7	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.3	.0	.0
20.	* .2	.2	.4	.6	.7	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.0	.0
25.	* .2	.3	.3	.6	.7	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.0	.0
30.	* .2	.3	.3	.8	.8	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.0	.0
35.	* .2	.3	.4	.7	.8	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.0	.0
40.	* .2	.3	.4	.8	.8	.8	.8	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.1	.0
45.	* .1	.3	.4	.7	.8	.8	.8	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.1	.0
50.	* .1	.2	.4	.7	.8	.8	.8	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.1	.0
55.	* .0	.2	.4	.7	.8	.9	.8	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.3	.1	.1
60.	* .0	.2	.4	.7	.8	.9	.8	.2	.2	.3	.1	.0	.0	.0	.1	.1	.1	.3	.3	.2
65.	* .0	.2	.2	.6	.8	.8	.8	.4	.4	.4	.4	.1	.0	.0	.1	.1	.3	.4	.3	.2
70.	* .0	.0	.2	.4	.6	.7	.5	.5	.6	.6	.6	.1	.0	.0	.1	.2	.4	.7	.5	.5
75.	* .0	.0	.1	.3	.4	.5	.4	.8	.8	.8	.7	.2	.1	.0	.1	.2	.4	.6	.7	.6
80.	* .0	.0	.0	.1	.2	.3	.2	.8	.9	.9	.8	.4	.1	.0	.2	.2	.7	.7	.6	.6
85.	* .0	.0	.0	.1	.2	.2	.1	.9	1.1	1.1	.9	.4	.3	.1	.2	.3	.8	.7	.7	.7
90.	* .0	.0	.0	.0	.1	.1	.1	1.0	1.1	1.1	.9	.5	.3	.1	.2	.4	.8	.7	.7	.7
95.	* .0	.0	.0	.0	.1	.1	.1	.9	.9	1.0	.9	.5	.3	.1	.2	.3	.7	.6	.7	.6
100.	* .0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.9	.4	.3	.2	.2	.4	.6	.7	.5	.6
105.	* .0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.9	.4	.2	.2	.2	.4	.6	.5	.5	.8
110.	* .0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.8	.4	.3	.2	.2	.5	.6	.5	.5	.8
115.	* .0	.0	.0	.0	.0	.0	.0	.9	.8	1.0	.7	.4	.3	.2	.2	.5	.5	.5	.7	.8
120.	* .0	.0	.0	.0	.0	.0	.0	.9	.8	1.0	.7	.4	.3	.2	.2	.4	.6	.5	.7	.8
125.	* .0	.0	.0	.0	.0	.0	.0	.8	.7	.8	.7	.4	.3	.2	.2	.4	.6	.5	.8	.8
130.	* .0	.0	.1	.0	.0	.0	.0	.7	.7	.8	.7	.4	.3	.2	.2	.3	.5	.4	.8	.8
135.	* .1	.1	.1	.1	.0	.0	.0	.7	.7	.8	.7	.4	.3	.2	.1	.4	.4	.4	.8	.8
140.	* .2	.1	.2	.1	.0	.0	.0	.7	.7	.8	.7	.4	.4	.2	.1	.3	.4	.5	.7	.6
145.	* .3	.3	.2	.2	.1	.0	.0	.7	.7	.9	.6	.5	.5	.2	.1	.3	.3	.5	.7	.6
150.	* .4	.4	.3	.2	.1	.0	.0	.7	.7	.9	.6	.4	.4	.2	.2	.3	.3	.5	.7	.7
155.	* .4	.4	.4	.2	.1	.0	.0	.7	.8	.9	.6	.4	.4	.2	.2	.2	.2	.6	.7	.7
160.	* .5	.4	.5	.3	.1	.1	.0	.7	.8	.9	.5	.5	.4	.2	.2	.2	.2	.6	.7	.7
165.	* .5	.4	.5	.4	.2	.1	.0	.7	.9	.9	.6	.4	.4	.3	.2	.2	.4	.6	.7	.7
170.	* .5	.4	.6	.5	.2	.1	.0	.7	.9	.9	.6	.5	.4	.3	.2	.3	.4	.6	.7	.7
175.	* .5	.4	.5	.5	.2	.1	.0	.7	.9	.9	.6	.4	.5	.3	.2	.4	.4	.6	.7	.7
180.	* .5	.4	.5	.5	.2	.1	.0	.8	.9	.9	.4	.5	.5	.3	.2	.4	.4	.6	.6	.6
185.	* .5	.4	.5	.5	.2	.1	.1	.8	.9	.9	.4	.3	.4	.3	.2	.4	.4	.6	.7	.7
190.	* .4	.4	.5	.4	.2	.1	.1	.8	.9	.8	.4	.3	.4	.3	.2	.4	.4	.6	.7	.7
195.	* .4	.4	.5	.4	.1	.1	.1	.8	.9	.7	.5	.4	.5	.3	.1	.4	.4	.6	.7	.7
200.	* .4	.4	.5	.4	.1	.1	.1	.8	.9	.7	.6	.5	.6	.3	.1	.4	.4	.6	.7	.7
205.	* .4	.4	.5	.3	.1	.1	.1	1.0	.9	.8	.6	.6	.5	.2	.0	.4	.4	.6	.7	.7

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .4	.4	.5	.3	.1	.1	.1	1.0	1.0	.8	.7	.6	.5	.1	.0	.4	.4	.7	.7	.7
215.	* .4	.4	.5	.3	.1	.1	.1	.9	1.0	.7	.7	.6	.5	.1	.0	.4	.4	.7	.7	.7
220.	* .4	.4	.5	.3	.1	.1	.1	.9	.9	.9	.8	.7	.5	.1	.1	.3	.4	.7	.7	.7
225.	* .4	.4	.5	.2	.1	.1	.1	1.0	.9	1.0	.8	.7	.5	.2	.1	.3	.4	.6	.6	.7
230.	* .4	.4	.5	.2	.1	.2	.2	1.1	1.0	1.0	.8	.7	.4	.2	.1	.1	.3	.6	.8	.7
235.	* .4	.4	.5	.2	.1	.2	.1	1.0	1.0	.9	.7	.7	.2	.2	.1	.1	.3	.7	.8	.9
240.	* .4	.4	.5	.4	.4	.4	.1	1.0	.9	.9	.7	.6	.2	.1	.0	.1	.3	.5	.8	.7
245.	* .4	.4	.6	.4	.3	.4	.4	1.0	.8	.9	.7	.4	.2	.1	.0	.1	.1	.4	.6	.6
250.	* .4	.4	.6	.5	.6	.4	.5	.8	.7	.8	.5	.3	.1	.1	.0	.0	.1	.4	.6	.5
255.	* .4	.5	.7	.6	.7	.7	.6	.5	.5	.5	.5	.2	.1	.1	.0	.0	.0	.2	.3	.4
260.	* .4	.5	.8	.9	.8	.8	.7	.3	.3	.3	.3	.2	.1	.1	.0	.0	.0	.1	.1	.1
265.	* .5	.6	.8	.8	.8	.8	.8	.2	.1	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.1
270.	* .5	.7	1.0	.8	.8	.8	.7	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1
275.	* .5	.7	.9	.6	.7	.9	.7	.0	.0	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
280.	* .5	.8	.9	.7	.6	.9	.7	.0	.0	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
285.	* .4	.8	.9	.6	.8	.7	.9	.0	.0	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
290.	* .6	.7	.7	.5	.7	.7	.8	.0	.0	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
295.	* .6	.6	.5	.5	.7	.7	.7	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
300.	* .6	.6	.6	.6	.8	.7	.7	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0
305.	* .6	.5	.6	.7	.8	.7	.7	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0
310.	* .6	.4	.7	.5	.7	.7	.6	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0
315.	* .4	.4	.4	.5	.6	.7	.6	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0
320.	* .4	.2	.3	.5	.6	.5	.5	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0
325.	* .2	.2	.3	.5	.6	.5	.5	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0
330.	* .2	.2	.4	.7	.6	.6	.5	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
335.	* .2	.3	.4	.6	.7	.6	.6	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
340.	* .2	.3	.5	.6	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	* .1	.3	.5	.6	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	* .2	.3	.5	.6	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	* .2	.3	.5	.6	.6	.6	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
360.	* .2	.3	.5	.6	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
MAX	* .6	.8	1.0	.9	.8	.9	.9	1.1	1.1	1.1	.9	.7	.6	.3	.2	.5	.8	.7	.8	.9
DEGR.	* 290	280	270	260	260	275	285	230	85	85	100	220	200	165	80	110	85	70	125	235

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.7	.7	.7	.6	.4	.5	.4
5.	.0	.7	.7	.7	.5	.3	.6	.4
10.	.0	.7	.7	.7	.5	.4	.6	.4
15.	.0	.8	.8	.7	.5	.3	.6	.4
20.	.0	.8	.8	.7	.6	.4	.5	.4
25.	.0	.8	.8	.7	.7	.6	.5	.4
30.	.0	.8	.8	.7	.7	.6	.5	.4
35.	.0	.9	.8	.7	.6	.6	.5	.4
40.	.0	.9	.9	.8	.7	.5	.6	.4
45.	.0	1.0	.9	.8	.8	.6	.6	.5
50.	.0	1.0	.9	.8	.9	.7	.6	.4
55.	.1	1.1	.9	.8	.9	.7	.5	.3
60.	.1	1.1	.9	.9	.7	.7	.5	.3
65.	.3	.9	.7	.7	.7	.5	.5	.3
70.	.4	.8	.6	.5	.4	.5	.3	.2
75.	.6	.6	.4	.4	.3	.4	.3	.3
80.	.7	.4	.3	.3	.3	.3	.3	.3
85.	.9	.1	.3	.3	.2	.3	.3	.3
90.	.8	.1	.1	.2	.2	.3	.3	.3
95.	.8	.1	.1	.1	.2	.3	.3	.3
100.	.7	.1	.1	.1	.2	.3	.3	.3
105.	.8	.1	.1	.1	.3	.3	.2	.3
110.	.8	.0	.1	.1	.3	.3	.2	.3
115.	.8	.0	.1	.1	.3	.3	.2	.3
120.	.7	.0	.1	.1	.2	.2	.2	.3
125.	.7	.0	.1	.1	.2	.2	.2	.3
130.	.7	.0	.1	.1	.2	.2	.2	.3
135.	.7	.0	.0	.1	.2	.2	.2	.2
140.	.6	.0	.0	.1	.2	.2	.2	.1
145.	.7	.0	.0	.0	.1	.1	.1	.1
150.	.7	.0	.0	.0	.1	.1	.1	.1
155.	.7	.0	.0	.0	.0	.0	.0	.0
160.	.7	.0	.0	.0	.0	.0	.0	.0
165.	.6	.0	.0	.0	.0	.0	.0	.0
170.	.7	.0	.0	.0	.0	.0	.0	.0
175.	.7	.0	.0	.0	.0	.0	.0	.0
180.	.6	.0	.0	.0	.0	.0	.0	.0
185.	.6	.0	.0	.0	.0	.0	.0	.0
190.	.6	.0	.0	.0	.0	.0	.0	.0
195.	.7	.0	.0	.0	.0	.0	.0	.0
200.	.7	.0	.0	.0	.0	.0	.0	.0
205.	.7	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT) RUN: Site 2 Existing AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.8	.0	.0	.0	.0	.0	.0	.0
215.	.9	.0	.0	.0	.0	.0	.0	.0
220.	.7	.0	.0	.0	.0	.0	.0	.0
225.	.8	.0	.0	.0	.0	.0	.0	.0
230.	.8	.0	.0	.0	.0	.0	.0	.0
235.	.8	.3	.2	.2	.0	.0	.0	.0
240.	.7	.3	.2	.2	.2	.0	.0	.0
245.	.5	.5	.5	.4	.2	.1	.0	.0
250.	.4	.6	.6	.7	.5	.1	.0	.0
255.	.3	.9	.9	.8	.6	.2	.1	.0
260.	.2	1.0	1.0	1.1	.7	.2	.1	.0
265.	.0	1.0	1.1	.9	.9	.3	.1	.1
270.	.0	1.0	1.0	1.0	.8	.3	.2	.1
275.	.0	.9	.9	.9	.8	.5	.3	.1
280.	.0	1.0	.9	.9	.8	.5	.3	.1
285.	.0	1.0	.9	.9	.8	.5	.4	.0
290.	.0	.9	.8	.8	.8	.5	.4	.0
295.	.0	.8	.8	.8	.7	.5	.4	.1
300.	.0	.8	.8	.8	.6	.5	.4	.1
305.	.0	.8	.8	.8	.6	.5	.3	.1
310.	.0	.9	.7	.7	.6	.5	.3	.1
315.	.0	.9	.7	.7	.6	.4	.2	.1
320.	.0	.8	.7	.7	.6	.3	.2	.1
325.	.0	.8	.7	.7	.5	.3	.2	.2
330.	.0	.8	.7	.7	.4	.3	.1	.1
335.	.0	.8	.7	.7	.4	.3	.1	.1
340.	.0	.8	.8	.7	.4	.4	.1	.2
345.	.0	.7	.7	.7	.4	.2	.2	.3
350.	.0	.7	.7	.7	.5	.2	.3	.3
355.	.0	.7	.7	.7	.5	.4	.3	.3
360.	.0	.7	.7	.7	.6	.4	.5	.4
MAX	.9	1.1	1.1	1.1	.9	.7	.6	.5
DEGR.	215	55	265	260	265	50	5	45

THE HIGHEST CONCENTRATION IS 1.10 PPM AT 230 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS 1.10 PPM AT 85 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS 1.10 PPM AT 85 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT) RUN: Site 2 Existing PM
DATE: 03/21/2010 TIME: 22:19:57.08

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	2564.	3.3	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	2564.	3.3	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	2293.	3.3	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	380.6	719.4	315.	251.	AG	88.	100.0	.0	48.0	1.00	16.0
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	271.	3.3	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	534.7	814.3	131.	252.	AG	92.	100.0	.0	24.0	.94	6.6
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	2453.	3.3	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	2853.	3.3	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	2778.	3.3	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	3381.7	1772.8	2713.	72.	AG	113.	100.0	.0	48.0	1.50	137.8
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	75.	3.3	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	1040.1	974.1	226.	73.	AG	105.	100.0	.0	24.0	1.76	11.5
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3732.	3.3	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3732.	3.3	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	1155.	3.5	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	957.	3.5	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1518.2	-236.3	1235.	146.	AG	118.	100.0	.0	36.0	1.43	62.8
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	198.	3.5	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	911.0	698.1	113.	145.	AG	37.	100.0	.0	12.0	.73	5.7
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	984.	3.5	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	984.	3.5	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1132.	3.5	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	422.	3.5	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	621.2	1074.1	110.	328.	AG	128.	100.0	.0	36.0	.86	5.6
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	710.	3.5	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	103.3	1842.1	1024.	328.	AG	69.	100.0	.0	24.0	1.27	52.0
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	535.	3.5	.0	44.0		

1 PAGE 2

JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT) RUN: Site 2 Existing PM
DATE: 03/21/2010 TIME: 22:19:57.08

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	60	2.0	2293	999	20.50	1	3
6.	EB Wil LT Q	150	126	2.0	271	1084	20.50	1	3
10.	WB Wil T+R Q	150	77	2.0	2778	1010	20.50	1	3
12.	WB Wil LT Q	150	143	2.0	75	1084	20.50	1	3
17.	NB Vet T+LT Q	150	107	2.0	957	860	20.50	1	3
19.	NB Vet RT Q	150	102	2.0	198	927	20.50	1	3
24.	SB Vet T+LT Q	150	116	2.0	422	817	20.50	1	3
26.	SB Vet RT Q	150	94	2.0	710	808	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

1 PAGE 3

JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT) RUN: Site 2 Existing PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.1	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.4	.3	.4	.1	.1
5.	.1	.4	.4	.5	.5	.6	.4	.0	.0	.0	.0	.0	.0	.0	.4	.4	.3	.4	.1	.1
10.	.1	.3	.4	.5	.5	.6	.4	.0	.0	.0	.0	.0	.0	.0	.4	.3	.4	.4	.1	.1
15.	.1	.2	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.3	.4	.4	.1	.1
20.	.1	.2	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.3	.4	.4	.2	.1
25.	.1	.3	.4	.5	.6	.7	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.2	.1
30.	.1	.3	.4	.5	.8	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.4	.2	.1
35.	.1	.3	.3	.6	.8	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.1
40.	.1	.3	.3	.7	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.1
45.	.1	.3	.3	.7	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.1
50.	.1	.3	.3	.7	.7	.6	.6	.1	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.1	.2
55.	.1	.2	.3	.7	.6	.6	.6	.2	.1	.2	.1	.0	.0	.0	.3	.3	.5	.3	.2	.2
60.	.0	.2	.3	.6	.6	.6	.6	.2	.3	.3	.2	.0	.0	.0	.3	.3	.5	.3	.3	.3
65.	.0	.1	.2	.4	.6	.6	.6	.4	.4	.4	.4	.1	.0	.0	.3	.3	.6	.4	.4	.4
70.	.0	.0	.2	.4	.5	.5	.3	.6	.6	.6	.5	.1	.1	.0	.3	.4	.6	.6	.6	.4
75.	.0	.0	.0	.2	.3	.3	.3	.7	.8	.8	.7	.2	.1	.0	.3	.4	.7	.6	.8	.8
80.	.0	.0	.0	.1	.3	.3	.1	.9	.9	.9	.8	.3	.1	.1	.4	.4	.8	.7	.8	.7
85.	.0	.0	.0	.1	.1	.1	.1	.9	.9	1.0	1.0	.4	.2	.1	.4	.6	1.0	.9	.7	.7
90.	.0	.0	.0	.0	.1	.1	.1	.9	.9	1.0	1.0	.5	.2	.1	.4	.6	1.0	.8	.7	.7
95.	.0	.0	.0	.0	.0	.0	.0	.9	.8	1.0	.8	.5	.3	.1	.4	.7	.9	.7	.7	.7
100.	.0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.8	.5	.3	.2	.4	.7	1.0	.7	.7	.6
105.	.0	.0	.0	.0	.0	.0	.0	.8	.9	.9	.8	.5	.3	.2	.4	.9	1.0	.5	.6	.7
110.	.0	.0	.0	.0	.0	.0	.0	.8	1.0	.9	.8	.5	.3	.1	.3	.9	.8	.6	.5	.8
115.	.0	.0	.0	.0	.0	.0	.0	.7	.8	.8	.7	.5	.3	.1	.3	.9	.7	.6	.7	.8
120.	.0	.0	.0	.0	.0	.0	.0	.7	.8	.8	.7	.4	.4	.1	.3	.7	.7	.6	.7	.8
125.	.0	.0	.0	.0	.0	.0	.0	.7	.8	.8	.7	.4	.4	.1	.2	.6	.5	.5	.8	.8
130.	.1	.1	.1	.0	.0	.0	.0	.7	.8	.8	.6	.4	.4	.1	.4	.7	.4	.5	.7	.7
135.	.2	.1	.1	.1	.0	.0	.0	.7	.8	.8	.6	.5	.3	.2	.5	.6	.4	.5	.7	.7
140.	.3	.3	.2	.1	.0	.0	.0	.7	.7	.7	.6	.4	.4	.1	.5	.5	.5	.5	.7	.7
145.	.4	.3	.2	.2	.1	.0	.0	.7	.7	.8	.5	.4	.3	.1	.5	.4	.5	.5	.7	.5
150.	.4	.4	.4	.2	.1	.0	.0	.7	.9	.9	.6	.4	.3	.2	.3	.5	.5	.5	.6	.5
155.	.5	.4	.5	.3	.1	.1	.0	.7	.9	.9	.5	.4	.3	.2	.2	.5	.4	.7	.6	.5
160.	.6	.4	.6	.4	.2	.1	.0	.7	.9	.9	.6	.3	.3	.3	.2	.2	.3	.6	.7	.6
165.	.6	.5	.6	.5	.2	.1	.0	.7	.9	.9	.5	.3	.4	.2	.1	.2	.5	.6	.7	.6
170.	.6	.4	.5	.5	.2	.1	.0	.7	.9	.9	.5	.4	.3	.4	.1	.3	.5	.6	.6	.5
175.	.5	.4	.5	.5	.2	.1	.1	.8	.9	.9	.5	.4	.3	.4	.1	.3	.5	.6	.6	.5
180.	.5	.4	.5	.5	.2	.1	.1	.7	.8	.8	.4	.4	.4	.3	.1	.3	.5	.6	.6	.5
185.	.4	.4	.5	.4	.1	.1	.1	.8	.8	.8	.4	.3	.5	.3	.1	.3	.5	.6	.6	.5
190.	.4	.4	.5	.4	.1	.1	.1	.8	.9	.8	.4	.3	.5	.3	.1	.3	.4	.6	.6	.5
195.	.4	.4	.5	.4	.1	.1	.1	.8	.9	.7	.5	.4	.6	.3	.1	.2	.4	.6	.6	.6
200.	.4	.4	.5	.4	.1	.1	.1	.8	.9	.7	.5	.6	.7	.3	.1	.2	.4	.6	.6	.6
205.	.4	.4	.5	.3	.1	.1	.1	.8	.8	.7	.6	.6	.7	.3	.1	.1	.4	.6	.6	.6

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.4	.4	.5	.3	.1	.1	.1	.8	.8	.6	.6	.6	.6	.3	.0	.1	.4	.6	.6	.6
215.	.4	.4	.5	.3	.1	.1	.1	.9	.8	.6	.7	.6	.5	.3	.1	.1	.3	.6	.6	.5
220.	.4	.4	.5	.3	.1	.1	.1	.9	.9	.8	.7	.7	.4	.2	.1	.1	.3	.6	.6	.5
225.	.4	.4	.5	.2	.1	.1	.1	1.0	.8	.8	.7	.7	.4	.2	.0	.2	.2	.6	.7	.5
230.	.4	.4	.5	.2	.1	.1	.1	1.0	.8	.7	.8	.5	.4	.3	.0	.2	.3	.6	.6	.7
235.	.4	.4	.5	.2	.1	.1	.1	1.0	.9	.8	.7	.6	.4	.3	.0	.1	.2	.6	.7	.6
240.	.4	.4	.5	.2	.1	.2	.1	.9	.8	.7	.7	.5	.3	.3	.0	.0	.2	.4	.6	.5
245.	.4	.4	.5	.2	.2	.2	.1	.8	.7	.6	.5	.5	.2	.3	.0	.0	.2	.4	.5	.5
250.	.4	.4	.5	.3	.3	.2	.2	.6	.4	.4	.4	.5	.2	.3	.0	.0	.0	.3	.4	.4
255.	.4	.4	.5	.4	.4	.4	.3	.5	.4	.3	.3	.4	.2	.3	.0	.0	.0	.1	.4	.3
260.	.4	.4	.6	.5	.5	.4	.6	.3	.2	.3	.3	.4	.2	.3	.0	.0	.0	.1	.2	.2
265.	.4	.4	.8	.6	.5	.5	.7	.2	.2	.3	.3	.4	.2	.3	.0	.0	.0	.0	.1	.1
270.	.4	.4	.8	.6	.5	.6	.7	.0	.2	.1	.2	.4	.2	.3	.0	.0	.0	.0	.1	.1
275.	.4	.6	.7	.6	.4	.6	.6	.0	.0	.1	.3	.4	.2	.3	.0	.0	.0	.0	.0	.0
280.	.4	.7	.7	.4	.4	.7	.6	.0	.0	.2	.4	.4	.2	.3	.0	.0	.0	.0	.0	.0
285.	.4	.7	.7	.3	.5	.7	.6	.0	.0	.2	.4	.3	.2	.3	.0	.0	.0	.0	.0	.0
290.	.4	.8	.6	.4	.5	.6	.6	.0	.0	.2	.4	.3	.2	.3	.0	.0	.0	.0	.0	.0
295.	.6	.7	.5	.5	.6	.6	.5	.0	.0	.2	.4	.3	.2	.3	.0	.0	.0	.0	.0	.0
300.	.6	.6	.5	.6	.5	.6	.5	.0	.0	.1	.4	.3	.2	.3	.0	.0	.0	.0	.0	.0
305.	.6	.6	.5	.5	.6	.5	.4	.0	.0	.1	.3	.2	.4	.3	.0	.0	.0	.0	.0	.0
310.	.4	.5	.6	.6	.6	.5	.4	.0	.0	.1	.3	.2	.4	.3	.0	.0	.0	.0	.0	.0
315.	.4	.3	.6	.5	.6	.5	.4	.0	.0	.1	.3	.2	.4	.2	.1	.1	.1	.0	.0	.0
320.	.4	.3	.4	.5	.5	.5	.4	.0	.0	.0	.2	.3	.4	.2	.1	.1	.1	.1	.0	.0
325.	.3	.4	.4	.5	.5	.5	.4	.0	.0	.0	.2	.3	.2	.1	.2	.3	.3	.1	.0	.0
330.	.1	.2	.2	.5	.5	.5	.4	.0	.0	.0	.1	.1	.1	.0	.3	.4	.4	.1	.0	.0
335.	.1	.2	.3	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.3	.4	.4	.2	.1	.0
340.	.1	.3	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.3	.5	.5	.3	.1	.0
345.	.0	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.6	.4	.3	.1	.1
350.	.0	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.6	.4	.3	.1	.1
355.	.1	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.5	.3	.4	.1	.1
360.	.1	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.4	.3	.4	.1	.1
MAX	.6	.8	.8	.7	.8	.7	.7	1.0	1.0	1.0	1.0	.7	.7	.4	.5	.9	1.0	.9	.8	.8
DEGR.	160	290	265	40	30	25	265	225	110	85	85	220	200	170	135	105	85	85	125	110

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.4	.8	.8	.5	.3	.5	.3
5.	.0	.4	.7	.8	.5	.3	.6	.4
10.	.0	.4	.7	.6	.4	.4	.7	.4
15.	.0	.4	.7	.5	.4	.5	.8	.4
20.	.0	.4	.7	.5	.4	.6	.8	.5
25.	.0	.4	.7	.6	.4	.6	.6	.5
30.	.0	.4	.6	.5	.5	.6	.5	.4
35.	.0	.6	.6	.5	.5	.6	.6	.4
40.	.0	.6	.8	.5	.5	.6	.6	.4
45.	.0	.6	.9	.6	.5	.6	.6	.4
50.	.1	.6	.8	.7	.8	.6	.6	.4
55.	.1	.7	.7	.8	.8	.6	.5	.4
60.	.2	.7	.7	.8	.7	.6	.5	.3
65.	.3	.7	.7	.7	.6	.5	.4	.3
70.	.4	.5	.4	.3	.5	.5	.3	.3
75.	.6	.4	.3	.3	.3	.3	.3	.3
80.	.8	.2	.3	.2	.3	.3	.3	.3
85.	.9	.1	.1	.2	.3	.3	.3	.4
90.	.7	.0	.1	.1	.2	.4	.4	.4
95.	.7	.1	.1	.1	.2	.4	.4	.4
100.	.7	.1	.1	.1	.2	.4	.4	.4
105.	.7	.1	.1	.1	.3	.4	.4	.4
110.	.7	.1	.1	.1	.3	.4	.3	.4
115.	.7	.1	.1	.1	.4	.4	.3	.4
120.	.7	.0	.1	.1	.4	.4	.3	.4
125.	.7	.0	.1	.1	.3	.3	.4	.4
130.	.6	.0	.1	.1	.3	.3	.4	.4
135.	.4	.0	.1	.1	.2	.3	.4	.3
140.	.4	.0	.0	.1	.2	.3	.3	.3
145.	.4	.0	.0	.1	.1	.1	.1	.1
150.	.4	.0	.0	.0	.1	.1	.1	.1
155.	.5	.0	.0	.0	.0	.1	.1	.1
160.	.5	.0	.0	.0	.0	.0	.0	.0
165.	.5	.0	.0	.0	.0	.0	.0	.0
170.	.4	.0	.0	.0	.0	.0	.0	.0
175.	.4	.0	.0	.0	.0	.0	.0	.0
180.	.4	.0	.0	.0	.0	.0	.0	.0
185.	.4	.0	.0	.0	.0	.0	.0	.0
190.	.4	.0	.0	.0	.0	.0	.0	.0
195.	.4	.0	.0	.0	.0	.0	.0	.0
200.	.5	.0	.0	.0	.0	.0	.0	.0
205.	.6	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT) RUN: Site 2 Existing PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.6	.0	.0	.0	.0	.0	.0	.0
215.	.5	.0	.0	.0	.0	.0	.0	.0
220.	.6	.0	.0	.0	.0	.0	.0	.0
225.	.7	.0	.0	.0	.0	.0	.0	.0
230.	.7	.0	.0	.0	.0	.0	.0	.0
235.	.7	.1	.0	.0	.0	.0	.0	.0
240.	.5	.1	.1	.1	.0	.0	.0	.0
245.	.4	.2	.1	.2	.2	.0	.0	.0
250.	.4	.4	.3	.3	.2	.0	.0	.0
255.	.2	.4	.4	.4	.4	.0	.0	.0
260.	.2	.4	.4	.6	.6	.0	.0	.0
265.	.2	.4	.7	.7	.6	.2	.0	.0
270.	.0	.5	.7	.7	.5	.3	.0	.0
275.	.0	.4	.7	.8	.7	.3	.0	.0
280.	.0	.4	.6	.8	.7	.3	.2	.0
285.	.0	.4	.8	.8	.7	.3	.3	.0
290.	.0	.4	.6	.8	.7	.3	.3	.0
295.	.0	.4	.6	.7	.7	.3	.3	.0
300.	.0	.4	.6	.7	.7	.4	.3	.1
305.	.0	.5	.6	.7	.6	.4	.3	.1
310.	.0	.5	.6	.7	.6	.4	.3	.1
315.	.0	.4	.6	.7	.6	.3	.2	.1
320.	.0	.4	.6	.7	.7	.2	.2	.1
325.	.0	.3	.6	.7	.6	.3	.3	.1
330.	.0	.4	.6	.8	.5	.3	.3	.1
335.	.0	.5	.6	.8	.4	.3	.2	.2
340.	.0	.4	.7	.8	.5	.3	.1	.4
345.	.0	.4	.8	.8	.5	.3	.2	.4
350.	.0	.4	.8	.8	.4	.4	.3	.3
355.	.0	.4	.8	.9	.3	.4	.4	.3
360.	.0	.4	.8	.8	.5	.3	.5	.3
MAX	.9	.7	.9	.9	.8	.6	.8	.5
DEGR.	85	55	45	355	50	20	15	20

THE HIGHEST CONCENTRATION IS 1.00 PPM AT 225 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS 1.00 PPM AT 110 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS 1.00 PPM AT 85 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT) RUN: Site 2 NO BUILD AM
DATE: 03/19/2010 TIME: 09:06:00.03

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	5619.	.8	.0	68.0		
2. EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	5619.	.8	.0	68.0		
3. EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	4678.	.8	.0	68.0		
4. EB Wil T+R Q	678.0	822.0	-5342.0	-1254.4	6368.	251.	AG	17.	100.0	.0	48.0	2.01	323.5
5. EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	941.	.8	.0	44.0		
6. EB Wil LT Q	659.0	855.0	-2454.5	-165.7	3277.	252.	AG	17.	100.0	.0	24.0	2.54	166.4
7. EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	4869.	.8	.0	68.0		
8. WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	3164.	.8	.0	68.0		
9. WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	3147.	.8	.0	68.0		
10. WB Wil T+R Q	798.0	946.0	8794.2	3504.8	8396.	72.	AG	24.	100.0	.0	48.0	****	426.5
11. WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	17.	.8	.0	44.0		
12. WB Wil LT Q	824.0	908.0	933.5	941.5	114.	73.	AG	21.	100.0	.0	24.0	8.00	5.8
13. WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3437.	.8	.0	68.0		
14. WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3437.	.8	.0	68.0		
15. NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	946.	.9	.0	32.0		
16. NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	814.	.9	.0	56.0		
17. NB Vet T+LT Q	820.0	783.0	1337.8	27.1	916.	146.	AG	24.	100.0	.0	36.0	1.33	46.5
18. NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	132.	.9	.0	32.0		
19. NB Vet RT Q	847.0	791.0	890.4	728.0	77.	145.	AG	8.	100.0	.0	12.0	.52	3.9
20. NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1787.	.9	.0	44.0		
21. NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1787.	.9	.0	44.0		
22. SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1155.	.9	.0	44.0		
23. SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	833.	.9	.0	56.0		
24. SB Vet T+LT Q	679.0	981.0	-150.8	2316.8	1573.	328.	AG	26.	100.0	.0	36.0	1.88	79.9
25. SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	322.	.9	.0	44.0		
26. SB Vet RT Q	643.0	972.0	601.2	1039.3	79.	328.	AG	13.	100.0	.0	24.0	.52	4.0
27. SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	791.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT) RUN: Site 2 NO BUILD AM
DATE: 03/19/2010 TIME: 09:06:00.03

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4. EB Wil T+R Q	150	57	2.0	4678	983	4.10	1	3
6. EB Wil LT Q	150	118	2.0	941	995	4.10	1	3
10. WB Wil T+R Q	150	82	2.0	3147	84	4.10	1	3
12. WB Wil LT Q	150	143	2.0	17	84	4.10	1	3
17. NB Vet T+LT Q	150	111	2.0	814	875	4.10	1	3
19. NB Vet RT Q	150	106	2.0	132	955	4.10	1	3
24. SB Vet T+LT Q	150	120	2.0	833	852	4.10	1	3
26. SB Vet RT Q	150	90	2.0	322	834	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	1066.0	492.0	5.0
2. SE 164 S	942.0	686.0	5.0
3. SE 82 S	892.0	756.0	5.0
4. SE CNR	869.0	821.0	5.0
5. SE 82 E	925.0	853.0	5.0
6. SE 164 E	1005.0	880.0	5.0
7. SE MID E	1219.0	947.0	5.0
8. NE MID E	1144.0	1099.0	5.0
9. NE 164 E	918.0	1026.0	5.0
10. NE 82 E	838.0	1000.0	5.0
11. NE CNR	759.0	983.0	5.0
12. NE 82 N	716.0	1047.0	5.0
13. NE 164 N	676.0	1120.0	5.0
14. NE MID N	595.0	1269.0	5.0
15. NW MID N	464.0	1209.0	5.0
16. NW 164 N	546.0	1079.0	5.0
17. NW 82 N	589.0	1010.0	5.0
18. NW CNR	611.0	945.0	5.0
19. NW 82 W	552.0	910.0	5.0
20. NW 164 W	475.0	884.0	5.0
21. NW MID W	273.0	815.0	5.0
22. SW MID W	305.0	649.0	5.0
23. SW 164 W	565.0	737.0	5.0
24. SW 82 W	645.0	764.0	5.0
25. SW CNR	718.0	779.0	5.0
26. SW 82 S	774.0	718.0	5.0
27. SW 164 S	824.0	646.0	5.0
28. SW MID S	957.0	459.0	5.0

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JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT) RUN: Site 2 NO BUILD AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
15.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
20.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
25.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.2	.2	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
75.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.4	.3	.3	.0	.0	.0	.0	.0	.0	.1	.2	.1
95.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.1	.0	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
120.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
125.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
130.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.2
135.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2
140.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
145.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
150.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
155.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
160.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
165.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
170.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
175.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
180.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
185.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
190.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
195.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
200.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
205.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1
215.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
220.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
225.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
230.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240.	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.1	.1	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.1	.1	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
255.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.1	.1	.1	.2	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
290.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
295.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
300.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.2	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
320.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
340.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
345.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
350.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
355.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
360.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.2	.2	.2	.2	.3	.4	.3	.3	.2	.1	.2	.1	.1	.1	.2	.2	.2
DEGR.	150	150	0	280	50	50	50	95	90	85	90	285	160	305	0	0	0	205	90	115

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.1	.0	.0	.0
5.	.0	.1	.1	.1	.1	.0	.0	.0
10.	.0	.1	.1	.1	.1	.0	.0	.0
15.	.0	.1	.1	.1	.1	.0	.0	.0
20.	.0	.1	.1	.1	.1	.0	.0	.0
25.	.0	.1	.1	.1	.1	.1	.0	.0
30.	.0	.1	.1	.1	.1	.1	.0	.0
35.	.0	.2	.1	.1	.1	.1	.0	.0
40.	.0	.2	.1	.1	.2	.1	.0	.0
45.	.0	.2	.1	.1	.2	.1	.0	.0
50.	.0	.2	.1	.1	.1	.1	.0	.0
55.	.0	.2	.1	.2	.1	.1	.0	.0
60.	.0	.1	.1	.2	.1	.1	.0	.0
65.	.1	.1	.2	.2	.1	.0	.0	.0
70.	.1	.1	.2	.2	.1	.0	.0	.0
75.	.1	.1	.1	.1	.1	.0	.0	.0
80.	.1	.1	.0	.0	.0	.0	.0	.0
85.	.1	.0	.0	.0	.0	.0	.0	.0
90.	.1	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.2	.0	.0	.0	.0	.0	.0	.0
105.	.2	.0	.0	.0	.0	.0	.0	.0
110.	.2	.0	.0	.0	.0	.0	.0	.0
115.	.2	.0	.0	.0	.0	.0	.0	.0
120.	.2	.0	.0	.0	.0	.0	.0	.0
125.	.2	.0	.0	.0	.0	.0	.0	.0
130.	.2	.0	.0	.0	.0	.0	.0	.0
135.	.2	.0	.0	.0	.0	.0	.0	.0
140.	.2	.0	.0	.0	.0	.0	.0	.0
145.	.2	.0	.0	.0	.0	.0	.0	.0
150.	.2	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT) RUN: Site 2 NO BUILD AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.1	.1	.0	.1	.0	.0	.0	.0
250.	.0	.1	.1	.1	.1	.0	.0	.0
255.	.0	.2	.2	.2	.1	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.2	.2	.2	.2	.0	.0	.0
275.	.0	.2	.2	.2	.1	.0	.0	.0
280.	.0	.2	.2	.2	.1	.1	.0	.0
285.	.0	.2	.2	.2	.1	.1	.0	.0
290.	.0	.2	.1	.1	.1	.1	.0	.0
295.	.0	.1	.1	.1	.1	.1	.0	.0
300.	.0	.1	.1	.1	.1	.1	.0	.0
305.	.0	.1	.1	.1	.1	.1	.0	.0
310.	.0	.1	.1	.1	.1	.1	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.2	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.1	.0	.0	.0
340.	.0	.1	.1	.1	.1	.0	.0	.0
345.	.0	.1	.1	.1	.1	.0	.0	.0
350.	.0	.1	.1	.1	.1	.0	.0	.0
355.	.0	.1	.1	.1	.1	.0	.0	.0
360.	.0	.1	.1	.1	.1	.0	.0	.0
MAX	.2	.2	.2	.2	.2	.1	.0	.0
DEGR.	95	35	65	55	40	25	0	0

THE HIGHEST CONCENTRATION IS .40 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 95 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT) RUN: Site 2 NO BUILD PM
DATE: 03/19/2010 TIME: 09:06:18.82

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	3358.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	3358.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	3073.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-2149.1	-153.1	2991.	251.	AG	20.	100.0	.0	48.0	1.51	151.9
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	285.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-858.8	357.4	1597.	252.	AG	18.	100.0	.0	24.0	****	81.1
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	3305.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	4295.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	4276.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	7799.9	3186.6	7352.	72.	AG	25.	100.0	.0	48.0	2.68	373.5
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	19.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	948.3	946.0	130.	73.	AG	21.	100.0	.0	24.0	9.00	6.6
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	4969.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	4969.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	1351.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	1028.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1448.3	-134.3	1112.	146.	AG	21.	100.0	.0	36.0	1.33	56.5
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	323.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	990.5	582.6	253.	145.	AG	7.	100.0	.0	12.0	1.00	12.9
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1719.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1719.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1987.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	858.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	85.1	1937.0	1125.	328.	AG	24.	100.0	.0	36.0	1.44	57.2
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	1129.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	-866.6	3405.5	2864.	328.	AG	13.	100.0	.0	24.0	1.78	145.5
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	968.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT) RUN: Site 2 NO BUILD PM
DATE: 03/19/2010 TIME: 09:06:18.82

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	68	2.0	3073	982	4.10	1	3
6.	EB Wil LT Q	150	126	2.0	285	84	4.10	1	3
10.	WB Wil T+R Q	150	85	2.0	4276	982	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	19	84	4.10	1	3
17.	NB Vet T+LT Q	150	97	2.0	1028	790	4.10	1	3
19.	NB Vet RT Q	150	95	2.0	323	955	4.10	1	3
24.	SB Vet T+LT Q	150	109	2.0	858	810	4.10	1	3
26.	SB Vet RT Q	150	87	2.0	1129	804	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

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JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT) RUN: Site 2 NO BUILD PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75.	.0	.0	.0	.0	.1	.1	.1	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.1	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
85.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
150.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
155.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
160.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.1	.0	.0	.0	.1	.1	.1	.1
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
170.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
175.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
180.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
185.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
190.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
195.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
200.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
205.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
215.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
220.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
225.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
230.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
235.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
240.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.0	.0	.0	.0	.0	.1	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255.	.1	.0	.0	.0	.0	.1	.1	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
290.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
295.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
300.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
345.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
350.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.1	.1	.2	.2	.2	.3	.3	.2	.2	.1	.0	.1	.2	.2	.2	.2	.1
DEGR.	150	155	150	0	0	40	30	65	75	75	75	300	160	0	0	340	340	80	230	65

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.3	.2	.2	.1	.0	.0	.0
5.	.0	.3	.2	.1	.1	.0	.0	.0
10.	.0	.3	.3	.1	.1	.0	.0	.0
15.	.0	.3	.3	.1	.1	.0	.0	.0
20.	.0	.3	.2	.1	.1	.0	.0	.0
25.	.0	.3	.2	.1	.1	.0	.0	.0
30.	.0	.3	.2	.1	.1	.0	.0	.0
35.	.0	.3	.2	.1	.0	.0	.0	.0
40.	.0	.3	.2	.1	.0	.0	.0	.0
45.	.0	.3	.1	.1	.0	.0	.0	.0
50.	.0	.2	.1	.1	.1	.0	.0	.0
55.	.0	.2	.1	.1	.1	.0	.0	.0
60.	.1	.2	.1	.1	.1	.0	.0	.0
65.	.1	.1	.1	.0	.1	.0	.0	.0
70.	.1	.1	.0	.0	.1	.0	.0	.0
75.	.1	.1	.0	.0	.0	.0	.0	.0
80.	.1	.0	.0	.0	.0	.0	.0	.0
85.	.2	.0	.0	.0	.0	.0	.0	.0
90.	.2	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.1	.0	.0	.0	.0	.0	.0	.0
105.	.1	.0	.0	.0	.0	.0	.0	.0
110.	.1	.0	.0	.0	.0	.0	.0	.0
115.	.1	.0	.0	.0	.0	.0	.0	.0
120.	.1	.0	.0	.0	.0	.0	.0	.0
125.	.1	.0	.0	.0	.0	.0	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT) RUN: Site 2 NO BUILD PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.2	.1	.2	.0	.0	.0	.0
255.	.0	.2	.2	.2	.1	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.3	.2	.2	.2	.0	.0	.0
275.	.0	.3	.2	.2	.2	.0	.0	.0
280.	.0	.3	.2	.3	.3	.0	.0	.0
285.	.0	.3	.3	.3	.2	.0	.0	.0
290.	.0	.3	.3	.3	.2	.0	.0	.0
295.	.0	.2	.3	.3	.2	.0	.0	.0
300.	.0	.2	.3	.3	.2	.0	.0	.0
305.	.0	.2	.3	.3	.2	.0	.0	.0
310.	.0	.1	.3	.3	.2	.0	.0	.0
315.	.0	.1	.3	.2	.2	.0	.0	.0
320.	.0	.1	.2	.2	.2	.0	.0	.0
325.	.0	.1	.2	.2	.2	.0	.0	.0
330.	.0	.1	.2	.2	.1	.0	.0	.0
335.	.0	.2	.2	.2	.1	.0	.0	.0
340.	.0	.3	.2	.2	.1	.0	.0	.0
345.	.0	.3	.2	.2	.1	.0	.0	.0
350.	.0	.3	.2	.2	.1	.0	.0	.0
355.	.0	.3	.2	.2	.1	.0	.0	.0
360.	.0	.3	.2	.2	.1	.0	.0	.0
MAX	.2	.3	.3	.3	.3	.0	.0	.0
DEGR.	85	0	10	280	280	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 0 DEGREES FROM REC22.

JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT) RUN: Site 2 BUILD ALT1 AM
DATE: 03/19/2010 TIME: 09:06:37.27

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	5595.	.8	.0	68.0		
2. EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	5595.	.8	.0	68.0		
3. EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	4672.	.8	.0	68.0		
4. EB Wil T+R Q	678.0	822.0	-5486.7	-1304.3	6521.	251.	AG	17.	100.0	.0	48.0	2.06	331.3
5. EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	923.	.8	.0	44.0		
6. EB Wil LT Q	659.0	855.0	-4349.7	-787.0	5271.	252.	AG	17.	100.0	.0	24.0	****	267.8
7. EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	4826.	.8	.0	68.0		
8. WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	3179.	.8	.0	68.0		
9. WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	3160.	.8	.0	68.0		
10. WB Wil T+R Q	798.0	946.0	4867.3	2248.2	4273.	72.	AG	25.	100.0	.0	48.0	1.92	217.0
11. WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	19.	.8	.0	44.0		
12. WB Wil LT Q	824.0	908.0	948.3	946.0	130.	73.	AG	21.	100.0	.0	24.0	9.00	6.6
13. WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3487.	.8	.0	68.0		
14. WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3487.	.8	.0	68.0		
15. NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	959.	.9	.0	32.0		
16. NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	827.	.9	.0	56.0		
17. NB Vet T+LT Q	820.0	783.0	1292.3	93.6	836.	146.	AG	24.	100.0	.0	36.0	1.27	42.5
18. NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	132.	.9	.0	32.0		
19. NB Vet RT Q	847.0	791.0	889.6	729.2	75.	145.	AG	8.	100.0	.0	12.0	.53	3.8
20. NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1751.	.9	.0	44.0		
21. NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1751.	.9	.0	44.0		
22. SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1151.	.9	.0	44.0		
23. SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	820.	.9	.0	56.0		
24. SB Vet T+LT Q	679.0	981.0	-122.4	2271.1	1519.	328.	AG	26.	100.0	.0	36.0	1.84	77.2
25. SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	331.	.9	.0	44.0		
26. SB Vet RT Q	643.0	972.0	600.2	1041.0	81.	328.	AG	13.	100.0	.0	24.0	.53	4.1
27. SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	817.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT) RUN: Site 2 BUILD ALT1 AM
DATE: 03/19/2010 TIME: 09:06:37.27

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4. EB Wil T+R Q	150	59	2.0	4672	981	4.10	1	3
6. EB Wil LT Q	150	118	2.0	923	84	4.10	1	3
10. WB Wil T+R Q	150	84	2.0	3160	997	4.10	1	3
12. WB Wil LT Q	150	143	2.0	19	84	4.10	1	3
17. NB Vet T+LT Q	150	109	2.0	827	877	4.10	1	3
19. NB Vet RT Q	150	104	2.0	132	885	4.10	1	3
24. SB Vet T+LT Q	150	120	2.0	820	858	4.10	1	3
26. SB Vet RT Q	150	90	2.0	331	834	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	1066.0	492.0	5.0
2. SE 164 S	942.0	686.0	5.0
3. SE 82 S	892.0	756.0	5.0
4. SE CNR	869.0	821.0	5.0
5. SE 82 E	925.0	853.0	5.0
6. SE 164 E	1005.0	880.0	5.0
7. SE MID E	1219.0	947.0	5.0
8. NE MID E	1144.0	1099.0	5.0
9. NE 164 E	918.0	1026.0	5.0
10. NE 82 E	838.0	1000.0	5.0
11. NE CNR	759.0	983.0	5.0
12. NE 82 N	716.0	1047.0	5.0
13. NE 164 N	676.0	1120.0	5.0
14. NE MID N	595.0	1269.0	5.0
15. NW MID N	464.0	1209.0	5.0
16. NW 164 N	546.0	1079.0	5.0
17. NW 82 N	589.0	1010.0	5.0
18. NW CNR	611.0	945.0	5.0
19. NW 82 W	552.0	910.0	5.0
20. NW 164 W	475.0	884.0	5.0
21. NW MID W	273.0	815.0	5.0
22. SW MID W	305.0	649.0	5.0
23. SW 164 W	565.0	737.0	5.0
24. SW 82 W	645.0	764.0	5.0
25. SW CNR	718.0	779.0	5.0
26. SW 82 S	774.0	718.0	5.0
27. SW 164 S	824.0	646.0	5.0

28. SW MID S * 957.0 459.0 5.0 *

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JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT) RUN: Site 2 BUILD ALT1 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
15.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
20.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
25.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	* .0	.0	.1	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	* .0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	* .0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	* .0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	* .0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
75.	* .0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	* .0	.0	.0	.0	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85.	* .0	.0	.0	.0	.0	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90.	* .0	.0	.0	.0	.0	.0	.0	.2	.4	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
100.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.1	.0	.0	.1	.1
105.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
110.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
115.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.2
120.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
125.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
130.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.2
135.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2
140.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
145.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
150.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
155.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
160.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.0	.1	.0	.0	.0	.0	.1	.2	.2
165.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
170.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
175.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
180.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
185.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
190.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
195.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
200.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
205.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2

1

JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT) RUN: Site 2 BUILD ALT1 AM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1
215.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
220.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
225.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
230.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240.	* .1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	* .1	.1	.1	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	* .1	.1	.1	.0	.0	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
255.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	* .1	.1	.1	.1	.2	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	* .1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	* .1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	* .1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
290.	* .1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
295.	* .1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
300.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0
305.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
310.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
315.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
320.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
325.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0

340.	*	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
345.	*	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
350.	*	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
355.	*	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
360.	*	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	*	.1	.1	.1	.2	.2	.2	.2	.3	.4	.3	.3	.2	.1	.1	.1	.1	.1	.2	.2	.2
DEGR.	*	150	150	0	280	50	50	55	95	90	85	90	285	160	305	0	0	0	205	135	115

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JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT) RUN: Site 2 BUILD ALT1 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	*	.0	.1	.1	.1	.1	.0	.0	.0
5.	*	.0	.1	.1	.1	.1	.0	.0	.0
10.	*	.0	.1	.1	.1	.1	.0	.0	.0
15.	*	.0	.1	.1	.1	.1	.0	.0	.0
20.	*	.0	.1	.1	.1	.1	.0	.0	.0
25.	*	.0	.1	.1	.1	.1	.1	.0	.0
30.	*	.0	.2	.1	.1	.1	.1	.0	.0
35.	*	.0	.2	.1	.1	.1	.1	.0	.0
40.	*	.0	.2	.1	.1	.2	.1	.0	.0
45.	*	.0	.2	.1	.1	.2	.1	.0	.0
50.	*	.0	.2	.1	.1	.1	.1	.0	.0
55.	*	.0	.2	.1	.2	.1	.1	.0	.0
60.	*	.0	.1	.1	.2	.1	.1	.0	.0
65.	*	.1	.1	.2	.2	.1	.0	.0	.0
70.	*	.1	.1	.2	.2	.1	.0	.0	.0
75.	*	.1	.1	.1	.1	.1	.0	.0	.0
80.	*	.1	.1	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.2	.0	.0	.0	.0	.0	.0	.0
100.	*	.2	.0	.0	.0	.0	.0	.0	.0
105.	*	.2	.0	.0	.0	.0	.0	.0	.0
110.	*	.2	.0	.0	.0	.0	.0	.0	.0
115.	*	.2	.0	.0	.0	.0	.0	.0	.0
120.	*	.2	.0	.0	.0	.0	.0	.0	.0
125.	*	.2	.0	.0	.0	.0	.0	.0	.0
130.	*	.2	.0	.0	.0	.0	.0	.0	.0
135.	*	.2	.0	.0	.0	.0	.0	.0	.0
140.	*	.2	.0	.0	.0	.0	.0	.0	.0
145.	*	.2	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.2	.0	.0	.0	.0	.0	.0	.0
205.	*	.2	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT) RUN: Site 2 BUILD ALT1 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.2	.0	.0	.0	.0	.0	.0	.0
215.	*	.2	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.2	.0	.0	.0	.0	.0	.0	.0
235.	*	.2	.0	.0	.0	.0	.0	.0	.0
240.	*	.2	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.1	.0	.0	.0	.0
250.	*	.0	.2	.1	.1	.1	.0	.0	.0
255.	*	.0	.2	.2	.2	.1	.0	.0	.0
260.	*	.0	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.1	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.1	.0	.0
285.	*	.0	.2	.2	.2	.1	.1	.0	.0

290.	*	.0	.2	.2	.2	.1	.1	.0	.0
295.	*	.0	.2	.1	.1	.1	.1	.0	.0
300.	*	.0	.1	.1	.1	.1	.1	.0	.0
305.	*	.0	.1	.1	.1	.1	.1	.0	.0
310.	*	.0	.1	.1	.1	.1	.1	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.2	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.1	.0	.0	.0
MAX	*	.2	.2	.2	.2	.2	.1	.0	.0
DEGR.	*	95	30	65	55	40	25	0	0

THE HIGHEST CONCENTRATION IS .40 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 95 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT) RUN: Site 2 BUILD ALT1 PM
DATE: 03/21/2010 TIME: 22:20:17.29

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	3430.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	3430.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	3138.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-2096.1	-134.8	2934.	251.	AG	19.	100.0	.0	48.0	1.48	149.1
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	292.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-925.3	335.6	1667.	252.	AG	19.	100.0	.0	24.0	****	84.7
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	3339.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	4302.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	4286.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	7629.1	3132.0	7172.	72.	AG	24.	100.0	.0	48.0	2.57	364.4
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	16.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	933.5	941.5	114.	73.	AG	21.	100.0	.0	24.0	8.00	5.8
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	4930.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	4930.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	1373.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	1090.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1686.5	-482.0	1533.	146.	AG	22.	100.0	.0	36.0	1.52	77.9
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	283.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	959.2	628.0	198.	145.	AG	7.	100.0	.0	12.0	.94	10.1
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1841.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1841.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1997.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	894.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	262.7	1651.2	789.	328.	AG	24.	100.0	.0	36.0	1.26	40.1
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	1103.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	-894.5	3450.6	2917.	328.	AG	13.	100.0	.0	24.0	1.85	148.2
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	992.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT) RUN: Site 2 BUILD ALT1 PM
DATE: 03/21/2010 TIME: 22:20:17.29

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	65	2.0	3138	984	4.10	1	3
6.	EB Wil LT Q	150	128	2.0	292	84	4.10	1	3
10.	WB Wil T+R Q	150	82	2.0	4286	979	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	16	84	4.10	1	3
17.	NB Vet T+LT Q	150	100	2.0	1090	782	4.10	1	3
19.	NB Vet RT Q	150	95	2.0	283	885	4.10	1	3
24.	SB Vet T+LT Q	150	109	2.0	800	858	4.10	1	3
26.	SB Vet RT Q	150	90	2.0	1103	800	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

1 PAGE 3

JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT) RUN: Site 2 BUILD ALT1 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
10.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75.	.0	.0	.0	.0	.1	.1	.1	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	.0	.0	.0	.0	.1	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
155.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
170.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
175.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
180.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
185.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
190.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
195.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
200.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
205.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.2	.1	.0	.0	.0	.1	.1	.1	.1

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JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT) RUN: Site 2 BUILD ALT1 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
215.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
220.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
225.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
230.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
235.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
240.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255.	.1	.0	.0	.0	.0	.1	.1	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
290.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
295.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0
300.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.1	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.1	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.0	.1	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
340.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
350.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.1	.1	.2	.2	.2	.3	.3	.2	.2	.1	.1	.1	.2	.2	.2	.2	.1
DEGR.	145	150	150	0	0	40	30	70	75	75	75	205	160	295	0	345	345	95	230	65

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JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT) RUN: Site 2 BUILD ALT1 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.0	.0
5.	.0	.2	.2	.1	.1	.0	.0	.0
10.	.0	.2	.2	.1	.1	.0	.0	.0
15.	.0	.3	.2	.1	.1	.0	.0	.0
20.	.0	.3	.2	.1	.1	.0	.0	.0
25.	.0	.3	.2	.1	.1	.0	.0	.0
30.	.0	.3	.2	.1	.1	.0	.0	.0
35.	.0	.3	.2	.1	.0	.0	.0	.0
40.	.0	.3	.1	.1	.0	.0	.0	.0
45.	.0	.3	.1	.1	.0	.0	.0	.0
50.	.0	.2	.1	.1	.1	.0	.0	.0
55.	.0	.2	.1	.1	.1	.0	.0	.0
60.	.1	.2	.1	.1	.1	.0	.0	.0
65.	.1	.1	.1	.0	.1	.0	.0	.0
70.	.1	.1	.0	.0	.1	.0	.0	.0
75.	.1	.1	.0	.0	.0	.0	.0	.0
80.	.1	.0	.0	.0	.0	.0	.0	.0
85.	.2	.0	.0	.0	.0	.0	.0	.0
90.	.2	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.1	.0	.0	.0	.0	.0	.0	.0
105.	.1	.0	.0	.0	.0	.0	.0	.0
110.	.1	.0	.0	.0	.0	.0	.0	.0
115.	.1	.0	.0	.0	.0	.0	.0	.0
120.	.1	.0	.0	.0	.0	.0	.0	.0
125.	.1	.0	.0	.0	.0	.0	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT) RUN: Site 2 BUILD ALT1 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.2	.0	.1	.0	.0	.0	.0
255.	.0	.2	.2	.2	.2	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.3	.2	.2	.2	.0	.0	.0
275.	.0	.3	.2	.2	.2	.0	.0	.0
280.	.0	.3	.2	.3	.2	.0	.0	.0
285.	.0	.3	.3	.3	.2	.0	.0	.0
290.	.0	.2	.3	.3	.2	.0	.0	.0
295.	.0	.2	.3	.3	.2	.0	.0	.0
300.	.0	.2	.3	.3	.2	.0	.0	.0
305.	.0	.2	.3	.2	.2	.0	.0	.0
310.	.0	.1	.2	.2	.2	.0	.0	.0
315.	.0	.0	.2	.2	.2	.0	.0	.0
320.	.0	.0	.2	.2	.2	.0	.0	.0
325.	.0	.0	.2	.2	.1	.0	.0	.0
330.	.0	.0	.2	.2	.1	.0	.0	.0
335.	.0	.1	.2	.2	.1	.0	.0	.0
340.	.0	.2	.2	.2	.1	.0	.0	.0
345.	.0	.2	.2	.2	.1	.0	.0	.0
350.	.0	.2	.2	.2	.1	.0	.0	.0
355.	.0	.2	.2	.2	.1	.0	.0	.0
360.	.0	.2	.2	.2	.1	.0	.0	.0
MAX	.2	.3	.3	.3	.2	.0	.0	.0
DEGR.	85	15	285	280	255	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 15 DEGREES FROM REC22.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT) RUN: Site 2 BUILD ALT2 AM
DATE: 03/19/2010 TIME: 13:25:51.13

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	5509.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	5509.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	4596.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-5231.7	-1216.4	6251.	251.	AG	17.	100.0	.0	48.0	2.00	317.6
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	913.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-4293.8	-768.7	5212.	252.	AG	17.	100.0	.0	24.0	****	264.8
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	4761.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	3138.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	3121.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	4643.8	2176.7	4038.	72.	AG	24.	100.0	.0	48.0	1.84	205.1
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	17.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	933.5	941.5	114.	73.	AG	21.	100.0	.0	24.0	8.00	5.8
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3409.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3409.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	947.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	815.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1320.7	52.0	886.	146.	AG	24.	100.0	.0	36.0	1.31	45.0
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	132.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	890.4	728.0	77.	145.	AG	8.	100.0	.0	12.0	.51	3.9
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1755.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1755.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1085.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	767.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	-24.3	2113.1	1333.	328.	AG	26.	100.0	.0	36.0	1.73	67.7
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	318.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	601.8	1038.5	78.	328.	AG	13.	100.0	.0	24.0	.51	4.0
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	751.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT) RUN: Site 2 BUILD ALT2 AM
DATE: 03/19/2010 TIME: 13:25:51.13

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	57	2.0	4596	969	4.10	1	3
6.	EB Wil LT Q	150	118	2.0	913	84	4.10	1	3
10.	WB Wil T+R Q	150	82	2.0	3121	995	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	17	84	4.10	1	3
17.	NB Vet T+LT Q	150	111	2.0	815	888	4.10	1	3
19.	NB Vet RT Q	150	106	2.0	132	967	4.10	1	3
24.	SB Vet T+LT Q	150	120	2.0	767	852	4.10	1	3
26.	SB Vet RT Q	150	90	2.0	318	837	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

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JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT) RUN: Site 2 BUILD ALT2 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
15.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
20.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
25.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.1	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
75.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	.0	.0	.0	.0	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85.	.0	.0	.0	.0	.0	.1	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.1	.0	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
120.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
125.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
145.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
150.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
155.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
160.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.0	.1	.0	.0	.0	.0	.1	.2	.2
165.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
170.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
175.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
180.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.2
185.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
190.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
195.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
200.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
205.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
215.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
220.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
225.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
230.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240.	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.1	.1	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.1	.1	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
255.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.1	.1	.1	.2	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
290.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
295.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
300.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
320.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
340.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
345.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
350.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
355.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
360.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.2	.2	.2	.2	.3	.3	.3	.3	.2	.1	.1	.1	.1	.1	.1	.2	.2
DEGR.	150	150	0	285	50	50	55	95	85	90	90	285	160	305	0	0	0	90	140	115

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.1	.0	.0	.0
5.	.0	.1	.1	.1	.1	.0	.0	.0
10.	.0	.1	.1	.1	.1	.0	.0	.0
15.	.0	.1	.1	.1	.1	.0	.0	.0
20.	.0	.1	.1	.1	.1	.0	.0	.0
25.	.0	.1	.1	.1	.1	.0	.0	.0
30.	.0	.1	.1	.1	.1	.1	.0	.0
35.	.0	.2	.1	.1	.1	.1	.0	.0
40.	.0	.2	.1	.1	.1	.1	.0	.0
45.	.0	.2	.1	.1	.2	.1	.0	.0
50.	.0	.2	.1	.1	.1	.1	.0	.0
55.	.0	.2	.1	.2	.1	.1	.0	.0
60.	.0	.1	.1	.2	.1	.1	.0	.0
65.	.1	.1	.2	.2	.1	.0	.0	.0
70.	.1	.1	.2	.2	.1	.0	.0	.0
75.	.1	.1	.1	.1	.1	.0	.0	.0
80.	.1	.1	.0	.0	.0	.0	.0	.0
85.	.1	.0	.0	.0	.0	.0	.0	.0
90.	.1	.0	.0	.0	.0	.0	.0	.0
95.	.1	.0	.0	.0	.0	.0	.0	.0
100.	.2	.0	.0	.0	.0	.0	.0	.0
105.	.2	.0	.0	.0	.0	.0	.0	.0
110.	.2	.0	.0	.0	.0	.0	.0	.0
115.	.2	.0	.0	.0	.0	.0	.0	.0
120.	.2	.0	.0	.0	.0	.0	.0	.0
125.	.2	.0	.0	.0	.0	.0	.0	.0
130.	.2	.0	.0	.0	.0	.0	.0	.0
135.	.2	.0	.0	.0	.0	.0	.0	.0
140.	.2	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT) RUN: Site 2 BUILD ALT2 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.1	.1	.0	.1	.0	.0	.0	.0
250.	.0	.1	.1	.1	.1	.0	.0	.0
255.	.0	.2	.2	.2	.1	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.2	.2	.2	.2	.0	.0	.0
275.	.0	.2	.2	.2	.1	.0	.0	.0
280.	.0	.2	.2	.2	.1	.1	.0	.0
285.	.0	.2	.2	.2	.1	.1	.0	.0
290.	.0	.2	.1	.1	.1	.1	.0	.0
295.	.0	.1	.1	.1	.1	.1	.0	.0
300.	.0	.1	.1	.1	.1	.1	.0	.0
305.	.0	.1	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.2	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.1	.0	.0	.0
340.	.0	.1	.1	.1	.1	.0	.0	.0
345.	.0	.1	.1	.1	.1	.0	.0	.0
350.	.0	.1	.1	.1	.1	.0	.0	.0
355.	.0	.1	.1	.1	.1	.0	.0	.0
360.	.0	.1	.1	.1	.1	.0	.0	.0
MAX	.2	.2	.2	.2	.2	.1	.0	.0
DEGR.	100	35	65	55	45	30	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 95 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 90 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT) RUN: Site 2 BUILD ALT2 PM
DATE: 03/21/2010 TIME: 22:20:39.42

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	3358.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	3358.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	3074.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-2336.8	-217.9	3189.	251.	AG	21.	100.0	.0	48.0	1.56	162.0
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	284.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-925.0	335.7	1667.	252.	AG	19.	100.0	.0	24.0	****	84.7
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	3319.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	4364.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	4346.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	7769.9	3177.0	7320.	72.	AG	24.	100.0	.0	48.0	2.60	371.9
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	18.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	948.3	946.0	130.	73.	AG	21.	100.0	.0	24.0	9.00	6.6
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	5006.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	5006.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	1384.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	1053.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1455.0	-144.1	1124.	146.	AG	21.	100.0	.0	36.0	1.32	57.1
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	331.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	1009.6	554.8	287.	145.	AG	7.	100.0	.0	12.0	1.01	14.6
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1795.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1795.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	2004.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	886.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	39.2	2010.9	1212.	328.	AG	24.	100.0	.0	36.0	1.48	61.6
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	1118.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	-916.4	3485.8	2958.	328.	AG	13.	100.0	.0	24.0	1.85	150.3
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	990.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT) RUN: Site 2 BUILD ALT2 PM
DATE: 03/21/2010 TIME: 22:20:39.42

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	70	2.0	3074	971	4.10	1	3
6.	EB Wil LT Q	150	131	2.0	284	84	4.10	1	3
10.	WB Wil T+R Q	150	82	2.0	4346	981	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	18	84	4.10	1	3
17.	NB Vet T+LT Q	150	95	2.0	1053	784	4.10	1	3
19.	NB Vet RT Q	150	93	2.0	331	929	4.10	1	3
24.	SB Vet T+LT Q	150	109	2.0	886	812	4.10	1	3
26.	SB Vet RT Q	150	89	2.0	1118	797	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

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JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT) RUN: Site 2 BUILD ALT2 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	* .0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	* .0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	* .0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	* .0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	* .0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	* .0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	* .0	.0	.0	.1	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70.	* .0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75.	* .0	.0	.0	.0	.1	.1	.1	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	* .0	.0	.0	.0	.1	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
85.	* .0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
90.	* .0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	* .0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
100.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
105.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1
125.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
150.	* .1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
155.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
160.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
165.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
170.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
175.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
180.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
185.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
190.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
195.	* .1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
200.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
205.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.2	.0	.0	.0	.0	.1	.1	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
215.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
220.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
225.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
230.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
235.	* .1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
240.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	* .1	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255.	* .1	.0	.0	.0	.0	.1	.1	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	* .1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	* .1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	* .1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
285.	* .1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
290.	* .1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
295.	* .1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
300.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0
305.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
310.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
315.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0
320.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
340.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
345.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
350.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	* .1	.1	.1	.1	.1	.2	.2	.2	.3	.3	.2	.2	.1	.1	.2	.2	.2	.2	.2	.1
DEGR.	* 150	155	150	0	0	35	25	70	75	75	75	205	160	305	340	340	340	95	230	65

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.3	.3	.2	.1	.0	.0	.0
5.	.0	.3	.3	.1	.1	.0	.0	.0
10.	.0	.3	.3	.1	.1	.0	.0	.0
15.	.0	.3	.3	.1	.1	.0	.0	.0
20.	.0	.3	.3	.1	.1	.0	.0	.0
25.	.0	.3	.2	.1	.1	.0	.0	.0
30.	.0	.3	.2	.1	.1	.0	.0	.0
35.	.0	.3	.2	.1	.0	.0	.0	.0
40.	.0	.3	.2	.1	.0	.0	.0	.0
45.	.0	.3	.1	.1	.0	.0	.0	.0
50.	.0	.2	.1	.1	.1	.0	.0	.0
55.	.0	.2	.1	.1	.1	.0	.0	.0
60.	.1	.2	.1	.1	.1	.0	.0	.0
65.	.1	.1	.1	.0	.1	.0	.0	.0
70.	.1	.1	.0	.0	.1	.0	.0	.0
75.	.1	.1	.0	.0	.0	.0	.0	.0
80.	.1	.0	.0	.0	.0	.0	.0	.0
85.	.2	.0	.0	.0	.0	.0	.0	.0
90.	.2	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.1	.0	.0	.0	.0	.0	.0	.0
105.	.1	.0	.0	.0	.0	.0	.0	.0
110.	.1	.0	.0	.0	.0	.0	.0	.0
115.	.1	.0	.0	.0	.0	.0	.0	.0
120.	.1	.0	.0	.0	.0	.0	.0	.0
125.	.1	.0	.0	.0	.0	.0	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT) RUN: Site 2 BUILD ALT2 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.2	.1	.2	.0	.0	.0	.0
255.	.0	.2	.2	.2	.1	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.3	.2	.2	.2	.0	.0	.0
275.	.0	.3	.2	.2	.2	.0	.0	.0
280.	.0	.3	.2	.3	.3	.0	.0	.0
285.	.0	.3	.3	.3	.2	.0	.0	.0
290.	.0	.3	.3	.3	.2	.0	.0	.0
295.	.0	.2	.3	.3	.2	.0	.0	.0
300.	.0	.2	.3	.3	.2	.0	.0	.0
305.	.0	.2	.3	.3	.2	.0	.0	.0
310.	.0	.1	.3	.3	.2	.0	.0	.0
315.	.0	.1	.3	.3	.2	.0	.0	.0
320.	.0	.1	.3	.3	.2	.0	.0	.0
325.	.0	.1	.3	.3	.2	.0	.0	.0
330.	.0	.1	.3	.3	.2	.0	.0	.0
335.	.0	.2	.3	.3	.1	.0	.0	.0
340.	.0	.3	.3	.3	.1	.0	.0	.0
345.	.0	.3	.3	.3	.1	.0	.0	.0
350.	.0	.3	.3	.2	.1	.0	.0	.0
355.	.0	.3	.3	.2	.1	.0	.0	.0
360.	.0	.3	.3	.2	.1	.0	.0	.0
MAX	.2	.3	.3	.3	.3	.0	.0	.0
DEGR.	85	0	0	280	280	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 0 DEGREES FROM REC22.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT) RUN: Site 2 BUILD ALT3 AM
DATE: 03/21/2010 TIME: 21:46:22.13

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	5495.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	5495.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	4593.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-5221.9	-1213.0	6241.	251.	AG	17.	100.0	.0	48.0	2.00	317.0
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	902.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-4238.0	-750.3	5153.	252.	AG	17.	100.0	.0	24.0	****	261.8
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	4799.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	3158.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	3142.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	4693.9	2192.7	4091.	72.	AG	24.	100.0	.0	48.0	1.85	207.8
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	16.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	933.5	941.5	114.	73.	AG	21.	100.0	.0	24.0	8.00	5.8
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3429.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3429.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	932.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	800.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1191.3	241.0	657.	146.	AG	24.	100.0	.0	36.0	1.19	33.4
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	132.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	890.4	728.0	77.	145.	AG	8.	100.0	.0	12.0	.52	3.9
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1754.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1754.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1134.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	795.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	-81.8	2205.7	1442.	328.	AG	26.	100.0	.0	36.0	1.80	73.2
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	339.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	599.2	1042.7	83.	328.	AG	13.	100.0	.0	24.0	.53	4.2
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	737.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT) RUN: Site 2 BUILD ALT3 AM
DATE: 03/21/2010 TIME: 21:46:22.13

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	57	2.0	4593	969	4.10	1	3
6.	EB Wil LT Q	150	118	2.0	902	84	4.10	1	3
10.	WB Wil T+R Q	150	82	2.0	3142	995	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	16	84	4.10	1	3
17.	NB Vet T+LT Q	150	108	2.0	800	885	4.10	1	3
19.	NB Vet RT Q	150	106	2.0	132	959	4.10	1	3
24.	SB Vet T+LT Q	150	120	2.0	795	853	4.10	1	3
26.	SB Vet RT Q	150	90	2.0	339	859	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

1 PAGE 3

JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT) RUN: Site 2 BUILD ALT3 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
15.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
20.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
25.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	* .0	.0	.1	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	* .0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	* .0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	* .0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	* .0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
75.	* .0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	* .0	.0	.0	.0	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85.	* .0	.0	.0	.0	.0	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90.	* .0	.0	.0	.0	.0	.0	.0	.2	.4	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
100.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.1	.0	.0	.1	.1
105.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
110.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
115.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
120.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
125.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.1
130.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
145.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
150.	* .0	.0	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
155.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
160.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.0	.1	.0	.0	.0	.0	.1	.2	.2
165.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
170.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
175.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
180.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.2
185.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
190.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
195.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
200.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
205.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2

1

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
215.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
220.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
225.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
230.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240.	* .1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	* .1	.1	.1	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	* .1	.1	.1	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
255.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	* .1	.1	.1	.1	.2	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	* .1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	* .1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	* .1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
290.	* .1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
295.	* .1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
300.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
305.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
310.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
315.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
320.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
325.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
340.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
345.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
350.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
355.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
360.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	* .1	.1	.1	.2	.2	.2	.2	.3	.4	.3	.3	.2	.1	.1	.1	.1	.1	.1	.2	.2
DEGR.	* 155	155	0	280	50	50	55	95	90	85	90	285	160	305	0	0	0	90	140	115

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	*	.0	.1	.1	.1	.1	.0	.0	.0
5.	*	.0	.1	.1	.1	.1	.0	.0	.0
10.	*	.0	.1	.1	.1	.1	.0	.0	.0
15.	*	.0	.1	.1	.1	.1	.0	.0	.0
20.	*	.0	.1	.1	.1	.1	.0	.0	.0
25.	*	.0	.1	.1	.1	.1	.1	.0	.0
30.	*	.0	.1	.1	.1	.1	.1	.0	.0
35.	*	.0	.2	.1	.1	.1	.1	.0	.0
40.	*	.0	.2	.1	.1	.1	.1	.0	.0
45.	*	.0	.2	.1	.1	.2	.1	.0	.0
50.	*	.0	.2	.1	.1	.1	.1	.0	.0
55.	*	.0	.2	.1	.2	.1	.1	.0	.0
60.	*	.0	.1	.1	.2	.1	.1	.0	.0
65.	*	.1	.1	.2	.2	.1	.0	.0	.0
70.	*	.1	.1	.2	.2	.1	.0	.0	.0
75.	*	.1	.1	.1	.1	.1	.0	.0	.0
80.	*	.1	.1	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.2	.0	.0	.0	.0	.0	.0	.0
105.	*	.2	.0	.0	.0	.0	.0	.0	.0
110.	*	.2	.0	.0	.0	.0	.0	.0	.0
115.	*	.2	.0	.0	.0	.0	.0	.0	.0
120.	*	.2	.0	.0	.0	.0	.0	.0	.0
125.	*	.2	.0	.0	.0	.0	.0	.0	.0
130.	*	.2	.0	.0	.0	.0	.0	.0	.0
135.	*	.2	.0	.0	.0	.0	.0	.0	.0
140.	*	.2	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.2	.0	.0	.0	.0	.0	.0	.0
205.	*	.2	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT) RUN: Site 2 BUILD ALT3 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.2	.0	.0	.0	.0	.0	.0	.0
215.	*	.2	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.2	.0	.0	.0	.0	.0	.0	.0
235.	*	.2	.0	.0	.0	.0	.0	.0	.0
240.	*	.2	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.1	.0	.0	.0	.0
250.	*	.0	.1	.1	.1	.1	.0	.0	.0
255.	*	.0	.2	.2	.2	.1	.0	.0	.0
260.	*	.0	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.1	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.1	.0	.0
285.	*	.0	.2	.2	.2	.1	.1	.0	.0
290.	*	.0	.2	.1	.1	.1	.1	.0	.0
295.	*	.0	.1	.1	.1	.1	.1	.0	.0
300.	*	.0	.1	.1	.1	.1	.1	.0	.0
305.	*	.0	.1	.1	.1	.1	.0	.0	.0
310.	*	.0	.1	.1	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.2	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.1	.0	.0	.0
MAX	*	.2	.2	.2	.2	.2	.1	.0	.0
DEGR.	*	100	35	65	55	45	25	0	0

THE HIGHEST CONCENTRATION IS .40 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 95 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT) RUN: Site 2 BUILD ALT3 PM
DATE: 03/21/2010 TIME: 22:20:55.63

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	3401.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	3401.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	3112.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-2266.6	-193.6	3115.	251.	AG	20.	100.0	.0	48.0	1.53	158.2
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	289.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-901.6	343.4	1642.	252.	AG	19.	100.0	.0	24.0	****	83.4
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	3325.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	4274.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	4256.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	7612.8	3126.7	7155.	72.	AG	24.	100.0	.0	48.0	2.58	363.5
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	18.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	948.3	946.0	130.	73.	AG	21.	100.0	.0	24.0	9.00	6.6
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	4918.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	4918.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	1362.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	1091.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1697.9	-498.6	1553.	146.	AG	22.	100.0	.0	36.0	1.53	78.9
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	271.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	938.2	658.5	161.	145.	AG	7.	100.0	.0	12.0	.85	8.2
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1792.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1792.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1983.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	912.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	-28.0	2119.1	1340.	328.	AG	24.	100.0	.0	36.0	1.54	68.1
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	1074.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	-749.2	3216.4	2641.	328.	AG	13.	100.0	.0	24.0	1.73	134.2
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	985.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT) RUN: Site 2 BUILD ALT3 PM
DATE: 03/21/2010 TIME: 22:20:55.63

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	68	2.0	3112	977	4.10	1	3
6.	EB Wil LT Q	150	127	2.0	289	84	4.10	1	3
10.	WB Wil T+R Q	150	83	2.0	4256	982	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	18	84	4.10	1	3
17.	NB Vet T+LT Q	150	100	2.0	1091	776	4.10	1	3
19.	NB Vet RT Q	150	95	2.0	271	933	4.10	1	3
24.	SB Vet T+LT Q	150	109	2.0	912	800	4.10	1	3
26.	SB Vet RT Q	150	88	2.0	1074	804	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

1 PAGE 3

JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT) RUN: Site 2 BUILD ALT3 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75.	.0	.0	.0	.0	.1	.1	.1	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.1	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
85.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
155.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
170.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
175.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
180.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
185.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
190.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
195.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
200.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
205.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1

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JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT) RUN: Site 2 BUILD ALT3 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
215.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
220.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
225.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
230.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1
235.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
240.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.0	.0	.0	.0	.0	.1	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255.	.1	.0	.0	.0	.0	.1	.1	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
290.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
295.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
300.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
345.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
350.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.1	.1	.2	.2	.2	.3	.3	.2	.2	.1	.1	.1	.2	.2	.2	.2	.1
DEGR.	145	150	150	0	0	40	30	70	75	75	75	300	160	305	0	340	340	80	235	65

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JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT) RUN: Site 2 BUILD ALT3 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.3	.2	.2	.1	.0	.0	.0
5.	.0	.3	.2	.1	.1	.0	.0	.0
10.	.0	.3	.3	.1	.1	.0	.0	.0
15.	.0	.3	.3	.1	.1	.0	.0	.0
20.	.0	.3	.2	.1	.1	.0	.0	.0
25.	.0	.3	.2	.1	.1	.0	.0	.0
30.	.0	.3	.2	.1	.1	.0	.0	.0
35.	.0	.3	.2	.1	.0	.0	.0	.0
40.	.0	.3	.2	.1	.0	.0	.0	.0
45.	.0	.3	.1	.1	.0	.0	.0	.0
50.	.0	.2	.1	.1	.1	.0	.0	.0
55.	.0	.2	.1	.1	.1	.0	.0	.0
60.	.1	.2	.1	.1	.1	.0	.0	.0
65.	.1	.1	.1	.0	.1	.0	.0	.0
70.	.1	.1	.0	.0	.1	.0	.0	.0
75.	.1	.1	.0	.0	.0	.0	.0	.0
80.	.1	.0	.0	.0	.0	.0	.0	.0
85.	.2	.0	.0	.0	.0	.0	.0	.0
90.	.2	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.1	.0	.0	.0	.0	.0	.0	.0
105.	.1	.0	.0	.0	.0	.0	.0	.0
110.	.1	.0	.0	.0	.0	.0	.0	.0
115.	.1	.0	.0	.0	.0	.0	.0	.0
120.	.1	.0	.0	.0	.0	.0	.0	.0
125.	.1	.0	.0	.0	.0	.0	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT) RUN: Site 2 BUILD ALT3 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.1	.2	.1	.2	.0	.0	.0	.0
255.	.0	.2	.2	.2	.2	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.3	.2	.2	.2	.0	.0	.0
275.	.0	.3	.2	.2	.2	.0	.0	.0
280.	.0	.3	.2	.3	.3	.0	.0	.0
285.	.0	.3	.3	.3	.2	.0	.0	.0
290.	.0	.2	.3	.3	.2	.0	.0	.0
295.	.0	.2	.3	.3	.2	.0	.0	.0
300.	.0	.2	.3	.3	.2	.0	.0	.0
305.	.0	.2	.3	.3	.2	.0	.0	.0
310.	.0	.1	.3	.3	.2	.0	.0	.0
315.	.0	.1	.3	.2	.2	.0	.0	.0
320.	.0	.1	.2	.2	.2	.0	.0	.0
325.	.0	.1	.2	.2	.1	.0	.0	.0
330.	.0	.1	.2	.2	.1	.0	.0	.0
335.	.0	.2	.2	.2	.1	.0	.0	.0
340.	.0	.3	.2	.2	.1	.0	.0	.0
345.	.0	.3	.2	.2	.1	.0	.0	.0
350.	.0	.3	.2	.2	.1	.0	.0	.0
355.	.0	.3	.2	.2	.1	.0	.0	.0
360.	.0	.3	.2	.2	.1	.0	.0	.0
MAX	.2	.3	.3	.3	.3	.0	.0	.0
DEGR.	85	0	10	280	280	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 0 DEGREES FROM REC22.

JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT) RUN: Site 2 BUILD ALT4 AM
DATE: 03/21/2010 TIME: 21:46:42.68

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	5553.	.8	.0	68.0		
2. EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	5553.	.8	.0	68.0		
3. EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	4635.	.8	.0	68.0		
4. EB Wil T+R Q	678.0	822.0	-5319.8	-1246.8	6345.	251.	AG	17.	100.0	.0	48.0	2.02	322.3
5. EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	918.	.8	.0	44.0		
6. EB Wil LT Q	659.0	855.0	-4327.3	-779.6	5247.	252.	AG	17.	100.0	.0	24.0	****	266.6
7. EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	4832.	.8	.0	68.0		
8. WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	3177.	.8	.0	68.0		
9. WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	3161.	.8	.0	68.0		
10. WB Wil T+R Q	798.0	946.0	4744.1	2208.7	4143.	72.	AG	24.	100.0	.0	48.0	1.86	210.5
11. WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	16.	.8	.0	44.0		
12. WB Wil LT Q	824.0	908.0	933.5	941.5	114.	73.	AG	21.	100.0	.0	24.0	8.00	5.8
13. WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3438.	.8	.0	68.0		
14. WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3438.	.8	.0	68.0		
15. NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	949.	.9	.0	32.0		
16. NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	817.	.9	.0	56.0		
17. NB Vet T+LT Q	820.0	783.0	1366.7	-15.1	967.	146.	AG	24.	100.0	.0	36.0	1.36	49.1
18. NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	132.	.9	.0	32.0		
19. NB Vet RT Q	847.0	791.0	890.4	728.0	77.	145.	AG	8.	100.0	.0	12.0	.52	3.9
20. NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1787.	.9	.0	44.0		
21. NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1787.	.9	.0	44.0		
22. SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1182.	.9	.0	44.0		
23. SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	853.	.9	.0	56.0		
24. SB Vet T+LT Q	679.0	981.0	-207.3	2407.7	1680.	328.	AG	26.	100.0	.0	36.0	1.97	85.3
25. SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	329.	.9	.0	44.0		
26. SB Vet RT Q	643.0	972.0	600.5	1040.6	81.	328.	AG	13.	100.0	.0	24.0	.53	4.1
27. SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	807.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT) RUN: Site 2 BUILD ALT4 AM
DATE: 03/21/2010 TIME: 21:46:42.68

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4. EB Wil T+R Q	150	57	2.0	4635	968	4.10	1	3
6. EB Wil LT Q	150	118	2.0	918	84	4.10	1	3
10. WB Wil T+R Q	150	82	2.0	3161	994	4.10	1	3
12. WB Wil LT Q	150	143	2.0	16	84	4.10	1	3
17. NB Vet T+LT Q	150	111	2.0	817	859	4.10	1	3
19. NB Vet RT Q	150	106	2.0	132	955	4.10	1	3
24. SB Vet T+LT Q	150	120	2.0	853	834	4.10	1	3
26. SB Vet RT Q	150	90	2.0	329	834	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	1066.0	492.0	5.0
2. SE 164 S	942.0	686.0	5.0
3. SE 82 S	892.0	756.0	5.0
4. SE CNR	869.0	821.0	5.0
5. SE 82 E	925.0	853.0	5.0
6. SE 164 E	1005.0	880.0	5.0
7. SE MID E	1219.0	947.0	5.0
8. NE MID E	1144.0	1099.0	5.0
9. NE 164 E	918.0	1026.0	5.0
10. NE 82 E	838.0	1000.0	5.0
11. NE CNR	759.0	983.0	5.0
12. NE 82 N	716.0	1047.0	5.0
13. NE 164 N	676.0	1120.0	5.0
14. NE MID N	595.0	1269.0	5.0
15. NW MID N	464.0	1209.0	5.0
16. NW 164 N	546.0	1079.0	5.0
17. NW 82 N	589.0	1010.0	5.0
18. NW CNR	611.0	945.0	5.0
19. NW 82 W	552.0	910.0	5.0
20. NW 164 W	475.0	884.0	5.0
21. NW MID W	273.0	815.0	5.0
22. SW MID W	305.0	649.0	5.0
23. SW 164 W	565.0	737.0	5.0
24. SW 82 W	645.0	764.0	5.0
25. SW CNR	718.0	779.0	5.0
26. SW 82 S	774.0	718.0	5.0
27. SW 164 S	824.0	646.0	5.0
28. SW MID S	957.0	459.0	5.0

1 PAGE 3

JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT) RUN: Site 2 BUILD ALT4 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
15.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
20.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
25.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.1	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
75.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	.0	.0	.0	.0	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85.	.0	.0	.0	.0	.0	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.4	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.1	.0	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
120.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
125.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
130.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.2
135.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2
140.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
145.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
150.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
155.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
160.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
165.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
170.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
175.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
180.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
185.	.1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
190.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
195.	.1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
200.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
205.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
215.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
220.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
225.	.1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
230.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240.	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.1	.1	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.1	.1	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
255.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.1	.1	.1	.2	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
290.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
295.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
300.	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.2	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
320.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
340.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
345.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
350.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
355.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
360.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.2	.2	.2	.2	.3	.4	.3	.3	.2	.1	.2	.1	.1	.1	.1	.2	.2
DEGR.	150	150	0	280	50	50	55	95	90	85	90	285	160	305	0	0	0	90	135	115

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.1	.0	.0	.0
5.	.0	.1	.1	.1	.1	.0	.0	.0
10.	.0	.1	.1	.1	.1	.0	.0	.0
15.	.0	.1	.1	.1	.1	.0	.0	.0
20.	.0	.1	.1	.1	.1	.0	.0	.0
25.	.0	.1	.1	.1	.1	.1	.0	.0
30.	.0	.1	.1	.1	.1	.1	.0	.0
35.	.0	.2	.1	.1	.1	.1	.0	.0
40.	.0	.2	.1	.1	.2	.1	.0	.0
45.	.0	.2	.1	.1	.2	.1	.0	.0
50.	.0	.2	.1	.1	.1	.1	.0	.0
55.	.0	.2	.1	.2	.1	.1	.0	.0
60.	.0	.1	.1	.2	.1	.1	.0	.0
65.	.1	.1	.2	.2	.1	.0	.0	.0
70.	.1	.1	.2	.2	.1	.0	.0	.0
75.	.1	.1	.1	.1	.1	.0	.0	.0
80.	.1	.1	.0	.0	.0	.0	.0	.0
85.	.1	.0	.0	.0	.0	.0	.0	.0
90.	.1	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.2	.0	.0	.0	.0	.0	.0	.0
105.	.2	.0	.0	.0	.0	.0	.0	.0
110.	.2	.0	.0	.0	.0	.0	.0	.0
115.	.2	.0	.0	.0	.0	.0	.0	.0
120.	.2	.0	.0	.0	.0	.0	.0	.0
125.	.2	.0	.0	.0	.0	.0	.0	.0
130.	.2	.0	.0	.0	.0	.0	.0	.0
135.	.2	.0	.0	.0	.0	.0	.0	.0
140.	.2	.0	.0	.0	.0	.0	.0	.0
145.	.2	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT) RUN: Site 2 BUILD ALT4 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.1	.1	.0	.1	.0	.0	.0	.0
250.	.0	.1	.1	.1	.1	.0	.0	.0
255.	.0	.2	.2	.2	.1	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.2	.2	.2	.2	.0	.0	.0
275.	.0	.2	.2	.2	.1	.0	.0	.0
280.	.0	.2	.2	.2	.1	.1	.0	.0
285.	.0	.2	.2	.2	.1	.1	.0	.0
290.	.0	.2	.1	.1	.1	.1	.0	.0
295.	.0	.1	.1	.1	.1	.1	.0	.0
300.	.0	.1	.1	.1	.1	.1	.0	.0
305.	.0	.1	.1	.1	.1	.1	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.2	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.1	.0	.0	.0
340.	.0	.1	.1	.1	.1	.0	.0	.0
345.	.0	.1	.1	.1	.1	.0	.0	.0
350.	.0	.1	.1	.1	.1	.0	.0	.0
355.	.0	.1	.1	.1	.1	.0	.0	.0
360.	.0	.1	.1	.1	.1	.0	.0	.0
MAX	.2	.2	.2	.2	.2	.1	.0	.0
DEGR.	95	35	65	55	40	25	0	0

THE HIGHEST CONCENTRATION IS .40 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 95 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT) RUN: Site 2 BUILD ALT4 PM
DATE: 03/21/2010 TIME: 22:21:18.75

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	3310.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	3310.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	3031.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-2106.8	-138.5	2946.	251.	AG	20.	100.0	.0	48.0	1.50	149.6
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	279.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-824.5	368.7	1561.	252.	AG	18.	100.0	.0	24.0	****	79.3
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	3239.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	4265.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	4246.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	7709.8	3157.8	7257.	72.	AG	25.	100.0	.0	48.0	2.65	368.7
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	19.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	948.3	946.0	130.	73.	AG	21.	100.0	.0	24.0	9.00	6.6
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	5001.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	5001.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	1387.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	1067.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1638.1	-411.3	1448.	146.	AG	22.	100.0	.0	36.0	1.49	73.5
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	320.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	1018.9	541.3	303.	145.	AG	7.	100.0	.0	12.0	1.02	15.4
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1703.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1703.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1982.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	871.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	2.0	2070.8	1283.	328.	AG	24.	100.0	.0	36.0	1.54	65.2
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	1111.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	-816.3	3324.5	2768.	328.	AG	13.	100.0	.0	24.0	1.76	140.6
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	999.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT) RUN: Site 2 BUILD ALT4 PM
DATE: 03/21/2010 TIME: 22:21:18.75

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	68	2.0	3031	969	4.10	1	3
6.	EB Wil LT Q	150	126	2.0	279	84	4.10	1	3
10.	WB Wil T+R Q	150	85	2.0	4246	984	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	19	84	4.10	1	3
17.	NB Vet T+LT Q	150	100	2.0	1067	782	4.10	1	3
19.	NB Vet RT Q	150	95	2.0	320	928	4.10	1	3
24.	SB Vet T+LT Q	150	111	2.0	871	806	4.10	1	3
26.	SB Vet RT Q	150	87	2.0	1111	804	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

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JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT) RUN: Site 2 BUILD ALT4 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
15.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75.	.0	.0	.0	.0	.1	.1	.1	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
85.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
150.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
155.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.1	.0	.0	.0	.1	.1	.1	.1
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
170.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
175.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
180.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
185.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
190.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
195.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
200.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
205.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
215.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
220.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
225.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
230.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
235.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
240.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.0	.0	.0	.0	.0	.1	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255.	.1	.0	.0	.0	.0	.1	.1	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
290.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
295.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
300.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
340.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
345.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
350.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.1	.1	.2	.2	.2	.3	.3	.2	.2	.1	.0	.1	.2	.2	.2	.2	.1
DEGR.	150	150	150	0	0	40	35	65	75	75	75	295	160	0	0	340	340	80	230	65

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.3	.2	.2	.1	.0	.0	.0
5.	.0	.3	.2	.1	.1	.0	.0	.0
10.	.0	.3	.3	.1	.1	.0	.0	.0
15.	.0	.3	.3	.1	.1	.0	.0	.0
20.	.0	.3	.2	.1	.1	.0	.0	.0
25.	.0	.3	.2	.1	.1	.0	.0	.0
30.	.0	.3	.2	.1	.0	.0	.0	.0
35.	.0	.3	.2	.1	.0	.0	.0	.0
40.	.0	.3	.2	.1	.0	.0	.0	.0
45.	.0	.3	.1	.1	.0	.0	.0	.0
50.	.0	.2	.1	.1	.1	.0	.0	.0
55.	.0	.2	.1	.1	.1	.0	.0	.0
60.	.1	.2	.1	.1	.1	.0	.0	.0
65.	.1	.1	.1	.0	.1	.0	.0	.0
70.	.1	.1	.0	.0	.1	.0	.0	.0
75.	.1	.1	.0	.0	.0	.0	.0	.0
80.	.1	.0	.0	.0	.0	.0	.0	.0
85.	.2	.0	.0	.0	.0	.0	.0	.0
90.	.2	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.1	.0	.0	.0	.0	.0	.0	.0
105.	.1	.0	.0	.0	.0	.0	.0	.0
110.	.1	.0	.0	.0	.0	.0	.0	.0
115.	.1	.0	.0	.0	.0	.0	.0	.0
120.	.1	.0	.0	.0	.0	.0	.0	.0
125.	.1	.0	.0	.0	.0	.0	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT) RUN: Site 2 BUILD ALT4 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.2	.1	.2	.0	.0	.0	.0
255.	.0	.2	.2	.2	.1	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.3	.2	.2	.2	.0	.0	.0
275.	.0	.3	.2	.2	.2	.0	.0	.0
280.	.0	.3	.2	.3	.3	.0	.0	.0
285.	.0	.3	.3	.3	.2	.0	.0	.0
290.	.0	.3	.3	.3	.2	.0	.0	.0
295.	.0	.2	.3	.3	.2	.0	.0	.0
300.	.0	.2	.3	.3	.2	.0	.0	.0
305.	.0	.2	.3	.3	.2	.0	.0	.0
310.	.0	.1	.3	.3	.2	.0	.0	.0
315.	.0	.1	.3	.2	.2	.0	.0	.0
320.	.0	.1	.2	.2	.2	.0	.0	.0
325.	.0	.1	.2	.2	.2	.0	.0	.0
330.	.0	.1	.2	.2	.2	.0	.0	.0
335.	.0	.2	.2	.2	.1	.0	.0	.0
340.	.0	.3	.2	.2	.1	.0	.0	.0
345.	.0	.3	.2	.2	.1	.0	.0	.0
350.	.0	.3	.2	.2	.1	.0	.0	.0
355.	.0	.3	.2	.2	.1	.0	.0	.0
360.	.0	.3	.2	.2	.1	.0	.0	.0
MAX	.2	.3	.3	.3	.3	.0	.0	.0
DEGR.	85	0	10	280	280	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 0 DEGREES FROM REC22.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT) RUN: Site 2 BUILD ALT5 AM
DATE: 03/21/2010 TIME: 21:57:39.04

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	5547.	.8	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	5547.	.8	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	4619.	.8	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-5290.1	-1236.5	6313.	251.	AG	17.	100.0	.0	48.0	2.01	320.7
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	928.	.8	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	-4383.2	-797.9	5306.	252.	AG	17.	100.0	.0	24.0	****	269.6
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	4794.	.8	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	3154.	.8	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	3137.	.8	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	4622.4	2169.8	4015.	72.	AG	24.	100.0	.0	48.0	1.82	204.0
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	17.	.8	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	933.5	941.5	114.	73.	AG	21.	100.0	.0	24.0	8.00	5.8
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3424.	.8	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3424.	.8	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	931.	.9	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	799.	.9	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1295.9	88.2	842.	146.	AG	24.	100.0	.0	36.0	1.29	42.8
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	132.	.9	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	890.4	728.0	77.	145.	AG	8.	100.0	.0	12.0	.52	3.9
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1771.	.9	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1771.	.9	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1108.	.9	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	777.	.9	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	-63.4	2176.2	1407.	328.	AG	26.	100.0	.0	36.0	1.80	71.5
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	331.	.9	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	600.2	1041.0	81.	328.	AG	13.	100.0	.0	24.0	.53	4.1
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	748.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT) RUN: Site 2 BUILD ALT5 AM
DATE: 03/21/2010 TIME: 21:57:39.04

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	57	2.0	4619	966	4.10	1	3
6.	EB Wil LT Q	150	118	2.0	928	84	4.10	1	3
10.	WB Wil T+R Q	150	81	2.0	3137	994	4.10	1	3
12.	WB Wil LT Q	150	143	2.0	17	84	4.10	1	3
17.	NB Vet T+LT Q	150	111	2.0	799	887	4.10	1	3
19.	NB Vet RT Q	150	106	2.0	132	955	4.10	1	3
24.	SB Vet T+LT Q	150	120	2.0	777	834	4.10	1	3
26.	SB Vet RT Q	150	90	2.0	331	834	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

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JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT) RUN: Site 2 BUILD ALT5 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
10.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
15.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
20.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
25.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	* .0	.0	.1	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	* .0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	* .0	.0	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	* .0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70.	* .0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
75.	* .0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	* .0	.0	.0	.0	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85.	* .0	.0	.0	.0	.0	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90.	* .0	.0	.0	.0	.0	.0	.0	.2	.4	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
100.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.1	.0	.0	.1	.1
105.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
110.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.3	.0	.0	.0	.1	.0	.0	.1	.1	.1
115.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
120.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
125.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.1	.0	.0	.1	.1	.2
130.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2
140.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
145.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
150.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
155.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2
160.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.0	.1	.0	.0	.0	.0	.1	.2	.2
165.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
170.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
175.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
180.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
185.	* .1	.1	.1	.1	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2
190.	* .1	.1	.1	.0	.0	.0	.0	.3	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
195.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
200.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.2	.1
205.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
215.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1
220.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
225.	* .1	.1	.1	.0	.0	.0	.0	.3	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
230.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240.	* .1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	* .1	.1	.1	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	* .1	.1	.1	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
255.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	* .1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	* .1	.1	.1	.1	.2	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	* .1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	* .1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
285.	* .1	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
290.	* .1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
295.	* .1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
300.	* .1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
305.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.2	.0	.0	.0	.0	.0	.0
310.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
315.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0
320.	* .1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
325.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
340.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
345.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
350.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
355.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
360.	* .0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	* .1	.1	.1	.2	.2	.2	.2	.3	.4	.3	.3	.2	.1	.2	.1	.1	.1	.1	.2	.2
DEGR.	* 150	150	0	280	50	50	55	95	90	85	90	285	160	305	0	0	0	90	140	115

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.1	.0	.0	.0
5.	.0	.1	.1	.1	.1	.0	.0	.0
10.	.0	.1	.1	.1	.1	.0	.0	.0
15.	.0	.1	.1	.1	.1	.0	.0	.0
20.	.0	.1	.1	.1	.1	.0	.0	.0
25.	.0	.1	.1	.1	.1	.1	.0	.0
30.	.0	.1	.1	.1	.1	.1	.0	.0
35.	.0	.2	.1	.1	.1	.1	.0	.0
40.	.0	.2	.1	.1	.1	.1	.0	.0
45.	.0	.2	.1	.1	.2	.1	.0	.0
50.	.0	.2	.1	.1	.1	.1	.0	.0
55.	.0	.2	.1	.2	.1	.1	.0	.0
60.	.0	.1	.1	.2	.1	.1	.0	.0
65.	.1	.1	.2	.2	.1	.0	.0	.0
70.	.1	.1	.2	.2	.1	.0	.0	.0
75.	.1	.1	.1	.1	.1	.0	.0	.0
80.	.1	.1	.0	.0	.0	.0	.0	.0
85.	.1	.0	.0	.0	.0	.0	.0	.0
90.	.1	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.2	.0	.0	.0	.0	.0	.0	.0
105.	.2	.0	.0	.0	.0	.0	.0	.0
110.	.2	.0	.0	.0	.0	.0	.0	.0
115.	.2	.0	.0	.0	.0	.0	.0	.0
120.	.2	.0	.0	.0	.0	.0	.0	.0
125.	.2	.0	.0	.0	.0	.0	.0	.0
130.	.2	.0	.0	.0	.0	.0	.0	.0
135.	.2	.0	.0	.0	.0	.0	.0	.0
140.	.2	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT) RUN: Site 2 BUILD ALT5 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.1	.1	.0	.1	.0	.0	.0	.0
250.	.0	.1	.1	.1	.1	.0	.0	.0
255.	.0	.2	.2	.2	.1	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.2	.2	.2	.2	.0	.0	.0
275.	.0	.2	.2	.2	.1	.0	.0	.0
280.	.0	.2	.2	.2	.1	.1	.0	.0
285.	.0	.2	.2	.2	.1	.1	.0	.0
290.	.0	.2	.1	.1	.1	.1	.0	.0
295.	.0	.1	.1	.1	.1	.1	.0	.0
300.	.0	.1	.1	.1	.1	.1	.0	.0
305.	.0	.1	.1	.1	.1	.1	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.2	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.1	.0	.0	.0
340.	.0	.1	.1	.1	.1	.0	.0	.0
345.	.0	.1	.1	.1	.1	.0	.0	.0
350.	.0	.1	.1	.1	.1	.0	.0	.0
355.	.0	.1	.1	.1	.1	.0	.0	.0
360.	.0	.1	.1	.1	.1	.0	.0	.0
MAX	.2	.2	.2	.2	.2	.1	.0	.0
DEGR.	95	35	65	55	45	25	0	0

THE HIGHEST CONCENTRATION IS .40 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 95 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT) RUN: Site 2 BUILD ALT5 PM
DATE: 03/21/2010 TIME: 22:44:13.37

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	*	-172.0	469.0	78.0	601.0	*	283.	62.	AG	3396.	.8	.0	68.0		
2.	EB Wil AP	*	78.0	601.0	276.0	684.0	*	215.	67.	AG	3396.	.8	.0	68.0		
3.	EB Wil T+R	*	276.0	684.0	778.0	856.0	*	531.	71.	AG	3109.	.8	.0	68.0		
4.	EB Wil T+R Q	*	678.0	822.0	-2495.9	-272.8	*	3357.	251.	AG	21.	100.0	.0	48.0	1.61	170.6
5.	EB Wil LT	*	259.0	724.0	761.0	889.0	*	528.	72.	AG	287.	.8	.0	44.0		
6.	EB Wil LT Q	*	659.0	855.0	-963.1	323.2	*	1707.	252.	AG	19.	100.0	.0	24.0	****	86.7
7.	EB Wil DP	*	782.0	851.0	1703.0	1145.0	*	967.	72.	AG	3318.	.8	.0	68.0		
8.	WB Wil AP	*	1025.0	1019.0	1677.0	1228.0	*	685.	72.	AG	4322.	.8	.0	68.0		
9.	WB Wil T+R	*	1025.0	1019.0	717.0	920.0	*	324.	252.	AG	4305.	.8	.0	68.0		
10.	WB Wil T+R Q	*	798.0	946.0	7669.6	3144.9	*	7215.	72.	AG	24.	100.0	.0	48.0	2.57	366.5
11.	WB Wil LT	*	1040.0	975.0	742.0	883.0	*	312.	253.	AG	17.	.8	.0	44.0		
12.	WB Wil LT Q	*	824.0	908.0	933.5	941.5	*	114.	73.	AG	21.	100.0	.0	24.0	8.00	5.8
13.	WB Wil DP	*	715.0	922.0	201.0	748.0	*	543.	251.	AG	4984.	.8	.0	68.0		
14.	WB Wil DP	*	201.0	748.0	-199.0	546.0	*	448.	243.	AG	4984.	.8	.0	68.0		
15.	NB Vet AP	*	967.0	583.0	1327.0	75.0	*	623.	145.	AG	1370.	.9	.0	32.0		
16.	NB Vet T+LT	*	960.0	579.0	781.0	840.0	*	316.	326.	AG	1075.	.9	.0	56.0		
17.	NB Vet T+LT Q	*	820.0	783.0	1539.2	-266.9	*	1273.	146.	AG	21.	100.0	.0	36.0	1.38	64.6
18.	NB Vet RT	*	964.0	622.0	813.0	839.0	*	264.	325.	AG	295.	.9	.0	32.0		
19.	NB Vet RT Q	*	847.0	791.0	947.0	645.7	*	176.	145.	AG	7.	100.0	.0	12.0	.88	9.0
20.	NB Vet DP	*	798.0	836.0	611.0	1170.0	*	383.	331.	AG	1793.	.9	.0	44.0		
21.	NB Vet DP	*	611.0	1170.0	214.0	1729.0	*	686.	325.	AG	1793.	.9	.0	44.0		
22.	SB Vet AP	*	544.0	1188.0	172.0	1701.0	*	634.	324.	AG	1986.	.9	.0	44.0		
23.	SB Vet T+LT	*	550.0	1188.0	730.0	898.0	*	341.	148.	AG	876.	.9	.0	56.0		
24.	SB Vet T+LT Q	*	679.0	981.0	83.8	1939.2	*	1128.	328.	AG	24.	100.0	.0	36.0	1.42	57.3
25.	SB Vet RT	*	521.0	1169.0	695.0	888.0	*	331.	148.	AG	1110.	.9	.0	44.0		
26.	SB Vet RT Q	*	643.0	972.0	-927.5	3503.8	*	2979.	328.	AG	13.	100.0	.0	24.0	1.88	151.4
27.	SB Vet DP	*	703.0	889.0	1292.0	46.0	*	1028.	145.	AG	979.	.9	.0	44.0		

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JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT) RUN: Site 2 BUILD ALT5 PM
DATE: 03/21/2010 TIME: 22:44:13.37

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	*	150	71	2.0	3109	969	4.10	1	3
6.	EB Wil LT Q	*	150	132	2.0	287	84	4.10	1	3
10.	WB Wil T+R Q	*	150	82	2.0	4305	981	4.10	1	3
12.	WB Wil LT Q	*	150	143	2.0	17	84	4.10	1	3
17.	NB Vet T+LT Q	*	150	97	2.0	1075	795	4.10	1	3
19.	NB Vet RT Q	*	150	92	2.0	295	929	4.10	1	3
24.	SB Vet T+LT Q	*	150	108	2.0	876	812	4.10	1	3
26.	SB Vet RT Q	*	150	90	2.0	1110	794	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	1066.0	492.0	5.0	*
2.	SE 164 S	*	942.0	686.0	5.0	*
3.	SE 82 S	*	892.0	756.0	5.0	*
4.	SE CNR	*	869.0	821.0	5.0	*
5.	SE 82 E	*	925.0	853.0	5.0	*
6.	SE 164 E	*	1005.0	880.0	5.0	*
7.	SE MID E	*	1219.0	947.0	5.0	*
8.	NE MID E	*	1144.0	1099.0	5.0	*
9.	NE 164 E	*	918.0	1026.0	5.0	*
10.	NE 82 E	*	838.0	1000.0	5.0	*
11.	NE CNR	*	759.0	983.0	5.0	*
12.	NE 82 N	*	716.0	1047.0	5.0	*
13.	NE 164 N	*	676.0	1120.0	5.0	*
14.	NE MID N	*	595.0	1269.0	5.0	*
15.	NW MID N	*	464.0	1209.0	5.0	*
16.	NW 164 N	*	546.0	1079.0	5.0	*
17.	NW 82 N	*	589.0	1010.0	5.0	*
18.	NW CNR	*	611.0	945.0	5.0	*
19.	NW 82 W	*	552.0	910.0	5.0	*
20.	NW 164 W	*	475.0	884.0	5.0	*
21.	NW MID W	*	273.0	815.0	5.0	*
22.	SW MID W	*	305.0	649.0	5.0	*
23.	SW 164 W	*	565.0	737.0	5.0	*
24.	SW 82 W	*	645.0	764.0	5.0	*
25.	SW CNR	*	718.0	779.0	5.0	*
26.	SW 82 S	*	774.0	718.0	5.0	*
27.	SW 164 S	*	824.0	646.0	5.0	*
28.	SW MID S	*	957.0	459.0	5.0	*

1 PAGE 3

JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT) RUN: Site 2 BUILD ALT5 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
5.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
10.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40.	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50.	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70.	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75.	.0	.0	.0	.0	.1	.1	.1	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80.	.0	.0	.0	.0	.1	.1	.0	.2	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
150.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
155.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
170.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
175.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
180.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
185.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
190.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
195.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
200.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1
205.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
215.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
220.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.1
225.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1
230.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
235.	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.0	.1	.2	.1
240.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250.	.1	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255.	.1	.0	.0	.0	.0	.1	.1	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
285.	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
290.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
295.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
300.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0
305.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.0	.1	.0	.0	.0	.0	.0	.0
310.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0
315.	.1	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
340.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
345.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
350.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
MAX	.1	.1	.1	.1	.1	.2	.2	.2	.3	.3	.2	.2	.1	.1	.2	.2	.2	.2	.2	.1
DEGR.	150	150	150	0	0	40	30	70	75	75	75	300	160	305	345	340	340	95	230	65

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.3	.3	.2	.1	.0	.0	.0
5.	.0	.3	.3	.1	.1	.0	.0	.0
10.	.0	.3	.3	.1	.1	.0	.0	.0
15.	.0	.3	.3	.1	.1	.0	.0	.0
20.	.0	.3	.2	.1	.1	.0	.0	.0
25.	.0	.3	.2	.1	.1	.0	.0	.0
30.	.0	.3	.2	.1	.1	.0	.0	.0
35.	.0	.3	.2	.1	.0	.0	.0	.0
40.	.0	.3	.2	.1	.0	.0	.0	.0
45.	.0	.3	.2	.1	.0	.0	.0	.0
50.	.0	.2	.1	.1	.1	.0	.0	.0
55.	.0	.2	.1	.1	.1	.0	.0	.0
60.	.1	.2	.1	.1	.1	.0	.0	.0
65.	.1	.2	.1	.0	.1	.0	.0	.0
70.	.1	.1	.0	.0	.1	.0	.0	.0
75.	.1	.1	.0	.0	.0	.0	.0	.0
80.	.1	.0	.0	.0	.0	.0	.0	.0
85.	.2	.0	.0	.0	.0	.0	.0	.0
90.	.2	.0	.0	.0	.0	.0	.0	.0
95.	.2	.0	.0	.0	.0	.0	.0	.0
100.	.1	.0	.0	.0	.0	.0	.0	.0
105.	.1	.0	.0	.0	.0	.0	.0	.0
110.	.1	.0	.0	.0	.0	.0	.0	.0
115.	.1	.0	.0	.0	.0	.0	.0	.0
120.	.1	.0	.0	.0	.0	.0	.0	.0
125.	.1	.0	.0	.0	.0	.0	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0
150.	.1	.0	.0	.0	.0	.0	.0	.0
155.	.1	.0	.0	.0	.0	.0	.0	.0
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT) RUN: Site 2 BUILD ALT5 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.2	.1	.2	.0	.0	.0	.0
255.	.0	.2	.2	.2	.2	.0	.0	.0
260.	.0	.2	.2	.2	.2	.0	.0	.0
265.	.0	.2	.2	.2	.2	.0	.0	.0
270.	.0	.3	.2	.2	.2	.0	.0	.0
275.	.0	.3	.2	.2	.2	.0	.0	.0
280.	.0	.3	.2	.3	.3	.0	.0	.0
285.	.0	.3	.3	.3	.2	.0	.0	.0
290.	.0	.3	.3	.3	.2	.0	.0	.0
295.	.0	.2	.3	.3	.2	.0	.0	.0
300.	.0	.2	.3	.3	.2	.0	.0	.0
305.	.0	.2	.3	.3	.2	.0	.0	.0
310.	.0	.1	.3	.3	.2	.0	.0	.0
315.	.0	.1	.3	.3	.2	.0	.0	.0
320.	.0	.1	.3	.3	.2	.0	.0	.0
325.	.0	.1	.3	.3	.2	.0	.0	.0
330.	.0	.1	.3	.3	.2	.0	.0	.0
335.	.0	.2	.3	.3	.1	.0	.0	.0
340.	.0	.3	.3	.3	.1	.0	.0	.0
345.	.0	.3	.3	.3	.1	.0	.0	.0
350.	.0	.3	.3	.3	.1	.0	.0	.0
355.	.0	.3	.3	.2	.1	.0	.0	.0
360.	.0	.3	.3	.2	.1	.0	.0	.0
MAX	.2	.3	.3	.3	.3	.0	.0	.0
DEGR.	85	0	0	280	280	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .30 PPM AT 75 DEGREES FROM REC10.
THE 3RD HIGHEST CONCENTRATION IS .30 PPM AT 0 DEGREES FROM REC22.

Site 2

Existing with Project

Input & Output Files

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Site 2 Veteran & Wilsh (S2EXWPAM.DAT)   60.0321.0.0000.000280.30480000
1    1
SE MID S                1066.      492.       5.0
SE 164 S                 942.      686.       5.0
SE 82 S                  892.      756.       5.0
SE CNR                   869.      821.       5.0
SE 82 E                  925.      853.       5.0
SE 164 E                1005.      880.       5.0
SE MID E                1219.      947.       5.0
NE MID E                1144.     1099.       5.0
NE 164 E                 918.     1026.       5.0
NE 82 E                  838.     1000.       5.0
NE CNR                   759.      983.       5.0
NE 82 N                  716.     1047.       5.0
NE 164 N                 676.     1120.       5.0
NE MID N                 595.     1269.       5.0
NW MID N                 464.     1209.       5.0
NW 164 N                 546.     1079.       5.0
NW 82 N                  589.     1010.       5.0
NW CNR                   611.      945.       5.0
NW 82 W                  552.      910.       5.0
NW 164 W                 475.      884.       5.0
NW MID W                 273.      815.       5.0
SW MID W                 305.      649.       5.0
SW 164 W                 565.      737.       5.0
SW 82 W                  645.      764.       5.0
SW CNR                   718.      779.       5.0
SW 82 S                  774.      718.       5.0
SW 164 S                 824.      646.       5.0
SW MID S                 957.      459.       5.0
Site 2 Existing WITH PROJ AM            27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    4263 3.3   0  68
30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    4263 3.3   0  68
30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3774 3.3   0  68
30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.       0.  48   4
      150        56       2.0 3774   20.5  995 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     489 3.3   0  44
30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.       0.  24   2
      150       118       2.0  489   20.5 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3927 3.3   0  68
30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    2540 3.3   0  68
30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    2472 3.3   0  68
30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.       0.  48   4
```

```
      150        82       2.0 2472   20.5 1009 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      68 3.3   0  44
30.
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
      150       142       2.0   68   20.5 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    2847 3.3   0  68
30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    2847 3.3   0  68
30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     980 3.5   0  32
30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     833 3.5   0  56
30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
      150       111       2.0  833   20.5  957 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     147 3.5   0  32
30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
      150       106       2.0  147   20.5  967 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1144 3.5   0  44
30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1144 3.5   0  44
30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.     477 3.5   0  44
30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     280 3.5   0  56
30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
      150       120       2.0  280   20.5  833 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     197 3.5   0  44
30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
      150        90       2.0  197   20.5  837 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     342 3.5   0  44
30.
1.0   04 1000.   0Y  5  0 72
```

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 2 Veteran & Wilsh (S2EXWPAM.DAT) RUN: Site 2 Existing WITH PROJ AM
DATE: 07/12/2011 TIME: 15:54:55.14

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	4263.	3.3	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	4263.	3.3	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	3774.	3.3	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-3001.7	-447.2	3892.	251.	AG	82.	100.0	.0	48.0	1.58	197.7
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	489.	3.3	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	37.2	651.2	654.	252.	AG	87.	100.0	.0	24.0	1.21	33.2
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	3927.	3.3	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	2540.	3.3	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	2472.	3.3	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	2962.3	1638.6	2272.	72.	AG	120.	100.0	.0	48.0	1.44	115.4
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	68.	3.3	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	935.8	942.2	117.	73.	AG	104.	100.0	.0	24.0	1.21	5.9
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	2847.	3.3	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	2847.	3.3	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	980.	3.5	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	833.	3.5	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1266.4	131.4	790.	146.	AG	122.	100.0	.0	36.0	1.24	40.1
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	147.	3.5	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	895.3	720.8	85.	145.	AG	39.	100.0	.0	12.0	.57	4.3
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	1144.	3.5	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	1144.	3.5	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	477.	3.5	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	280.	3.5	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	646.0	1034.1	62.	328.	AG	132.	100.0	.0	36.0	.65	3.2
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	197.	3.5	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	617.6	1013.0	48.	328.	AG	66.	100.0	.0	24.0	.31	2.5
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	342.	3.5	.0	44.0		

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JOB: Site 2 Veteran & Wilsh (S2EXWPAM.DAT) RUN: Site 2 Existing WITH PROJ AM
DATE: 07/12/2011 TIME: 15:54:55.14

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	56	2.0	3774	995	20.50	1	3
6.	EB Wil LT Q	150	118	2.0	489	1084	20.50	1	3
10.	WB Wil T+R Q	150	82	2.0	2472	1009	20.50	1	3
12.	WB Wil LT Q	150	142	2.0	68	1084	20.50	1	3
17.	NB Vet T+LT Q	150	111	2.0	833	957	20.50	1	3
19.	NB Vet RT Q	150	106	2.0	147	967	20.50	1	3
24.	SB Vet T+LT Q	150	120	2.0	280	833	20.50	1	3
26.	SB Vet RT Q	150	90	2.0	197	837	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

1 PAGE 3

JOB: Site 2 Veteran & Wilsh (S2EXWPAM.DAT) RUN: Site 2 Existing WITH PROJ AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.2	.3	.5	.6	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
5.	.2	.2	.5	.6	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
10.	.2	.2	.5	.6	.7	.7	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.2	.0	.0
15.	.2	.2	.4	.6	.7	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.2	.0	.0
20.	.2	.2	.4	.6	.7	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.3	.0	.0
25.	.2	.3	.3	.6	.7	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.0	.0
30.	.2	.3	.3	.8	.8	.7	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.0	.0
35.	.2	.3	.4	.7	.8	.8	.7	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.4	.1	.0
40.	.2	.3	.4	.8	.8	.8	.8	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.4	.1	.0
45.	.1	.3	.4	.7	.8	.8	.8	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.4	.1	.0
50.	.1	.2	.4	.7	.8	.8	.8	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.3	.1	.0
55.	.0	.2	.4	.7	.8	.9	.8	.2	.1	.1	.1	.0	.0	.0	.1	.0	.2	.3	.1	.1
60.	.0	.2	.4	.7	.8	.9	.8	.2	.2	.3	.1	.0	.0	.0	.1	.1	.2	.3	.3	.2
65.	.0	.2	.2	.6	.8	.8	.8	.4	.4	.4	.4	.1	.0	.0	.1	.1	.3	.4	.3	.2
70.	.0	.0	.2	.4	.6	.7	.5	.5	.7	.6	.6	.1	.0	.0	.1	.2	.3	.7	.5	.5
75.	.0	.0	.1	.3	.4	.5	.4	.8	.8	.8	.7	.2	.1	.0	.1	.2	.5	.6	.7	.6
80.	.0	.0	.0	.1	.2	.3	.2	.8	.9	.9	.8	.4	.1	.0	.2	.2	.8	.7	.6	.6
85.	.0	.0	.0	.1	.2	.2	.1	.9	1.1	1.1	.9	.4	.3	.1	.2	.3	.9	.8	.7	.7
90.	.0	.0	.0	.0	.1	.1	.1	1.1	1.1	1.1	1.0	.5	.3	.1	.1	.4	.9	.7	.7	.7
95.	.0	.0	.0	.0	.1	.1	.1	.9	.9	1.0	.9	.5	.3	.1	.2	.3	.7	.6	.7	.6
100.	.0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.9	.4	.3	.2	.2	.4	.7	.7	.5	.6
105.	.0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.9	.4	.2	.2	.2	.5	.6	.4	.5	.8
110.	.0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.9	.4	.3	.2	.2	.5	.6	.5	.5	.8
115.	.0	.0	.0	.0	.0	.0	.0	.9	.8	1.0	.7	.4	.3	.2	.2	.5	.5	.5	.6	.8
120.	.0	.0	.0	.0	.0	.0	.0	.9	.8	1.0	.7	.4	.3	.2	.2	.4	.6	.5	.7	.8
125.	.0	.0	.0	.0	.0	.0	.0	.8	.7	.8	.7	.4	.3	.2	.2	.4	.6	.5	.8	.8
130.	.0	.0	.0	.0	.0	.0	.0	.7	.7	.8	.7	.4	.3	.2	.1	.3	.5	.4	.8	.8
135.	.1	.1	.1	.1	.0	.0	.0	.7	.7	.8	.7	.4	.3	.2	.1	.4	.4	.4	.8	.8
140.	.2	.1	.2	.1	.0	.0	.0	.7	.7	.8	.7	.4	.4	.2	.1	.3	.4	.5	.7	.6
145.	.3	.3	.2	.1	.1	.0	.0	.7	.7	.9	.6	.5	.5	.2	.1	.3	.3	.5	.7	.6
150.	.4	.4	.3	.2	.1	.0	.0	.7	.7	.9	.6	.4	.4	.2	.2	.3	.3	.5	.7	.7
155.	.4	.4	.4	.2	.1	.0	.0	.7	.8	.9	.6	.4	.4	.2	.2	.2	.2	.6	.7	.7
160.	.5	.4	.4	.3	.1	.1	.0	.7	.8	.9	.5	.5	.4	.2	.2	.2	.2	.6	.7	.7
165.	.5	.4	.5	.4	.2	.1	.0	.7	.9	.9	.6	.4	.4	.3	.2	.2	.4	.6	.7	.7
170.	.5	.4	.6	.5	.2	.1	.0	.7	.9	.9	.6	.4	.4	.3	.2	.3	.4	.6	.7	.7
175.	.5	.4	.5	.5	.2	.1	.0	.7	.9	.9	.6	.4	.5	.3	.2	.4	.4	.6	.7	.7
180.	.5	.4	.5	.5	.2	.1	.0	.7	.9	.9	.4	.4	.4	.3	.2	.4	.4	.6	.7	.7
185.	.5	.4	.5	.5	.2	.1	.1	.8	.9	.9	.4	.3	.4	.3	.2	.4	.4	.6	.7	.7
190.	.4	.4	.5	.4	.2	.1	.1	.8	.9	.8	.4	.3	.4	.3	.2	.4	.4	.6	.7	.7
195.	.4	.4	.5	.4	.1	.1	.1	.8	.9	.7	.5	.4	.5	.3	.1	.4	.4	.6	.7	.7
200.	.4	.4	.5	.4	.1	.1	.1	.9	.9	.7	.6	.5	.6	.3	.1	.4	.4	.6	.7	.7
205.	.4	.4	.5	.3	.1	.1	.1	1.0	.9	.8	.6	.6	.6	.2	.0	.4	.4	.6	.7	.7

1

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.4	.4	.5	.3	.1	.1	.1	1.0	1.0	.8	.7	.6	.6	.1	.0	.4	.4	.7	.7	.7
215.	.4	.4	.5	.3	.1	.1	.1	.9	1.0	.6	.7	.6	.5	.1	.0	.4	.4	.7	.7	.7
220.	.4	.4	.5	.3	.1	.1	.1	.9	.9	.8	.8	.7	.5	.1	.1	.3	.4	.7	.7	.7
225.	.4	.4	.5	.2	.1	.1	.1	1.0	.9	.9	.8	.7	.4	.2	.1	.2	.4	.6	.6	.7
230.	.4	.4	.5	.2	.1	.2	.2	1.1	1.0	1.1	.8	.7	.3	.2	.1	.1	.3	.6	.8	.7
235.	.4	.4	.5	.2	.1	.2	.1	1.0	1.0	.9	.7	.7	.2	.1	.1	.1	.3	.6	.8	.9
240.	.4	.4	.5	.4	.4	.4	.1	1.0	.9	.9	.8	.6	.2	.1	.0	.1	.2	.5	.8	.7
245.	.4	.4	.6	.4	.3	.4	.4	1.0	.8	.9	.7	.5	.2	.1	.0	.1	.1	.4	.6	.6
250.	.4	.4	.6	.4	.5	.4	.5	.8	.7	.8	.5	.4	.1	.1	.0	.0	.1	.3	.6	.5
255.	.4	.5	.7	.6	.7	.7	.6	.5	.5	.3	.4	.2	.1	.1	.0	.0	.0	.2	.3	.4
260.	.4	.5	.7	.8	.8	.8	.7	.3	.3	.2	.3	.2	.1	.1	.0	.0	.0	.1	.1	.1
265.	.4	.6	.8	.8	.8	.8	.8	.2	.1	.4	.3	.2	.1	.1	.0	.0	.0	.0	.1	.1
270.	.5	.6	1.0	.8	.8	.8	.7	.0	.0	.2	.2	.2	.1	.1	.0	.0	.0	.0	.1	.1
275.	.5	.7	.9	.6	.6	.9	.7	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
280.	.5	.8	.9	.7	.6	.9	.7	.0	.0	.2	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
285.	.4	.8	.9	.5	.7	.7	.9	.0	.0	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
290.	.6	.7	.7	.5	.7	.7	.8	.0	.0	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
295.	.6	.6	.5	.5	.7	.7	.7	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
300.	.6	.6	.6	.6	.8	.7	.7	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0
305.	.6	.5	.6	.7	.7	.7	.7	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0
310.	.6	.4	.7	.5	.7	.7	.6	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0
315.	.4	.4	.4	.5	.6	.7	.6	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0
320.	.4	.2	.3	.5	.6	.5	.5	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0
325.	.2	.2	.3	.5	.6	.5	.5	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
330.	.2	.2	.4	.6	.6	.6	.6	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0
335.	.2	.3	.4	.6	.7	.6	.6	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0
340.	.2	.3	.5	.6	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345.	.1	.3	.5	.6	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350.	.2	.3	.5	.6	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355.	.2	.3	.5	.6	.6	.6	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
360.	.2	.3	.5	.6	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
MAX	.6	.8	1.0	.8	.8	.9	.9	1.1	1.1	1.1	1.0	.7	.6	.3	.2	.5	.9	.8	.8	.9
DEGR.	290	280	270	260	260	275	285	90	85	85	90	220	200	165	80	105	85	85	125	235

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.7	.7	.7	.6	.4	.5	.4
5.	.0	.7	.7	.7	.5	.3	.6	.4
10.	.0	.7	.7	.7	.5	.4	.6	.4
15.	.0	.8	.8	.6	.5	.3	.6	.4
20.	.0	.8	.8	.7	.6	.3	.5	.4
25.	.0	.8	.8	.7	.7	.6	.5	.4
30.	.0	.8	.8	.7	.7	.6	.5	.4
35.	.0	.9	.8	.7	.5	.6	.5	.4
40.	.0	.9	.9	.8	.7	.5	.6	.4
45.	.0	1.0	.9	.8	.8	.6	.6	.4
50.	.1	1.0	.9	.7	.9	.7	.6	.3
55.	.1	1.1	.9	.8	.9	.7	.5	.4
60.	.1	1.1	.9	.9	.7	.7	.5	.3
65.	.3	.9	.7	.7	.7	.5	.5	.2
70.	.4	.7	.6	.5	.4	.5	.3	.2
75.	.6	.6	.4	.4	.3	.4	.3	.3
80.	.8	.4	.3	.3	.3	.3	.3	.3
85.	.9	.1	.3	.3	.2	.3	.3	.3
90.	.8	.1	.1	.2	.2	.3	.3	.3
95.	.8	.1	.1	.1	.2	.3	.3	.3
100.	.7	.1	.1	.1	.2	.3	.3	.3
105.	.8	.1	.1	.1	.3	.3	.2	.3
110.	.8	.0	.1	.1	.3	.3	.2	.3
115.	.8	.0	.1	.1	.3	.3	.2	.3
120.	.7	.0	.1	.1	.2	.2	.2	.3
125.	.7	.0	.1	.1	.2	.2	.2	.3
130.	.7	.0	.1	.1	.2	.2	.2	.3
135.	.7	.0	.0	.1	.2	.2	.2	.2
140.	.7	.0	.0	.1	.1	.2	.2	.1
145.	.7	.0	.0	.0	.1	.1	.1	.1
150.	.7	.0	.0	.0	.1	.1	.1	.1
155.	.7	.0	.0	.0	.0	.0	.0	.0
160.	.7	.0	.0	.0	.0	.0	.0	.0
165.	.6	.0	.0	.0	.0	.0	.0	.0
170.	.7	.0	.0	.0	.0	.0	.0	.0
175.	.7	.0	.0	.0	.0	.0	.0	.0
180.	.6	.0	.0	.0	.0	.0	.0	.0
185.	.6	.0	.0	.0	.0	.0	.0	.0
190.	.6	.0	.0	.0	.0	.0	.0	.0
195.	.7	.0	.0	.0	.0	.0	.0	.0
200.	.7	.0	.0	.0	.0	.0	.0	.0
205.	.7	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 2 Veteran & Wilsh (S2EXWPAM.DAT) RUN: Site 2 Existing WITH PROJ AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.8	.0	.0	.0	.0	.0	.0	.0
215.	.9	.0	.0	.0	.0	.0	.0	.0
220.	.8	.0	.0	.0	.0	.0	.0	.0
225.	.8	.0	.0	.0	.0	.0	.0	.0
230.	.8	.0	.0	.0	.0	.0	.0	.0
235.	.8	.3	.2	.2	.0	.0	.0	.0
240.	.7	.3	.2	.2	.2	.0	.0	.0
245.	.4	.5	.5	.4	.2	.1	.0	.0
250.	.3	.6	.5	.6	.4	.1	.0	.0
255.	.3	.8	.9	.8	.6	.2	.1	.0
260.	.2	.9	1.0	1.1	.7	.2	.1	.0
265.	.0	1.0	1.1	.9	.9	.3	.1	.0
270.	.0	1.0	1.0	1.0	.8	.3	.2	.1
275.	.0	.9	.9	.9	.8	.5	.2	.1
280.	.0	1.0	.9	.9	.8	.5	.3	.1
285.	.0	1.0	.9	.9	.8	.5	.4	.0
290.	.0	.9	.8	.8	.8	.5	.4	.0
295.	.0	.8	.8	.8	.7	.5	.4	.1
300.	.0	.8	.8	.8	.6	.5	.4	.1
305.	.0	.8	.8	.8	.6	.5	.3	.1
310.	.0	.9	.7	.7	.6	.5	.3	.1
315.	.0	.8	.7	.7	.6	.4	.2	.1
320.	.0	.8	.7	.7	.6	.3	.2	.1
325.	.0	.8	.7	.7	.5	.3	.2	.2
330.	.0	.7	.7	.7	.4	.3	.1	.1
335.	.0	.8	.7	.7	.4	.3	.1	.1
340.	.0	.8	.7	.7	.4	.3	.1	.2
345.	.0	.7	.7	.7	.4	.2	.3	.3
350.	.0	.7	.7	.7	.5	.2	.2	.3
355.	.0	.7	.7	.7	.5	.4	.3	.3
360.	.0	.7	.7	.7	.6	.4	.5	.4
MAX	.9	1.1	1.1	1.1	.9	.7	.6	.4
DEGR.	215	55	265	260	265	50	5	0

THE HIGHEST CONCENTRATION IS 1.10 PPM AT 90 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS 1.10 PPM AT 85 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS 1.10 PPM AT 85 DEGREES FROM REC10.

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Site 2 Veteran & Wilsh (S2EXWPPM.DAT)   60.0321.0.0000.000280.30480000
1    1
SE MID S                1066.      492.       5.0
SE 164 S                 942.      686.       5.0
SE 82 S                  892.      756.       5.0
SE CNR                   869.      821.       5.0
SE 82 E                  925.      853.       5.0
SE 164 E                1005.      880.       5.0
SE MID E                1219.      947.       5.0
NE MID E                1144.     1099.       5.0
NE 164 E                 918.     1026.       5.0
NE 82 E                  838.     1000.       5.0
NE CNR                   759.      983.       5.0
NE 82 N                  716.     1047.       5.0
NE 164 N                 676.     1120.       5.0
NE MID N                 595.     1269.       5.0
NW MID N                 464.     1209.       5.0
NW 164 N                 546.     1079.       5.0
NW 82 N                  589.     1010.       5.0
NW CNR                   611.      945.       5.0
NW 82 W                  552.      910.       5.0
NW 164 W                 475.      884.       5.0
NW MID W                 273.      815.       5.0
SW MID W                 305.      649.       5.0
SW 164 W                 565.      737.       5.0
SW 82 W                  645.      764.       5.0
SW CNR                   718.      779.       5.0
SW 82 S                  774.      718.       5.0
SW 164 S                 824.      646.       5.0
SW MID S                 957.      459.       5.0
Site 2 Existing WITH PROJ PM            27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    2611 3.3   0  68
30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    2611 3.3   0  68
30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    2532 3.3   0  68
30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
      150        60       2.0 2532   20.5  950 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.      79 3.3   0  44
30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
      150       130       2.0   79   20.5 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    2607 3.3   0  68
30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    2863 3.3   0  68
30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    2774 3.3   0  68
30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
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       150        72       2.0 2774   20.5 1004 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      89 3.3   0  44
30.
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       142       2.0   89   20.5 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3507 3.3   0  68
30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3507 3.3   0  68
30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1173 3.5   0  32
30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     843 3.5   0  56
30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       108       2.0  843   20.5  855 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     330 3.5   0  32
30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       102       2.0  330   20.5  929 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.     894 3.5   0  44
30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.     894 3.5   0  44
30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1135 3.5   0  44
30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     430 3.5   0  56
30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       118       2.0  430   20.5  814 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     705 3.5   0  44
30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150       100       2.0  705   20.5  804 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     774 3.5   0  44
30.
1.0   04 1000.   0Y  5  0 72
```

JOB: Site 2 Veteran & Wilsh (S2EXWPPM.DAT) RUN: Site 2 Existing WITH PROJ PM
DATE: 07/12/2011 TIME: 16:08:36.60

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Wil AP	-172.0	469.0	78.0	601.0	283.	62.	AG	2611.	3.3	.0	68.0		
2.	EB Wil AP	78.0	601.0	276.0	684.0	215.	67.	AG	2611.	3.3	.0	68.0		
3.	EB Wil T+R	276.0	684.0	778.0	856.0	531.	71.	AG	2532.	3.3	.0	68.0		
4.	EB Wil T+R Q	678.0	822.0	-471.5	425.5	1216.	251.	AG	88.	100.0	.0	48.0	1.16	61.8
5.	EB Wil LT	259.0	724.0	761.0	889.0	528.	72.	AG	79.	3.3	.0	44.0		
6.	EB Wil LT Q	659.0	855.0	632.7	846.4	28.	252.	AG	95.	100.0	.0	24.0	.34	1.4
7.	EB Wil DP	782.0	851.0	1703.0	1145.0	967.	72.	AG	2607.	3.3	.0	68.0		
8.	WB Wil AP	1025.0	1019.0	1677.0	1228.0	685.	72.	AG	2863.	3.3	.0	68.0		
9.	WB Wil T+R	1025.0	1019.0	717.0	920.0	324.	252.	AG	2774.	3.3	.0	68.0		
10.	WB Wil T+R Q	798.0	946.0	3058.3	1669.3	2373.	72.	AG	106.	100.0	.0	48.0	1.40	120.6
11.	WB Wil LT	1040.0	975.0	742.0	883.0	312.	253.	AG	89.	3.3	.0	44.0		
12.	WB Wil LT Q	824.0	908.0	1046.2	975.9	232.	73.	AG	104.	100.0	.0	24.0	1.57	11.8
13.	WB Wil DP	715.0	922.0	201.0	748.0	543.	251.	AG	3507.	3.3	.0	68.0		
14.	WB Wil DP	201.0	748.0	-199.0	546.0	448.	243.	AG	3507.	3.3	.0	68.0		
15.	NB Vet AP	967.0	583.0	1327.0	75.0	623.	145.	AG	1173.	3.5	.0	32.0		
16.	NB Vet T+LT	960.0	579.0	781.0	840.0	316.	326.	AG	843.	3.5	.0	56.0		
17.	NB Vet T+LT Q	820.0	783.0	1327.9	41.5	899.	146.	AG	119.	100.0	.0	36.0	1.30	45.7
18.	NB Vet RT	964.0	622.0	813.0	839.0	264.	325.	AG	330.	3.5	.0	32.0		
19.	NB Vet RT Q	847.0	791.0	1330.2	89.0	852.	145.	AG	37.	100.0	.0	12.0	1.21	43.3
20.	NB Vet DP	798.0	836.0	611.0	1170.0	383.	331.	AG	894.	3.5	.0	44.0		
21.	NB Vet DP	611.0	1170.0	214.0	1729.0	686.	325.	AG	894.	3.5	.0	44.0		
22.	SB Vet AP	544.0	1188.0	172.0	1701.0	634.	324.	AG	1135.	3.5	.0	44.0		
23.	SB Vet T+LT	550.0	1188.0	730.0	898.0	341.	148.	AG	430.	3.5	.0	56.0		
24.	SB Vet T+LT Q	679.0	981.0	608.6	1094.3	133.	328.	AG	130.	100.0	.0	36.0	.95	6.8
25.	SB Vet RT	521.0	1169.0	695.0	888.0	331.	148.	AG	705.	3.5	.0	44.0		
26.	SB Vet RT Q	643.0	972.0	-66.0	2115.0	1345.	328.	AG	73.	100.0	.0	24.0	1.43	68.3
27.	SB Vet DP	703.0	889.0	1292.0	46.0	1028.	145.	AG	774.	3.5	.0	44.0		

JOB: Site 2 Veteran & Wilsh (S2EXWPPM.DAT) RUN: Site 2 Existing WITH PROJ PM
DATE: 07/12/2011 TIME: 16:08:36.60

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
4.	EB Wil T+R Q	150	60	2.0	2532	950	20.50	1	3
6.	EB Wil LT Q	150	130	2.0	79	1084	20.50	1	3
10.	WB Wil T+R Q	150	72	2.0	2774	1004	20.50	1	3
12.	WB Wil LT Q	150	142	2.0	89	1084	20.50	1	3
17.	NB Vet T+LT Q	150	108	2.0	843	855	20.50	1	3
19.	NB Vet RT Q	150	102	2.0	330	929	20.50	1	3
24.	SB Vet T+LT Q	150	118	2.0	430	814	20.50	1	3
26.	SB Vet RT Q	150	100	2.0	705	804	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	1066.0	492.0	5.0
2.	SE 164 S	942.0	686.0	5.0
3.	SE 82 S	892.0	756.0	5.0
4.	SE CNR	869.0	821.0	5.0
5.	SE 82 E	925.0	853.0	5.0
6.	SE 164 E	1005.0	880.0	5.0
7.	SE MID E	1219.0	947.0	5.0
8.	NE MID E	1144.0	1099.0	5.0
9.	NE 164 E	918.0	1026.0	5.0
10.	NE 82 E	838.0	1000.0	5.0
11.	NE CNR	759.0	983.0	5.0
12.	NE 82 N	716.0	1047.0	5.0
13.	NE 164 N	676.0	1120.0	5.0
14.	NE MID N	595.0	1269.0	5.0
15.	NW MID N	464.0	1209.0	5.0
16.	NW 164 N	546.0	1079.0	5.0
17.	NW 82 N	589.0	1010.0	5.0
18.	NW CNR	611.0	945.0	5.0
19.	NW 82 W	552.0	910.0	5.0
20.	NW 164 W	475.0	884.0	5.0
21.	NW MID W	273.0	815.0	5.0
22.	SW MID W	305.0	649.0	5.0
23.	SW 164 W	565.0	737.0	5.0
24.	SW 82 W	645.0	764.0	5.0
25.	SW CNR	718.0	779.0	5.0
26.	SW 82 S	774.0	718.0	5.0
27.	SW 164 S	824.0	646.0	5.0
28.	SW MID S	957.0	459.0	5.0

JOB: Site 2 Veteran & Wilsh (S2EXWPPM.DAT) RUN: Site 2 Existing WITH PROJ PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	.0	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.3	.5	.4	.1	.1
5.	*	.0	.4	.4	.5	.5	.6	.4	.0	.0	.0	.0	.0	.0	.0	.4	.3	.4	.5	.1	.1
10.	*	.0	.3	.4	.5	.5	.6	.4	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.5	.1	.1
15.	*	.0	.2	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.3	.3	.4	.5	.2	.1
20.	*	.1	.2	.4	.5	.6	.6	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.1
25.	*	.1	.3	.4	.5	.6	.6	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.1
30.	*	.1	.3	.4	.5	.7	.6	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.1
35.	*	.1	.3	.3	.6	.7	.5	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.2
40.	*	.1	.3	.3	.7	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.2
45.	*	.1	.3	.3	.6	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.2	.1
50.	*	.1	.3	.3	.7	.7	.6	.6	.1	.0	.0	.0	.0	.0	.0	.3	.3	.5	.4	.1	.1
55.	*	.0	.2	.3	.7	.7	.7	.6	.2	.1	.2	.0	.0	.0	.0	.3	.3	.5	.3	.2	.2
60.	*	.0	.2	.3	.5	.7	.7	.6	.2	.3	.3	.2	.0	.0	.0	.3	.3	.5	.3	.3	.3
65.	*	.0	.1	.2	.4	.5	.5	.5	.4	.4	.4	.4	.1	.0	.0	.3	.4	.6	.4	.4	.4
70.	*	.0	.0	.2	.4	.5	.5	.4	.6	.6	.6	.4	.1	.0	.0	.3	.4	.6	.6	.5	.4
75.	*	.0	.0	.0	.2	.3	.3	.3	.6	.7	.7	.7	.2	.1	.0	.3	.5	.7	.6	.7	.7
80.	*	.0	.0	.0	.1	.2	.2	.1	.9	.9	.9	.7	.3	.1	.0	.4	.5	.7	.7	.8	.6
85.	*	.0	.0	.0	.1	.1	.1	.1	.9	.9	.9	1.0	.4	.2	.1	.4	.7	1.0	.9	.7	.7
90.	*	.0	.0	.0	.0	.1	.1	.1	.9	.9	1.0	.9	.5	.2	.1	.4	.8	1.0	.7	.7	.8
95.	*	.0	.0	.0	.0	.0	.0	.0	.9	.8	1.0	.8	.5	.3	.1	.4	.8	.8	.7	.7	.6
100.	*	.0	.0	.0	.0	.0	.0	.0	.9	.9	.9	.8	.5	.3	.2	.4	.8	.9	.7	.7	.6
105.	*	.0	.0	.0	.0	.0	.0	.0	.7	1.0	.9	.8	.5	.3	.2	.4	.8	.9	.5	.6	.6
110.	*	.0	.0	.0	.0	.0	.0	.0	.7	.9	.8	.7	.4	.3	.1	.4	.8	.7	.5	.5	.7
115.	*	.0	.0	.0	.0	.0	.0	.0	.7	.8	.8	.7	.4	.3	.1	.3	.8	.7	.7	.6	.7
120.	*	.0	.0	.0	.0	.0	.0	.0	.7	.8	.8	.7	.4	.4	.1	.3	.7	.7	.7	.6	.7
125.	*	.0	.0	.0	.0	.0	.0	.0	.7	.8	.8	.7	.4	.4	.1	.3	.6	.6	.5	.6	.6
130.	*	.2	.0	.1	.0	.0	.0	.0	.7	.8	.8	.5	.4	.4	.1	.4	.6	.4	.6	.6	.6
135.	*	.3	.2	.2	.1	.0	.0	.0	.7	.7	.8	.6	.4	.3	.2	.5	.6	.5	.6	.6	.6
140.	*	.4	.3	.3	.1	.0	.0	.0	.7	.7	.7	.6	.4	.4	.1	.5	.5	.5	.6	.6	.5
145.	*	.4	.4	.3	.3	.1	.0	.0	.7	.7	.8	.5	.3	.3	.1	.6	.4	.4	.6	.6	.5
150.	*	.6	.5	.5	.3	.1	.0	.0	.7	.8	.9	.5	.4	.3	.1	.3	.5	.5	.5	.5	.5
155.	*	.6	.5	.6	.3	.1	.1	.0	.7	.9	.9	.5	.4	.3	.3	.2	.4	.4	.5	.5	.5
160.	*	.9	.5	.7	.4	.1	.1	.0	.7	.9	.9	.5	.3	.3	.3	.2	.2	.3	.5	.5	.5
165.	*	.9	.6	.8	.5	.2	.1	.0	.7	.9	.9	.5	.3	.4	.2	.1	.2	.4	.5	.5	.5
170.	*	.9	.6	.7	.5	.2	.1	.0	.7	.9	.9	.6	.4	.3	.4	.1	.3	.4	.5	.5	.5
175.	*	.9	.6	.7	.5	.2	.1	.0	.7	.9	.9	.5	.4	.4	.4	.1	.3	.4	.5	.5	.5
180.	*	.8	.6	.7	.5	.2	.1	.0	.8	.8	.8	.4	.4	.4	.4	.1	.3	.4	.5	.5	.5
185.	*	.7	.6	.6	.4	.2	.1	.1	.8	.8	.8	.4	.3	.5	.3	.1	.3	.4	.5	.5	.5
190.	*	.6	.5	.5	.4	.1	.1	.1	.8	.9	.8	.4	.3	.5	.3	.1	.3	.4	.5	.5	.5
195.	*	.6	.5	.5	.4	.1	.1	.1	.8	.9	.7	.4	.5	.6	.3	.1	.3	.4	.5	.5	.5
200.	*	.5	.5	.5	.4	.1	.1	.1	.8	.9	.8	.5	.5	.7	.3	.1	.3	.4	.5	.5	.5
205.	*	.5	.5	.5	.3	.1	.1	.1	.8	.8	.7	.6	.6	.7	.3	.1	.3	.4	.5	.6	.6

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WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	*	.5	.5	.5	.3	.1	.1	.1	.8	.8	.6	.6	.6	.7	.3	.0	.2	.4	.5	.6	.6
215.	*	.5	.5	.5	.3	.1	.1	.1	.8	.8	.6	.7	.6	.7	.2	.0	.2	.4	.5	.6	.6
220.	*	.5	.5	.5	.3	.1	.1	.1	.8	.9	.8	.6	.7	.6	.2	.0	.2	.4	.5	.6	.6
225.	*	.5	.5	.5	.2	.1	.1	.1	1.0	.9	.8	.6	.7	.6	.2	.0	.3	.3	.5	.6	.6
230.	*	.5	.5	.5	.2	.1	.1	.1	1.0	.9	.7	.7	.8	.6	.3	.0	.3	.2	.5	.6	.8
235.	*	.5	.5	.5	.2	.1	.1	.1	1.0	.8	.8	.7	.7	.6	.3	.0	.1	.3	.5	.7	.6
240.	*	.5	.5	.5	.2	.3	.2	.1	1.1	.8	.7	.7	.6	.3	.3	.0	.0	.3	.5	.6	.6
245.	*	.5	.5	.5	.4	.3	.3	.1	.9	.8	.7	.7	.6	.3	.3	.0	.0	.2	.4	.6	.6
250.	*	.5	.5	.6	.3	.3	.4	.3	.7	.5	.5	.4	.5	.3	.3	.0	.0	.0	.4	.5	.5
255.	*	.5	.5	.6	.4	.4	.5	.5	.5	.4	.3	.3	.4	.3	.3	.0	.0	.0	.1	.3	.3
260.	*	.5	.6	.7	.5	.5	.5	.7	.3	.2	.3	.3	.4	.3	.3	.0	.0	.0	.1	.2	.2
265.	*	.5	.6	.8	.6	.5	.6	.7	.2	.3	.3	.3	.4	.2	.3	.0	.0	.0	.0	.1	.1
270.	*	.5	.7	.8	.6	.5	.7	.7	.0	.2	.1	.3	.4	.2	.3	.0	.0	.0	.0	.1	.1
275.	*	.6	.8	.7	.5	.4	.6	.6	.0	.1	.1	.3	.4	.2	.3	.0	.0	.0	.0	.0	.0
280.	*	.6	.8	.7	.4	.5	.6	.6	.0	.1	.2	.4	.4	.2	.3	.0	.0	.0	.0	.0	.0
285.	*	.6	.8	.7	.3	.5	.7	.7	.0	.0	.2	.4	.4	.2	.3	.0	.0	.0	.0	.0	.0
290.	*	.7	.9	.7	.3	.5	.6	.6	.0	.1	.2	.4	.4	.2	.3	.0	.0	.0	.0	.0	.0
295.	*	.8	.8	.6	.5	.6	.6	.5	.0	.1	.2	.4	.3	.2	.3	.0	.0	.0	.0	.0	.0
300.	*	.9	.7	.6	.6	.5	.6	.5	.0	.1	.1	.4	.3	.2	.3	.0	.0	.0	.0	.0	.0
305.	*	.9	.7	.6	.6	.7	.7	.5	.0	.1	.1	.4	.3	.4	.3	.0	.0	.0	.0	.0	.0
310.	*	.7	.7	.8	.6	.6	.6	.4	.0	.0	.1	.3	.2	.4	.3	.0	.0	.0	.0	.0	.0
315.	*	.6	.5	.3	.6	.6	.5	.4	.0	.0	.1	.3	.2	.4	.2	.1	.1	.1	.0	.0	.0
320.	*	.6	.4	.4	.6	.6	.5	.4	.0	.0	.1	.3	.2	.3	.2	.1	.1	.1	.1	.0	.0
325.	*	.4	.5	.3	.5	.5	.5	.4	.0	.0	.0	.2	.2	.2	.2	.3	.3	.3	.1	.0	.0
330.	*	.2	.2	.2	.5	.5	.5	.4	.0	.0	.0	.0	.2	.1	.0	.3	.4	.4	.2	.1	.0
335.	*	.2	.2	.2	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.3	.5	.5	.2	.1	.0
340.	*	.2	.3	.4	.5	.5	.6	.4	.0	.0	.0	.0	.0	.0	.0	.4	.5	.5	.3	.1	.1
345.	*	.0	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.5	.4	.4	.1	.1
350.	*	.0	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.4	.4	.1	.1
355.	*	.0	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.4	.4	.1	.1
360.	*	.0	.4	.4	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.4	.3	.5	.4	.1	.1
MAX	*	.9	.9	.8	.7	.7	.7	.7	1.1	1.0	1.0	1.0	.8	.7	.4	.6	.8	1.0	.9	.8	.8
DEGR.	*	160	290	165	40	30	270	260	240	105	90	85	230	200	170	145	90	85	85	80	230

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.6	.7	.6	.5	.3	.5	.3
5.	.0	.6	.7	.6	.5	.3	.6	.3
10.	.0	.6	.6	.6	.4	.4	.7	.3
15.	.0	.6	.6	.5	.4	.4	.8	.3
20.	.0	.6	.5	.5	.4	.6	.8	.6
25.	.0	.8	.6	.6	.5	.7	.7	.6
30.	.0	.8	.6	.6	.6	.7	.6	.5
35.	.0	.8	.6	.6	.7	.7	.7	.5
40.	.0	.8	.7	.6	.6	.7	.7	.5
45.	.0	.8	.8	.6	.6	.7	.7	.5
50.	.1	.7	.8	.7	.8	.7	.7	.5
55.	.1	.8	.8	.7	.9	.7	.6	.4
60.	.1	.8	.7	.8	.8	.7	.6	.4
65.	.3	.8	.7	.7	.6	.6	.5	.4
70.	.4	.6	.5	.5	.5	.6	.4	.4
75.	.6	.5	.3	.3	.4	.4	.4	.4
80.	.7	.2	.2	.2	.3	.4	.4	.4
85.	.9	.1	.1	.2	.3	.4	.4	.4
90.	.7	.0	.1	.1	.2	.4	.4	.4
95.	.6	.1	.1	.1	.3	.4	.4	.4
100.	.6	.1	.1	.1	.3	.4	.4	.4
105.	.7	.1	.1	.1	.4	.4	.3	.4
110.	.7	.1	.1	.1	.4	.4	.3	.4
115.	.7	.0	.1	.1	.4	.4	.3	.4
120.	.7	.0	.1	.1	.3	.3	.3	.4
125.	.5	.0	.1	.1	.3	.3	.4	.4
130.	.5	.0	.1	.1	.3	.3	.4	.4
135.	.5	.0	.1	.1	.3	.3	.4	.4
140.	.5	.0	.0	.1	.3	.3	.3	.3
145.	.5	.0	.0	.0	.1	.2	.2	.2
150.	.5	.0	.0	.0	.1	.1	.1	.1
155.	.5	.0	.0	.0	.0	.0	.0	.0
160.	.5	.0	.0	.0	.0	.0	.0	.0
165.	.5	.0	.0	.0	.0	.0	.0	.0
170.	.5	.0	.0	.0	.0	.0	.0	.0
175.	.5	.0	.0	.0	.0	.0	.0	.0
180.	.6	.0	.0	.0	.0	.0	.0	.0
185.	.5	.0	.0	.0	.0	.0	.0	.0
190.	.5	.0	.0	.0	.0	.0	.0	.0
195.	.5	.0	.0	.0	.0	.0	.0	.0
200.	.5	.0	.0	.0	.0	.0	.0	.0
205.	.6	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 2 Veteran & Wilson (S2EXWPPM.DAT) RUN: Site 2 Existing WITH PROJ PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.6	.0	.0	.0	.0	.0	.0	.0
215.	.6	.0	.0	.0	.0	.0	.0	.0
220.	.7	.0	.0	.0	.0	.0	.0	.0
225.	.8	.0	.0	.0	.0	.0	.0	.0
230.	.7	.0	.0	.0	.0	.0	.0	.0
235.	.7	.1	.0	.0	.0	.0	.0	.0
240.	.5	.2	.2	.2	.1	.0	.0	.0
245.	.5	.3	.2	.2	.2	.0	.0	.0
250.	.3	.6	.4	.4	.3	.1	.0	.0
255.	.2	.6	.5	.5	.4	.1	.0	.0
260.	.2	.7	.6	.8	.6	.2	.1	.0
265.	.0	.8	.8	.8	.6	.2	.1	.0
270.	.0	.8	.8	.7	.7	.3	.1	.0
275.	.0	.8	.7	.7	.6	.3	.2	.0
280.	.0	.7	.7	.8	.7	.3	.3	.0
285.	.0	.7	.8	.8	.6	.3	.3	.0
290.	.0	.6	.8	.8	.6	.3	.3	.0
295.	.0	.7	.8	.7	.6	.3	.3	.0
300.	.0	.6	.6	.6	.6	.3	.3	.0
305.	.0	.7	.6	.6	.5	.3	.3	.1
310.	.0	.7	.6	.6	.4	.3	.3	.1
315.	.0	.6	.6	.6	.4	.3	.2	.1
320.	.0	.6	.6	.6	.5	.3	.2	.0
325.	.0	.5	.6	.6	.5	.3	.3	.2
330.	.0	.6	.6	.7	.4	.3	.4	.2
335.	.0	.6	.6	.7	.5	.4	.4	.2
340.	.0	.5	.7	.7	.5	.4	.2	.3
345.	.0	.6	.7	.7	.5	.3	.2	.3
350.	.0	.6	.7	.8	.4	.3	.3	.3
355.	.0	.6	.7	.8	.4	.3	.4	.3
360.	.0	.6	.7	.6	.5	.3	.5	.3
MAX	.9	.8	.8	.8	.9	.7	.8	.6
DEGR.	85	55	45	260	55	25	15	20

THE HIGHEST CONCENTRATION IS 1.10 PPM AT 240 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS 1.00 PPM AT 105 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS 1.00 PPM AT 90 DEGREES FROM REC10.

Site 3 – Glendon & Wilshire
Input Files

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Site 3 Glendon & Wilshire (S3EXAM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                   685.      365.       5.0
SE 164 S                   638.      508.       5.0
SE 82 S                    611.      586.       5.0
SE CNR                     595.      659.       5.0
SE 82 E                    664.      689.       5.0
SE 164 E                   742.      713.       5.0
SE MID E                   849.      747.       5.0
NE MID E                   793.      878.       5.0
NE 164 E                   674.      839.       5.0
NE 82 E                    595.      813.       5.0
NE CNR                     515.      792.       5.0
NE 82 N                    452.      847.       5.0
NE 164 N                   396.      907.       5.0
NE MID N                   319.      990.       5.0
NW MID N                   190.      983.       5.0
NW 164 N                   267.      900.       5.0
NW 82 N                    323.      841.       5.0
NW CNR                     381.      759.       5.0
NW 82 W                    299.      719.       5.0
NW 164 W                   222.      694.       5.0
NW MID W                   107.      658.       5.0
SW MID W                   213.      548.       5.0
SW 164 W                   367.      595.       5.0
SW 82 W                    447.      619.       5.0
SW CNR                     518.      634.       5.0
SW 82 S                    550.      565.       5.0
SW 164 S                   577.      487.       5.0
SW MID S                   622.      354.       5.0
Site 3 Existing AM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2246 3.3  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    1981 3.3  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
       150        35       2.0 1981   20.5 1001 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     265 3.3  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
       150       124       2.0  265   20.5 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    1928 3.3  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2442 3.3  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2375 3.3  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
       150        63       2.0 2375   20.5  991 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      67 3.3  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.       0.  12   1
```

```
       150        63       2.0   67   20.5   98 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2168 3.3  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     199 3.5  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       120       2.0  199   20.5 1143 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     757 3.5  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     229 3.5  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     117 3.5  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       120       2.0  117   20.5  806 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     112 3.5  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        96       2.0  112   20.5 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     263 3.5  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     263 3.5  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3EXPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 Existing PM                      22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    1996 3.3  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    1842 3.3  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
       150        56       2.0 1842   20.5 1008 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     154 3.3  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
       150       124       2.0  154     20.5 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2144 3.3  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2124 3.3  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2044 3.3  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
       150        74       2.0 2044   20.5  994 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      80 3.3  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.       0.  12   1
```

```
      150        74       2.0   80   20.5   50 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2158 3.3  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     367 3.5  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
      150        99       2.0  367   20.5  566 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     531 3.5  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     797 3.5  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     547 3.5  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
      150        99       2.0  547   20.5  838 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     250 3.5  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
      150        85       2.0  250   20.5 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     451 3.5  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     451 3.5  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3NBAM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                   685.      365.       5.0
SE 164 S                   638.      508.       5.0
SE 82 S                    611.      586.       5.0
SE CNR                     595.      659.       5.0
SE 82 E                    664.      689.       5.0
SE 164 E                   742.      713.       5.0
SE MID E                   849.      747.       5.0
NE MID E                   793.      878.       5.0
NE 164 E                   674.      839.       5.0
NE 82 E                    595.      813.       5.0
NE CNR                     515.      792.       5.0
NE 82 N                    452.      847.       5.0
NE 164 N                   396.      907.       5.0
NE MID N                   319.      990.       5.0
NW MID N                   190.      983.       5.0
NW 164 N                   267.      900.       5.0
NW 82 N                    323.      841.       5.0
NW CNR                     381.      759.       5.0
NW 82 W                    299.      719.       5.0
NW 164 W                   222.      694.       5.0
NW MID W                   107.      658.       5.0
SW MID W                   213.      548.       5.0
SW 164 W                   367.      595.       5.0
SW 82 W                    447.      619.       5.0
SW CNR                     518.      634.       5.0
SW 82 S                    550.      565.       5.0
SW 164 S                   577.      487.       5.0
SW MID S                   622.      354.       5.0
Site 3 NO BUILD AM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2967 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2763 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        39       2.0 2763   4.1  992 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     204 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  204   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2497 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3144 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3048 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        62       2.0 3048   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        62       2.0   96   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2816 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     311 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  311   4.1 1039 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     898 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     540 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     336 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  336   4.1  731 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     204 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        98       2.0  204   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     751 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     751 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3NBPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                   685.      365.       5.0
SE 164 S                   638.      508.       5.0
SE 82 S                    611.      586.       5.0
SE CNR                     595.      659.       5.0
SE 82 E                    664.      689.       5.0
SE 164 E                   742.      713.       5.0
SE MID E                   849.      747.       5.0
NE MID E                   793.      878.       5.0
NE 164 E                   674.      839.       5.0
NE 82 E                    595.      813.       5.0
NE CNR                     515.      792.       5.0
NE 82 N                    452.      847.       5.0
NE 164 N                   396.      907.       5.0
NE MID N                   319.      990.       5.0
NW MID N                   190.      983.       5.0
NW 164 N                   267.      900.       5.0
NW 82 N                    323.      841.       5.0
NW CNR                     381.      759.       5.0
NW 82 W                    299.      719.       5.0
NW 164 W                   222.      694.       5.0
NW MID W                   107.      658.       5.0
SW MID W                   213.      548.       5.0
SW 164 W                   367.      595.       5.0
SW 82 W                    447.      619.       5.0
SW CNR                     518.      634.       5.0
SW 82 S                    550.      565.       5.0
SW 164 S                   577.      487.       5.0
SW MID S                   622.      354.       5.0
Site 3 NO BUILD PM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2690 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2457 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2457   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     233 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       129       2.0  233   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2819 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2887 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2754 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        79       2.0 2754   4.1  991 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     133 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
      150        79       2.0  133   4.1   68 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    3052 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     899 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
      150        99       2.0  899   4.1  276 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     960 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1017 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     713 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
      150        99       2.0  713   4.1  836 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     304 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
      150        80       2.0  304   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     662 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     662 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B1AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 1  AM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2885 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2690 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
       150        39       2.0 2690   4.1  994 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     195 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
       150       130       2.0  195   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2465 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3121 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3035 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
       150        62       2.0 3035   4.1  924 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      86 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.       0.  12   1
```

```
       150        62       2.0   86   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2899 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     388 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  388   4.1 1069 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     929 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     593 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     330 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  330   4.1  678 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     263 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        98       2.0  263   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     694 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     694 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

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Site 3 Glendon & Wilshire (S3B1PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                   685.      365.       5.0
SE 164 S                   638.      508.       5.0
SE 82 S                    611.      586.       5.0
SE CNR                     595.      659.       5.0
SE 82 E                    664.      689.       5.0
SE 164 E                   742.      713.       5.0
SE MID E                   849.      747.       5.0
NE MID E                   793.      878.       5.0
NE 164 E                   674.      839.       5.0
NE 82 E                    595.      813.       5.0
NE CNR                     515.      792.       5.0
NE 82 N                    452.      847.       5.0
NE 164 N                   396.      907.       5.0
NE MID N                   319.      990.       5.0
NW MID N                   190.      983.       5.0
NW 164 N                   267.      900.       5.0
NW 82 N                    323.      841.       5.0
NW CNR                     381.      759.       5.0
NW 82 W                    299.      719.       5.0
NW 164 W                   222.      694.       5.0
NW MID W                   107.      658.       5.0
SW MID W                   213.      548.       5.0
SW 164 W                   367.      595.       5.0
SW 82 W                    447.      619.       5.0
SW CNR                     518.      634.       5.0
SW 82 S                    550.      565.       5.0
SW 164 S                   577.      487.       5.0
SW MID S                   622.      354.       5.0
Site 3 BUILD A1 PM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2704 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2475 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2475   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     229 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  229   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2819 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2895 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2762 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        78       2.0 2762   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     133 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
      150        78       2.0  133   4.1   68 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    3001 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     870 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
      150        99       2.0  870   4.1  280 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     988 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1004 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     699 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
      150        99       2.0  699   4.1  816 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     305 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
      150        81       2.0  305   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     665 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     665 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
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```
Site 3 Glendon & Wilshire (S3B2AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                   685.      365.       5.0
SE 164 S                   638.      508.       5.0
SE 82 S                    611.      586.       5.0
SE CNR                     595.      659.       5.0
SE 82 E                    664.      689.       5.0
SE 164 E                   742.      713.       5.0
SE MID E                   849.      747.       5.0
NE MID E                   793.      878.       5.0
NE 164 E                   674.      839.       5.0
NE 82 E                    595.      813.       5.0
NE CNR                     515.      792.       5.0
NE 82 N                    452.      847.       5.0
NE 164 N                   396.      907.       5.0
NE MID N                   319.      990.       5.0
NW MID N                   190.      983.       5.0
NW 164 N                   267.      900.       5.0
NW 82 N                    323.      841.       5.0
NW CNR                     381.      759.       5.0
NW 82 W                    299.      719.       5.0
NW 164 W                   222.      694.       5.0
NW MID W                   107.      658.       5.0
SW MID W                   213.      548.       5.0
SW 164 W                   367.      595.       5.0
SW 82 W                    447.      619.       5.0
SW CNR                     518.      634.       5.0
SW 82 S                    550.      565.       5.0
SW 164 S                   577.      487.       5.0
SW MID S                   622.      354.       5.0
Site 3 BUILD 2  AM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2910 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2733 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
       150        39       2.0 2733   4.1  993 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     177 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
       150       131       2.0  177   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2513 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3134 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3039 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
       150        60       2.0 3039   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      95 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.       0.  12   1
```

```
       150        60       2.0   95   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2846 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     382 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  382   4.1 1075 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     951 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     604 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     352 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  352   4.1  681 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     252 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        99       2.0  252   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     720 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     720 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B2PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A2 PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2692 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2479 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2479   4.1 1006 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     229 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  229   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2820 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2921 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2789 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        77       2.0 2789   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
      150        77       2.0  132   4.1   66 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    3052 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     888 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
      150        99       2.0  888   4.1  268 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     964 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1003 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     706 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
      150        99       2.0  706   4.1  833 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     303 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
      150        83       2.0  303   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     674 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     674 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B3AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 3  AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2883 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2678 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
       150        39       2.0 2678   4.1  994 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     205 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
       150       129       2.0  205   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2652 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3101 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3005 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
       150        62       2.0 3005   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.       0.  12   1
```

```
       150        62       2.0   96   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2818 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     316 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  316   4.1 1046 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     885 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     570 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     340 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  340   4.1  727 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     230 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        97       2.0  230   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     698 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     698 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B3PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A3 PM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2689 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2449 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2449   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     240 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       129       2.0  240   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2786 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2876 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2744 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        79       2.0 2744   4.1  991 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
      150        79       2.0  132   4.1   68 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2979 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     855 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
      150        99       2.0  855   4.1  262 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     973 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     998 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     708 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
      150        99       2.0  708   4.1  808 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     290 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
      150        80       2.0  290   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     680 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     680 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B4AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 4  AM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2883 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2701 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
       150        39       2.0 2701   4.1  994 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     182 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
       150       131       2.0  182   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2517 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3126 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3030 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
       150        60       2.0 3030   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.       0.  12   1
```

```
       150        60       2.0   96   4.1   53 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2821 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     371 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  371   4.1 1064 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     928 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     583 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     363 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  363   4.1  689 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     220 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        99       2.0  220   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     697 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     697 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B4PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A4 PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2660 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2445 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2445   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     205 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       131       2.0  205   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2820 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2950 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2818 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        77       2.0 2818   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
      150        77       2.0  132   4.1   66 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    3022 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     880 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
      150        99       2.0  880   4.1  282 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.    1010 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1034 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     727 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
      150        99       2.0  727   4.1  794 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     307 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
      150        82       2.0  307   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     672 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     672 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B5AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 5  AM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2901 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2690 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
       150        45       2.0 2690   4.1  992 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     211 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
       150       137       2.0  211   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2446 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3128 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3032 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
       150        60       2.0 3032   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.       0.  12   1
```

```
       150        60       2.0   96   4.1   53 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2795 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     374 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       110       2.0  374   4.1 1141 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     975 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     574 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     367 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       110       2.0  367   4.1  733 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     207 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        99       2.0  207   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     761 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     761 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B5PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A5 PM                        22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2699 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2469 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2469   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     230 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  230   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2814 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2904 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2772 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        78       2.0 2772   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
      150        78       2.0  132   4.1   68 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2979 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     881 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
      150        99       2.0  881   4.1  285 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.    1031 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1010 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     705 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
      150        99       2.0  705   4.1  804 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     305 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
      150        81       2.0  305   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     670 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     670 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

Site 3 – Glendon & Wilshire
Output Files

JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT) RUN: Site 3 Existing AM
DATE: 03/22/2010 TIME: 09:10:02.31

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB	Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2246.	3.3	.0	68.0		
2. EB	Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	1981.	3.3	.0	68.0		
3. EB	Wil T+R	475.0	663.0	384.5	635.1	95.	253.	AG	51.	100.0	.0	48.0	.67	4.8
4. EB	Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	265.	3.3	.0	44.0		
5. EB	Wil LT	444.0	690.0	342.0	658.7	107.	253.	AG	91.	100.0	.0	24.0	.84	5.4
6. EB	Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	1928.	3.3	.0	68.0		
7. WB	Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	2442.	3.3	.0	68.0		
8. WB	Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	2375.	3.3	.0	68.0		
9. WB	Wil T+R	540.0	760.0	1274.1	994.4	771.	72.	AG	92.	100.0	.0	48.0	1.08	39.1
10. WB	Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	67.	3.3	.0	32.0		
11. WB	Wil LT	566.0	723.0	751.9	784.3	196.	72.	AG	23.	100.0	.0	12.0	1.24	9.9
12. WB	Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2168.	3.3	.0	68.0		
13. NB	Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	199.	3.5	.0	32.0		
14. NB	Gln AP	564.0	640.0	632.8	442.4	209.	161.	AG	44.	100.0	.0	12.0	1.01	10.6
15. NB	Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	757.	3.5	.0	32.0		
16. SB	Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	229.	3.5	.0	32.0		
17. SB	Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	117.	3.5	.0	44.0		
18. SB	Gln T+LT	430.0	786.0	403.5	813.3	38.	316.	AG	88.	100.0	.0	24.0	.42	1.9
19. SB	Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	112.	3.5	.0	32.0		
20. SB	Gln R	400.0	780.0	360.7	823.7	59.	318.	AG	35.	100.0	.0	12.0	.34	3.0
21. SB	Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	263.	3.5	.0	32.0		
22. SB	Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	263.	3.5	.0	32.0		

JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT) RUN: Site 3 Existing AM
DATE: 03/22/2010 TIME: 09:10:02.31

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB	Wil T+R	150	35	2.0	1981	1001	20.50	1	3
5. EB	Wil LT	150	124	2.0	265	1084	20.50	1	3
9. WB	Wil T+R	150	63	2.0	2375	991	20.50	1	3
11. WB	Wil LT	150	63	2.0	67	98	20.50	1	3
14. NB	Gln AP	150	120	2.0	199	1143	20.50	1	3
18. SB	Gln T+LT	150	120	2.0	117	806	20.50	1	3
20. SB	Gln R	150	96	2.0	112	1000	20.50	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT) RUN: Site 3 Existing AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
5. *	.0	.3	.3	.4	.4	.5	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
10. *	.0	.2	.3	.4	.4	.5	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
15. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0
20. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0
25. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0
30. *	.0	.3	.2	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
35. *	.0	.3	.3	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
40. *	.0	.3	.3	.5	.6	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
45. *	.0	.3	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
50. *	.0	.3	.3	.6	.5	.5	.5	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1
55. *	.0	.1	.3	.5	.5	.5	.5	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
60. *	.0	.0	.3	.5	.5	.5	.5	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.2	.1	.1
65. *	.0	.0	.1	.4	.5	.5	.5	.3	.4	.4	.3	.0	.0	.0	.0	.0	.0	.3	.3	.3
70. *	.0	.0	.1	.4	.5	.5	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.3	.4	.4
75. *	.0	.0	.0	.2	.2	.2	.2	.7	.7	.7	.7	.2	.0	.0	.0	.0	.1	.5	.6	.5
80. *	.0	.0	.0	.1	.2	.2	.1	.8	.8	.8	.8	.2	.0	.0	.0	.0	.2	.6	.5	.6
85. *	.0	.0	.0	.1	.1	.1	.1	.9	.9	.9	.8	.3	.2	.0	.0	.1	.2	.5	.6	.6
90. *	.0	.0	.0	.0	.1	.1	.1	.9	.9	.9	.8	.4	.2	.0	.0	.1	.4	.4	.6	.6
95. *	.0	.0	.0	.0	.1	.0	.0	.9	.9	.9	.7	.4	.3	.2	.1	.1	.3	.4	.6	.5
100. *	.0	.0	.0	.0	.0	.0	.0	.7	.8	.8	.7	.3	.3	.1	.1	.2	.3	.5	.6	.5
105. *	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.7	.3	.3	.1	.1	.3	.3	.4	.5	.5
110. *	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.7	.3	.3	.1	.1	.2	.3	.4	.5	.4
115. *	.0	.0	.0	.0	.0	.0	.0	.7	.6	.7	.6	.3	.3	.1	.0	.1	.2	.3	.4	.4
120. *	.0	.0	.0	.0	.0	.0	.0	.7	.6	.7	.5	.3	.3	.1	.0	.0	.1	.3	.4	.3
125. *	.0	.0	.0	.0	.0	.0	.0	.7	.6	.7	.5	.3	.3	.2	.0	.0	.1	.3	.4	.4
130. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.2	.1	.0	.0	.1	.3	.4	.3
135. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.1	.1	.0	.0	.1	.4	.4	.3
140. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.2	.1	.0	.1	.1	.4	.4	.3
145. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.2	.1	.0	.1	.2	.4	.4	.3
150. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.1	.1	.0	.1	.2	.5	.3	.3
155. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.1	.1	.0	.1	.3	.5	.3	.3
160. *	.0	.0	.0	.0	.0	.0	.0	.7	.6	.6	.3	.2	.2	.1	.0	.1	.3	.5	.3	.3
165. *	.0	.0	.1	.0	.0	.0	.0	.7	.6	.6	.3	.4	.2	.1	.0	.1	.2	.5	.4	.3
170. *	.0	.0	.1	.1	.0	.0	.0	.6	.6	.6	.4	.3	.2	.2	.0	.1	.1	.4	.3	.3
175. *	.0	.0	.1	.1	.0	.0	.0	.6	.6	.6	.4	.3	.2	.2	.0	.1	.1	.4	.3	.3
180. *	.0	.0	.1	.1	.0	.0	.0	.6	.6	.6	.4	.3	.2	.2	.0	.1	.1	.4	.3	.3
185. *	.0	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.3	.2	.2	.1	.1	.1	.4	.3	.3
190. *	.0	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.3	.2	.2	.1	.2	.2	.4	.3	.3
195. *	.0	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.5	.2	.2	.1	.2	.2	.4	.3	.3
200. *	.0	.1	.1	.1	.0	.0	.0	.7	.7	.7	.5	.5	.2	.2	.1	.2	.2	.4	.3	.3
205. *	.0	.1	.1	.1	.0	.0	.0	.7	.7	.7	.5	.4	.3	.2	.1	.2	.2	.4	.3	.3

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JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT) RUN: Site 3 Existing AM

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.1	.1	.1	.0	.0	.0	.7	.7	.7	.5	.3	.3	.3	.1	.2	.2	.3	.4	.4
215. *	.0	.1	.1	.1	.0	.0	.0	.7	.7	.7	.6	.4	.3	.2	.1	.2	.2	.3	.4	.4
220. *	.0	.1	.1	.1	.0	.0	.0	.7	.7	.6	.5	.4	.3	.2	.0	.2	.2	.3	.4	.4
225. *	.0	.1	.1	.1	.0	.0	.0	.8	.7	.7	.7	.4	.3	.2	.0	.2	.2	.3	.4	.4
230. *	.0	.1	.1	.1	.0	.0	.0	.8	.7	.7	.7	.4	.3	.1	.0	.1	.2	.4	.4	.4
235. *	.0	.1	.1	.0	.0	.1	.1	.7	.8	.8	.6	.4	.2	.1	.0	.1	.2	.4	.4	.4
240. *	.0	.1	.1	.0	.1	.1	.1	.7	.7	.5	.5	.4	.2	.1	.0	.0	.1	.4	.4	.4
245. *	.0	.1	.1	.2	.2	.1	.1	.7	.7	.6	.5	.2	.1	.1	.0	.0	.1	.3	.4	.4
250. *	.0	.1	.1	.2	.4	.3	.2	.6	.6	.6	.5	.2	.1	.1	.0	.0	.0	.3	.4	.4
255. *	.0	.1	.2	.3	.5	.5	.3	.5	.4	.4	.4	.1	.1	.1	.0	.0	.0	.2	.3	.3
260. *	.0	.1	.2	.4	.5	.5	.3	.4	.3	.2	.2	.1	.1	.1	.0	.0	.0	.1	.2	.2
265. *	.0	.2	.3	.4	.5	.3	.6	.3	.1	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1
270. *	.0	.2	.3	.5	.4	.4	.6	.0	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1
275. *	.0	.3	.4	.4	.4	.4	.5	.0	.1	.0	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1
280. *	.0	.3	.3	.4	.4	.5	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
285. *	.0	.2	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
290. *	.0	.2	.3	.3	.3	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
295. *	.0	.2	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
300. *	.0	.3	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
305. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
310. *	.0	.3	.3	.4	.4	.4	.5	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
315. *	.0	.2	.2	.4	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320. *	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325. *	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.1	.2	.5	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
340. *	.0	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
345. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
350. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
355. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
360. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
MAX *	.0	.3	.4	.6	.6	.5	.6	.9	.9	.9	.8	.5	.3	.3	.1	.3	.4	.6	.6	.6
DEGR. *	0	0	275	50	40	5	265	85	85	85	80	195	95	210	95	105	90	80	75	80

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JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT) RUN: Site 3 Existing AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.3	.4	.5	.2	.2	.2	.1

5.	*	.0	.3	.4	.4	.3	.3	.4	.0
10.	*	.0	.3	.4	.4	.4	.3	.4	.0
15.	*	.0	.3	.5	.5	.4	.4	.4	.0
20.	*	.0	.3	.5	.5	.4	.4	.3	.1
25.	*	.0	.4	.5	.4	.4	.4	.3	.1
30.	*	.0	.4	.5	.5	.4	.4	.3	.1
35.	*	.0	.4	.5	.5	.4	.4	.3	.0
40.	*	.0	.4	.6	.6	.5	.3	.4	.0
45.	*	.0	.4	.7	.6	.5	.4	.4	.0
50.	*	.1	.5	.6	.6	.5	.4	.4	.0
55.	*	.1	.6	.7	.7	.5	.4	.2	.0
60.	*	.1	.6	.7	.7	.4	.4	.1	.0
65.	*	.2	.5	.7	.6	.4	.2	.1	.0
70.	*	.3	.5	.5	.5	.4	.2	.1	.0
75.	*	.4	.4	.5	.3	.2	.1	.1	.0
80.	*	.5	.2	.2	.2	.1	.1	.1	.0
85.	*	.4	.1	.1	.2	.1	.1	.1	.0
90.	*	.3	.1	.1	.0	.0	.1	.1	.0
95.	*	.4	.1	.1	.0	.0	.1	.1	.0
100.	*	.4	.0	.0	.0	.1	.1	.1	.0
105.	*	.4	.0	.0	.0	.1	.1	.1	.0
110.	*	.4	.0	.0	.0	.1	.1	.1	.0
115.	*	.3	.0	.0	.0	.1	.1	.1	.0
120.	*	.3	.0	.0	.0	.1	.1	.1	.0
125.	*	.3	.0	.0	.0	.1	.1	.0	.0
130.	*	.3	.0	.0	.0	.1	.1	.0	.0
135.	*	.3	.0	.0	.0	.1	.1	.0	.0
140.	*	.3	.0	.0	.0	.1	.1	.0	.0
145.	*	.3	.0	.0	.0	.1	.1	.0	.0
150.	*	.3	.0	.0	.0	.0	.0	.0	.0
155.	*	.3	.0	.0	.0	.0	.0	.0	.0
160.	*	.3	.0	.0	.0	.0	.0	.0	.0
165.	*	.3	.0	.0	.0	.0	.0	.0	.0
170.	*	.3	.0	.0	.0	.0	.0	.0	.0
175.	*	.3	.0	.0	.0	.0	.0	.0	.0
180.	*	.3	.0	.0	.0	.0	.0	.0	.0
185.	*	.3	.0	.0	.0	.0	.0	.0	.0
190.	*	.3	.0	.0	.0	.0	.0	.0	.0
195.	*	.3	.0	.0	.0	.0	.0	.0	.0
200.	*	.3	.0	.0	.0	.0	.0	.0	.0
205.	*	.3	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT) RUN: Site 3 Existing AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.4	.0	.0	.0	.0	.0	.0	.0
215.	*	.4	.0	.0	.0	.0	.0	.0	.0
220.	*	.4	.0	.0	.0	.0	.0	.0	.0
225.	*	.4	.1	.0	.0	.0	.0	.0	.0
230.	*	.4	.1	.0	.0	.0	.0	.0	.0
235.	*	.4	.1	.1	.1	.0	.0	.0	.0
240.	*	.4	.2	.1	.2	.0	.0	.0	.0
245.	*	.4	.2	.3	.2	.2	.0	.0	.0
250.	*	.4	.3	.3	.2	.2	.0	.0	.0
255.	*	.2	.4	.4	.5	.3	.1	.0	.0
260.	*	.2	.5	.5	.5	.5	.1	.0	.0
265.	*	.1	.5	.5	.5	.5	.2	.1	.0
270.	*	.1	.5	.5	.5	.5	.2	.1	.0
275.	*	.1	.4	.4	.5	.6	.2	.2	.0
280.	*	.0	.4	.4	.5	.5	.3	.2	.0
285.	*	.0	.4	.4	.5	.5	.3	.2	.0
290.	*	.0	.4	.3	.5	.5	.2	.2	.0
295.	*	.0	.4	.3	.5	.5	.2	.1	.0
300.	*	.0	.4	.3	.5	.5	.2	.1	.0
305.	*	.0	.3	.4	.5	.5	.3	.1	.0
310.	*	.0	.3	.4	.5	.5	.2	.2	.0
315.	*	.0	.3	.4	.5	.3	.2	.2	.0
320.	*	.0	.3	.3	.5	.3	.2	.2	.0
325.	*	.0	.3	.3	.5	.3	.2	.1	.0
330.	*	.0	.3	.3	.5	.4	.2	.1	.0
335.	*	.0	.3	.4	.5	.4	.1	.1	.0
340.	*	.0	.3	.4	.5	.5	.1	.0	.0
345.	*	.0	.3	.4	.5	.4	.2	.0	.0
350.	*	.0	.3	.4	.5	.3	.1	.0	.0
355.	*	.0	.3	.4	.5	.3	.2	.2	.1
360.	*	.0	.3	.4	.5	.2	.2	.2	.1
MAX	*	.5	.6	.7	.7	.6	.4	.4	.1
DEGR.	*	80	55	45	55	275	15	5	0

THE HIGHEST CONCENTRATION IS .90 PPM AT 85 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .90 PPM AT 85 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .90 PPM AT 85 DEGREES FROM REC10.

JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT) RUN: Site 3 Existing PM
DATE: 03/22/2010 TIME: 09:47:43.86

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	1996.	3.3	.0	68.0		
2. EB Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	1842.	3.3	.0	68.0		
3. EB Wil T+R	475.0	663.0	340.4	621.5	141.	253.	AG	82.	100.0	.0	48.0	.76	7.2
4. EB Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	154.	3.3	.0	44.0		
5. EB Wil LT	444.0	690.0	365.9	666.0	82.	253.	AG	1.	100.0	.0	24.0	1.04	4.2
6. EB Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2144.	3.3	.0	68.0		
7. WB Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	2124.	3.3	.0	68.0		
8. WB Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	2044.	3.3	.0	68.0		
9. WB Wil T+R	540.0	760.0	1164.2	959.3	655.	72.	AG	109.	100.0	.0	48.0	1.07	33.3
10. WB Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	80.	3.3	.0	32.0		
11. WB Wil LT	566.0	723.0	1196.3	931.0	664.	72.	AG	27.	100.0	.0	12.0	3.33	33.7
12. WB Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2158.	3.3	.0	68.0		
13. NB Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	367.	3.5	.0	32.0		
14. NB Gln AP	564.0	640.0	1288.8	-1440.6	2203.	161.	AG	36.	100.0	.0	12.0	2.07	111.9
15. NB Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	531.	3.5	.0	32.0		
16. SB Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	797.	3.5	.0	32.0		
17. SB Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	547.	3.5	.0	44.0		
18. SB Gln T+LT	430.0	786.0	194.3	1028.4	338.	316.	AG	73.	100.0	.0	24.0	1.04	17.2
19. SB Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	250.	3.5	.0	32.0		
20. SB Gln R	400.0	780.0	322.3	866.4	116.	318.	AG	31.	100.0	.0	12.0	.62	5.9
21. SB Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	451.	3.5	.0	32.0		
22. SB Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	451.	3.5	.0	32.0		

JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT) RUN: Site 3 Existing PM
DATE: 03/22/2010 TIME: 09:47:43.86

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	150	56	2.0	1842	1008	20.50	1	3
5. EB Wil LT	150	124	2.0	154	510	.20	4	1
9. WB Wil T+R	150	74	2.0	2044	994	20.50	1	3
11. WB Wil LT	150	74	2.0	80	50	20.50	1	3
14. NB Gln AP	150	99	2.0	367	566	20.50	1	3
18. SB Gln T+LT	150	99	2.0	547	838	20.50	1	3
20. SB Gln R	150	85	2.0	250	1000	20.50	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT) RUN: Site 3 Existing PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.1	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.2	.1	.0
5. *	.1	.2	.3	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.2	.1	.0
10. *	.1	.2	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.2	.1	.0
15. *	.1	.2	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.2	.1	.0
20. *	.1	.2	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.2	.1	.0
25. *	.1	.2	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.1	.1	.1
30. *	.0	.2	.2	.5	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.1	.1	.1
35. *	.0	.3	.2	.5	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.1	.0
40. *	.0	.3	.3	.6	.6	.6	.6	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.1	.0
45. *	.0	.3	.3	.7	.6	.6	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.1	.0
50. *	.0	.1	.3	.6	.6	.6	.5	.1	.0	.0	.0	.0	.0	.0	.3	.3	.3	.1	.1	.1
55. *	.0	.1	.3	.5	.5	.5	.5	.2	.1	.2	.1	.0	.0	.0	.3	.3	.3	.1	.1	.1
60. *	.0	.0	.3	.5	.5	.5	.5	.2	.3	.3	.2	.0	.0	.0	.3	.2	.3	.2	.2	.1
65. *	.0	.0	.1	.5	.5	.5	.5	.3	.4	.4	.4	.0	.0	.0	.3	.2	.3	.3	.2	.3
70. *	.0	.0	.1	.4	.5	.5	.4	.4	.5	.6	.4	.0	.0	.0	.3	.2	.3	.3	.5	.3
75. *	.0	.0	.0	.2	.2	.2	.2	.7	.7	.7	.7	.2	.0	.0	.3	.2	.5	.6	.5	.4
80. *	.0	.0	.0	.1	.2	.2	.2	.7	.8	.8	.8	.2	.0	.0	.3	.2	.5	.6	.5	.5
85. *	.0	.0	.0	.1	.1	.1	.1	.8	.8	.8	.8	.3	.2	.0	.3	.3	.7	.5	.6	.5
90. *	.0	.0	.0	.0	.1	.1	.1	.8	.9	.9	.9	.5	.3	.0	.3	.3	.6	.4	.6	.6
95. *	.0	.0	.0	.0	.1	.1	.0	.8	.8	.8	.8	.5	.3	.1	.4	.4	.7	.4	.4	.6
100. *	.0	.0	.0	.0	.0	.0	.0	.8	.8	.8	.7	.4	.2	.1	.4	.5	.7	.4	.5	.5
105. *	.0	.0	.0	.0	.0	.0	.0	.8	.8	.7	.6	.4	.2	.1	.4	.5	.6	.4	.5	.5
110. *	.0	.0	.0	.0	.0	.0	.0	.8	.8	.7	.6	.4	.3	.1	.4	.5	.6	.4	.5	.5
115. *	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.6	.3	.3	.1	.4	.4	.6	.3	.4	.4
120. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.7	.6	.3	.3	.1	.2	.2	.2	.3	.4	.4
125. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.3	.1	.2	.1	.3	.3	.4	.3
130. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.3	.1	.1	.1	.3	.3	.4	.3
135. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.2	.0	.1	.1	.2	.4	.4	.3
140. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.1	.0	.1	.1	.1	.4	.4	.3
145. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.1	.2	.0	.1	.2	.4	.4	.3
150. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.1	.2	.0	.1	.3	.4	.4	.3
155. *	.1	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.2	.1	.2	.0	.1	.3	.4	.4	.3
160. *	.1	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.2	.3	.2	.0	.1	.3	.4	.3	.3
165. *	.2	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.2	.3	.2	.0	.1	.2	.4	.3	.3
170. *	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.3	.3	.3	.0	.1	.1	.4	.3	.3
175. *	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.3	.3	.3	.0	.1	.1	.4	.3	.3
180. *	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.3	.3	.3	.0	.1	.1	.4	.3	.3
185. *	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.4	.3	.3	.0	.1	.1	.4	.3	.3
190. *	.2	.2	.1	.1	.0	.0	.0	.6	.6	.6	.3	.4	.3	.3	.0	.1	.1	.4	.3	.3
195. *	.2	.1	.1	.1	.0	.0	.0	.6	.6	.6	.3	.4	.3	.3	.1	.1	.2	.4	.3	.3
200. *	.1	.1	.1	.1	.0	.0	.0	.6	.6	.6	.5	.5	.3	.3	.1	.2	.2	.3	.3	.3
205. *	.1	.1	.1	.1	.0	.0	.0	.7	.6	.6	.5	.3	.3	.3	.1	.2	.2	.3	.3	.3

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JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT) RUN: Site 3 Existing PM

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.1	.1	.1	.1	.0	.0	.0	.8	.7	.7	.4	.3	.4	.3	.1	.2	.2	.3	.4	.4
215. *	.1	.1	.1	.1	.0	.0	.0	.8	.7	.6	.4	.3	.4	.3	.1	.2	.2	.3	.4	.4
220. *	.1	.1	.1	.1	.0	.0	.0	.8	.8	.6	.4	.4	.4	.3	.0	.2	.2	.3	.4	.4
225. *	.1	.1	.1	.0	.0	.0	.0	.7	.8	.8	.5	.4	.4	.3	.0	.1	.2	.3	.4	.4
230. *	.1	.1	.1	.0	.0	.0	.0	.8	.6	.7	.6	.4	.4	.2	.0	.1	.2	.4	.4	.4
235. *	.1	.1	.1	.0	.1	.1	.1	.8	.7	.7	.4	.4	.3	.2	.0	.1	.2	.4	.4	.4
240. *	.1	.1	.1	.0	.1	.1	.1	.9	.7	.6	.4	.4	.3	.2	.0	.0	.1	.4	.4	.4
245. *	.1	.1	.1	.1	.1	.1	.1	.7	.6	.6	.4	.3	.2	.2	.0	.0	.1	.3	.4	.4
250. *	.1	.1	.1	.3	.4	.3	.2	.5	.5	.6	.4	.3	.2	.2	.0	.0	.0	.3	.4	.4
255. *	.1	.1	.2	.4	.6	.4	.3	.5	.4	.3	.2	.2	.2	.2	.0	.0	.0	.2	.3	.3
260. *	.1	.1	.2	.5	.6	.3	.4	.4	.3	.2	.1	.2	.2	.2	.0	.0	.0	.1	.2	.2
265. *	.1	.1	.3	.5	.5	.4	.6	.2	.2	.2	.2	.2	.2	.3	.0	.0	.0	.1	.1	.1
270. *	.1	.2	.3	.4	.4	.4	.6	.0	.1	.2	.1	.2	.2	.3	.0	.0	.0	.0	.1	.1
275. *	.1	.3	.5	.4	.4	.6	.5	.0	.0	.1	.2	.2	.2	.3	.0	.0	.0	.0	.1	.1
280. *	.1	.3	.4	.4	.3	.5	.5	.0	.0	.1	.2	.2	.2	.3	.0	.0	.0	.0	.0	.0
285. *	.1	.2	.4	.3	.4	.5	.5	.0	.0	.1	.2	.2	.2	.3	.0	.0	.0	.0	.0	.0
290. *	.1	.2	.4	.3	.3	.4	.6	.0	.0	.1	.2	.2	.2	.3	.0	.0	.0	.0	.0	.0
295. *	.1	.2	.4	.3	.4	.4	.5	.0	.0	.1	.2	.2	.3	.2	.0	.0	.0	.0	.0	.0
300. *	.1	.3	.3	.4	.4	.4	.5	.0	.0	.0	.2	.2	.3	.2	.0	.0	.0	.0	.0	.0
305. *	.2	.3	.3	.5	.4	.4	.5	.0	.0	.0	.2	.2	.3	.2	.0	.0	.0	.0	.0	.0
310. *	.2	.3	.3	.5	.4	.4	.6	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0
315. *	.2	.1	.2	.5	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.1	.1	.0	.0
320. *	.2	.1	.0	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
325. *	.2	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
330. *	.2	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
335. *	.1	.0	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.0	.0
340. *	.1	.1	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.3	.3	.2	.0	.0
345. *	.0	.2	.3	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.3	.2	.2	.0	.0
350. *	.0	.3	.3	.4	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.1	.3	.2	.2	.1	.0
355. *	.1	.3	.3	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.1	.0
360. *	.1	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.2	.1	.0
MAX *	.2	.3	.5	.7	.7	.6	.6	.9	.9	.9	.9	.5	.4	.3	.4	.5	.7	.6	.6	.6
DEGR. *	165	35	275	45	35	35	35	240	90	90	90	90	210	170	95	100	85	75	85	90

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JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT) RUN: Site 3 Existing PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.3	.6	.5	.3	.3	.4	.2

5.	*	.0	.3	.5	.5	.5	.4	.4	.3
10.	*	.0	.3	.5	.5	.5	.4	.4	.3
15.	*	.0	.3	.5	.5	.4	.4	.4	.3
20.	*	.0	.3	.6	.6	.4	.4	.4	.3
25.	*	.0	.3	.6	.5	.4	.5	.4	.4
30.	*	.0	.3	.6	.6	.4	.5	.4	.4
35.	*	.0	.3	.6	.6	.6	.4	.4	.3
40.	*	.0	.3	.8	.6	.6	.4	.4	.2
45.	*	.0	.3	.7	.6	.5	.5	.5	.2
50.	*	.1	.4	.8	.6	.6	.4	.4	.1
55.	*	.1	.6	.7	.8	.7	.4	.3	.2
60.	*	.1	.7	.7	.8	.5	.5	.3	.2
65.	*	.2	.6	.6	.6	.4	.3	.2	.2
70.	*	.3	.6	.5	.4	.4	.3	.2	.2
75.	*	.5	.4	.5	.3	.2	.2	.2	.2
80.	*	.5	.2	.3	.2	.1	.2	.2	.2
85.	*	.5	.1	.2	.2	.1	.2	.2	.2
90.	*	.3	.1	.1	.0	.0	.2	.2	.2
95.	*	.3	.0	.0	.0	.0	.2	.2	.2
100.	*	.4	.0	.0	.0	.0	.2	.2	.2
105.	*	.4	.0	.0	.0	.0	.2	.2	.2
110.	*	.4	.0	.0	.0	.1	.2	.2	.2
115.	*	.3	.0	.0	.0	.1	.2	.2	.2
120.	*	.3	.0	.0	.0	.1	.2	.2	.2
125.	*	.3	.0	.0	.0	.1	.2	.2	.2
130.	*	.3	.0	.0	.0	.2	.2	.2	.2
135.	*	.3	.0	.0	.0	.2	.2	.2	.2
140.	*	.3	.0	.0	.0	.2	.2	.2	.2
145.	*	.3	.0	.0	.0	.2	.2	.2	.2
150.	*	.3	.0	.0	.0	.2	.2	.2	.2
155.	*	.3	.0	.0	.0	.2	.2	.2	.2
160.	*	.3	.0	.0	.0	.1	.2	.2	.2
165.	*	.3	.0	.0	.0	.0	.2	.2	.2
170.	*	.3	.0	.0	.0	.0	.0	.0	.0
175.	*	.3	.0	.0	.0	.0	.0	.0	.0
180.	*	.3	.0	.0	.0	.0	.0	.0	.0
185.	*	.3	.0	.0	.0	.0	.0	.0	.0
190.	*	.3	.0	.0	.0	.0	.0	.0	.0
195.	*	.3	.0	.0	.0	.0	.0	.0	.0
200.	*	.3	.0	.0	.0	.0	.0	.0	.0
205.	*	.3	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT) RUN: Site 3 Existing PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.4	.0	.0	.0	.0	.0	.0	.0
215.	*	.4	.0	.0	.0	.0	.0	.0	.0
220.	*	.4	.0	.0	.0	.0	.0	.0	.0
225.	*	.4	.1	.0	.0	.0	.0	.0	.0
230.	*	.4	.1	.0	.0	.0	.0	.0	.0
235.	*	.4	.1	.1	.0	.0	.0	.0	.0
240.	*	.4	.1	.1	.2	.0	.0	.0	.0
245.	*	.4	.2	.2	.2	.2	.0	.0	.0
250.	*	.3	.3	.3	.3	.3	.0	.0	.0
255.	*	.2	.4	.4	.4	.4	.1	.0	.0
260.	*	.2	.4	.4	.5	.5	.1	.0	.0
265.	*	.1	.4	.4	.6	.6	.2	.0	.0
270.	*	.1	.4	.4	.6	.6	.2	.1	.0
275.	*	.1	.4	.4	.6	.6	.2	.2	.0
280.	*	.0	.4	.4	.6	.5	.2	.2	.0
285.	*	.0	.4	.4	.6	.5	.3	.2	.0
290.	*	.0	.4	.4	.6	.5	.3	.1	.0
295.	*	.0	.3	.4	.6	.4	.3	.1	.0
300.	*	.0	.3	.4	.6	.4	.3	.1	.0
305.	*	.0	.3	.4	.6	.4	.3	.1	.0
310.	*	.0	.3	.5	.5	.4	.3	.3	.0
315.	*	.0	.3	.4	.5	.5	.3	.3	.0
320.	*	.0	.3	.4	.5	.4	.3	.3	.0
325.	*	.0	.3	.5	.5	.4	.2	.1	.0
330.	*	.0	.3	.5	.6	.4	.2	.1	.0
335.	*	.0	.3	.5	.6	.4	.1	.0	.0
340.	*	.0	.3	.5	.6	.3	.1	.0	.0
345.	*	.0	.3	.5	.6	.3	.1	.0	.1
350.	*	.0	.3	.6	.6	.4	.1	.1	.2
355.	*	.0	.3	.6	.5	.4	.2	.1	.2
360.	*	.0	.3	.6	.5	.3	.3	.4	.2
MAX	*	.5	.7	.8	.8	.7	.5	.5	.4
DEGR.	*	75	60	40	60	55	25	45	25

THE HIGHEST CONCENTRATION IS .90 PPM AT 240 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .90 PPM AT 90 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .90 PPM AT 90 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT) RUN: Site 3 NO BUILD AM
DATE: 03/22/2010 TIME: 10:01:38.62

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	*	323.0	617.0	-426.0	376.0	*	787.	252.	AG	2967.	.8	.0	68.0		
2. EB Wil T+R	*	323.0	616.0	531.0	681.0	*	218.	73.	AG	2763.	.8	.0	68.0		
3. EB Wil T+R	*	475.0	663.0	242.0	591.2	*	244.	253.	AG	11.	100.0	.0	48.0	.98	12.4
4. EB Wil LT	*	315.0	650.0	513.0	712.0	*	207.	73.	AG	204.	.8	.0	44.0		
5. EB Wil LT	*	444.0	690.0	-678.9	345.2	*	1175.	253.	AG	19.	100.0	.0	24.0	****	59.7
6. EB Wil DP	*	532.0	683.0	1471.0	989.0	*	988.	72.	AG	2497.	.8	.0	68.0		
7. WB Wil AP	*	756.0	830.0	1454.0	1051.0	*	732.	72.	AG	3144.	.8	.0	68.0		
8. WB Wil T+R	*	756.0	829.0	484.0	742.0	*	286.	252.	AG	3048.	.8	.0	68.0		
9. WB Wil T+R	*	540.0	760.0	2886.6	1509.1	*	2463.	72.	AG	18.	100.0	.0	48.0	1.38	125.1
10. WB Wil LT	*	767.0	790.0	513.0	706.0	*	268.	252.	AG	96.	.8	.0	32.0		
11. WB Wil LT	*	566.0	723.0	1295.5	963.7	*	768.	72.	AG	5.	100.0	.0	12.0	3.20	39.0
12. WB Wil DP	*	483.0	742.0	-451.0	441.0	*	981.	252.	AG	2816.	.8	.0	68.0		
13. NB Gln AP	*	542.0	703.0	861.0	-211.0	*	968.	161.	AG	311.	.9	.0	32.0		
14. NB Gln AP	*	564.0	640.0	1803.0	-2916.8	*	3766.	161.	AG	9.	100.0	.0	12.0	****	191.3
15. NB Gln DP	*	545.0	705.0	-160.0	1462.0	*	1034.	317.	AG	898.	.9	.0	32.0		
16. SB Gln AP	*	305.0	915.0	-182.0	1445.0	*	720.	317.	AG	540.	.9	.0	32.0		
17. SB Gln T+LT	*	305.0	915.0	479.0	736.0	*	250.	136.	AG	336.	.9	.0	44.0		
18. SB Gln T+LT	*	430.0	786.0	157.5	1066.2	*	391.	316.	AG	17.	100.0	.0	24.0	1.15	19.9
19. SB Gln R	*	300.0	890.0	443.0	732.0	*	213.	138.	AG	204.	.9	.0	32.0		
20. SB Gln R	*	400.0	780.0	326.9	861.3	*	109.	318.	AG	7.	100.0	.0	12.0	.40	5.6
21. SB Gln DP	*	478.0	734.0	548.0	638.0	*	119.	144.	AG	751.	.9	.0	32.0		
22. SB Gln DP	*	548.0	638.0	840.0	-220.0	*	906.	161.	AG	751.	.9	.0	32.0		

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JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT) RUN: Site 3 NO BUILD AM
DATE: 03/22/2010 TIME: 10:01:38.62

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	*	150	39	2.0	2763	992	4.10	1	3
5. EB Wil LT	*	150	130	2.0	204	84	4.10	1	3
9. WB Wil T+R	*	150	62	2.0	3048	990	4.10	1	3
11. WB Wil LT	*	150	62	2.0	96	54	4.10	1	3
14. NB Gln AP	*	150	116	2.0	311	39	4.10	1	3
18. SB Gln T+LT	*	150	116	2.0	336	731	4.10	1	3
20. SB Gln R	*	150	98	2.0	204	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. SE MID S	*	685.0	365.0	5.0	*
2. SE 164 S	*	638.0	508.0	5.0	*
3. SE 82 S	*	611.0	586.0	5.0	*
4. SE CNR	*	595.0	659.0	5.0	*
5. SE 82 E	*	664.0	689.0	5.0	*
6. SE 164 E	*	742.0	713.0	5.0	*
7. SE MID E	*	849.0	747.0	5.0	*
8. NE MID E	*	793.0	878.0	5.0	*
9. NE 164 E	*	674.0	839.0	5.0	*
10. NE 82 E	*	595.0	813.0	5.0	*
11. NE CNR	*	515.0	792.0	5.0	*
12. NE 82 N	*	452.0	847.0	5.0	*
13. NE 164 N	*	396.0	907.0	5.0	*
14. NE MID N	*	319.0	990.0	5.0	*
15. NW MID N	*	190.0	983.0	5.0	*
16. NW 164 N	*	267.0	900.0	5.0	*
17. NW 82 N	*	323.0	841.0	5.0	*
18. NW CNR	*	381.0	759.0	5.0	*
19. NW 82 W	*	299.0	719.0	5.0	*
20. NW 164 W	*	222.0	694.0	5.0	*
21. NW MID W	*	107.0	658.0	5.0	*
22. SW MID W	*	213.0	548.0	5.0	*
23. SW 164 W	*	367.0	595.0	5.0	*
24. SW 82 W	*	447.0	619.0	5.0	*
25. SW CNR	*	518.0	634.0	5.0	*
26. SW 82 S	*	550.0	565.0	5.0	*
27. SW 164 S	*	577.0	487.0	5.0	*
28. SW MID S	*	622.0	354.0	5.0	*

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT) RUN: Site 3 NO BUILD AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1

1

JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT) RUN: Site 3 NO BUILD AM

WIND ANGLE (DEGR)* | * CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.0	.1	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	85	70	70	0	0	0	0	0	0	105	70	70

1

JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT) RUN: Site 3 NO BUILD AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)* | * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.1	.1	.1	.0	.0	.0	.0
25.	*	.0	.1	.1	.1	.0	.0	.0	.0
30.	*	.0	.1	.1	.1	.0	.0	.0	.0
35.	*	.0	.1	.1	.1	.0	.0	.0	.0
40.	*	.0	.1	.1	.1	.1	.0	.0	.0
45.	*	.0	.1	.1	.1	.1	.0	.0	.0
50.	*	.0	.1	.1	.1	.1	.0	.0	.0
55.	*	.0	.1	.1	.1	.1	.0	.0	.0
60.	*	.0	.1	.1	.1	.1	.0	.0	.0
65.	*	.1	.1	.1	.2	.1	.0	.0	.0
70.	*	.1	.1	.1	.0	.1	.0	.0	.0
75.	*	.1	.1	.1	.0	.0	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT) RUN: Site 3 NO BUILD AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.1	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.1	.0	.0	.0	.0	.0
250.	*	.1	.1	.1	.0	.0	.0	.0	.0
255.	*	.1	.1	.1	.1	.0	.0	.0	.0
260.	*	.1	.1	.1	.2	.1	.0	.0	.0
265.	*	.0	.1	.1	.1	.1	.0	.0	.0
270.	*	.0	.1	.1	.1	.1	.0	.0	.0
275.	*	.0	.1	.1	.1	.1	.0	.0	.0
280.	*	.0	.1	.1	.1	.1	.0	.0	.0
285.	*	.0	.1	.1	.1	.1	.0	.0	.0
290.	*	.0	.1	.0	.1	.1	.0	.0	.0
295.	*	.0	.1	.0	.1	.1	.0	.0	.0
300.	*	.0	.1	.0	.1	.1	.0	.0	.0
305.	*	.0	.1	.1	.1	.1	.0	.0	.0
310.	*	.0	.1	.1	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.1	.1	.2	.1	.0	.0	.0
DEGR.	*	65	0	0	65	40	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT) RUN: Site 3 NO BUILD PM
DATE: 03/22/2010 TIME: 10:12:07.35

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	*	323.0	617.0	-426.0	376.0	*	787.	252.	AG	2690.	.8	.0	68.0		
2. EB Wil T+R	*	323.0	616.0	531.0	681.0	*	218.	73.	AG	2457.	.8	.0	68.0		
3. EB Wil T+R	*	475.0	663.0	-6884.3	-1605.3	*	7701.	253.	AG	16.	100.0	.0	48.0	****	391.2
4. EB Wil LT	*	315.0	650.0	513.0	712.0	*	207.	73.	AG	233.	.8	.0	44.0		
5. EB Wil LT	*	444.0	690.0	-822.3	301.1	*	1325.	253.	AG	19.	100.0	.0	24.0	****	67.3
6. EB Wil DP	*	532.0	683.0	1471.0	989.0	*	988.	72.	AG	2819.	.8	.0	68.0		
7. WB Wil AP	*	756.0	830.0	1454.0	1051.0	*	732.	72.	AG	2887.	.8	.0	68.0		
8. WB Wil T+R	*	756.0	829.0	484.0	742.0	*	286.	252.	AG	2754.	.8	.0	68.0		
9. WB Wil T+R	*	540.0	760.0	3281.3	1635.2	*	2878.	72.	AG	23.	100.0	.0	48.0	1.56	146.2
10. WB Wil LT	*	767.0	790.0	513.0	706.0	*	268.	252.	AG	133.	.8	.0	32.0		
11. WB Wil LT	*	566.0	723.0	1696.4	1096.0	*	1190.	72.	AG	6.	100.0	.0	12.0	4.43	60.5
12. WB Wil DP	*	483.0	742.0	-451.0	441.0	*	981.	252.	AG	3052.	.8	.0	68.0		
13. NB Gln AP	*	542.0	703.0	861.0	-211.0	*	968.	161.	AG	899.	.9	.0	32.0		
14. NB Gln AP	*	564.0	640.0	3512.4	-7823.7	*	8963.	161.	AG	7.	100.0	.0	12.0	****	455.3
15. NB Gln DP	*	545.0	705.0	-160.0	1462.0	*	1034.	317.	AG	960.	.9	.0	32.0		
16. SB Gln AP	*	305.0	915.0	-182.0	1445.0	*	720.	317.	AG	1017.	.9	.0	32.0		
17. SB Gln T+LT	*	305.0	915.0	479.0	736.0	*	250.	136.	AG	713.	.9	.0	44.0		
18. SB Gln T+LT	*	430.0	786.0	-430.9	1671.5	*	1235.	316.	AG	15.	100.0	.0	24.0	1.36	62.7
19. SB Gln R	*	300.0	890.0	443.0	732.0	*	213.	138.	AG	304.	.9	.0	32.0		
20. SB Gln R	*	400.0	780.0	311.0	878.8	*	133.	318.	AG	6.	100.0	.0	12.0	.43	6.8
21. SB Gln DP	*	478.0	734.0	548.0	638.0	*	119.	144.	AG	662.	.9	.0	32.0		
22. SB Gln DP	*	548.0	638.0	840.0	-220.0	*	906.	161.	AG	662.	.9	.0	32.0		

1 PAGE 2

JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT) RUN: Site 3 NO BUILD PM
DATE: 03/22/2010 TIME: 10:12:07.35

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	*	150	56	2.0	2457	7	4.10	1	3
5. EB Wil LT	*	150	129	2.0	233	84	4.10	1	3
9. WB Wil T+R	*	150	79	2.0	2754	991	4.10	1	3
11. WB Wil LT	*	150	79	2.0	133	68	4.10	1	3
14. NB Gln AP	*	150	99	2.0	899	276	4.10	1	3
18. SB Gln T+LT	*	150	99	2.0	713	836	4.10	1	3
20. SB Gln R	*	150	80	2.0	304	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. SE MID S	*	685.0	365.0	5.0	*
2. SE 164 S	*	638.0	508.0	5.0	*
3. SE 82 S	*	611.0	586.0	5.0	*
4. SE CNR	*	595.0	659.0	5.0	*
5. SE 82 E	*	664.0	689.0	5.0	*
6. SE 164 E	*	742.0	713.0	5.0	*
7. SE MID E	*	849.0	747.0	5.0	*
8. NE MID E	*	793.0	878.0	5.0	*
9. NE 164 E	*	674.0	839.0	5.0	*
10. NE 82 E	*	595.0	813.0	5.0	*
11. NE CNR	*	515.0	792.0	5.0	*
12. NE 82 N	*	452.0	847.0	5.0	*
13. NE 164 N	*	396.0	907.0	5.0	*
14. NE MID N	*	319.0	990.0	5.0	*
15. NW MID N	*	190.0	983.0	5.0	*
16. NW 164 N	*	267.0	900.0	5.0	*
17. NW 82 N	*	323.0	841.0	5.0	*
18. NW CNR	*	381.0	759.0	5.0	*
19. NW 82 W	*	299.0	719.0	5.0	*
20. NW 164 W	*	222.0	694.0	5.0	*
21. NW MID W	*	107.0	658.0	5.0	*
22. SW MID W	*	213.0	548.0	5.0	*
23. SW 164 W	*	367.0	595.0	5.0	*
24. SW 82 W	*	447.0	619.0	5.0	*
25. SW CNR	*	518.0	634.0	5.0	*
26. SW 82 S	*	550.0	565.0	5.0	*
27. SW 164 S	*	577.0	487.0	5.0	*
28. SW MID S	*	622.0	354.0	5.0	*

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT) RUN: Site 3 NO BUILD PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	* CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT) RUN: Site 3 NO BUILD PM

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.1	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	65	90	70	75	0	0	0	0	0	0	100	70	65

1

JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT) RUN: Site 3 NO BUILD PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.2	.2	.1	.0	.0	.0	.0
25.	*	.0	.2	.2	.1	.0	.0	.0	.0
30.	*	.0	.2	.2	.1	.0	.0	.0	.0
35.	*	.0	.2	.2	.1	.1	.0	.0	.0
40.	*	.0	.2	.2	.1	.1	.0	.0	.0
45.	*	.0	.2	.2	.1	.1	.0	.0	.0
50.	*	.0	.2	.2	.1	.1	.0	.0	.0
55.	*	.0	.2	.1	.1	.1	.0	.0	.0
60.	*	.0	.2	.1	.2	.1	.0	.0	.0
65.	*	.1	.2	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.1	.1	.0	.0	.0
75.	*	.1	.0	.1	.0	.1	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT) RUN: Site 3 NO BUILD PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.0	.0	.0	.0	.0
250.	*	.1	.2	.2	.1	.0	.0	.0	.0
255.	*	.1	.2	.2	.1	.1	.0	.0	.0
260.	*	.1	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.2	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.0	.0	.0
285.	*	.0	.2	.2	.2	.1	.0	.0	.0
290.	*	.0	.2	.1	.2	.1	.0	.0	.0
295.	*	.0	.2	.1	.2	.1	.0	.0	.0
300.	*	.0	.2	.1	.2	.1	.0	.0	.0
305.	*	.0	.2	.1	.2	.1	.0	.0	.0
310.	*	.0	.1	.0	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.0	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX DEGR.	*	.1 65	.2 20	.2 20	.2 60	.2 260	.0 0	.0 0	.0 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 65 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT) RUN: Site 3 BUILD 1 AM
DATE: 03/22/2010 TIME: 10:42:44.83

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2885.	.8	.0	68.0		
2. EB Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2690.	.8	.0	68.0		
3. EB Wil T+R	475.0	663.0	274.5	601.2	210.	253.	AG	11.	100.0	.0	48.0	.95	10.7
4. EB Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	195.	.8	.0	44.0		
5. EB Wil LT	444.0	690.0	-620.2	363.2	1113.	253.	AG	19.	100.0	.0	24.0	****	56.6
6. EB Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2465.	.8	.0	68.0		
7. WB Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	3121.	.8	.0	68.0		
8. WB Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	3035.	.8	.0	68.0		
9. WB Wil T+R	540.0	760.0	3199.2	1609.0	2791.	72.	AG	18.	100.0	.0	48.0	1.47	141.8
10. WB Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	86.	.8	.0	32.0		
11. WB Wil LT	566.0	723.0	1190.3	929.0	657.	72.	AG	5.	100.0	.0	12.0	2.87	33.4
12. WB Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2899.	.8	.0	68.0		
13. NB Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	388.	.9	.0	32.0		
14. NB Gln AP	564.0	640.0	2032.8	-3576.4	4465.	161.	AG	9.	100.0	.0	12.0	****	226.8
15. NB Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	929.	.9	.0	32.0		
16. SB Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	593.	.9	.0	32.0		
17. SB Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	330.	.9	.0	44.0		
18. SB Gln T+LT	430.0	786.0	103.0	1122.4	469.	316.	AG	17.	100.0	.0	24.0	1.22	23.8
19. SB Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	263.	.9	.0	32.0		
20. SB Gln R	400.0	780.0	305.7	884.8	141.	318.	AG	7.	100.0	.0	12.0	.51	7.2
21. SB Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	694.	.9	.0	32.0		
22. SB Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	694.	.9	.0	32.0		

1 PAGE 2

JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT) RUN: Site 3 BUILD 1 AM
DATE: 03/22/2010 TIME: 10:42:44.83

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	150	39	2.0	2690	994	4.10	1	3
5. EB Wil LT	150	130	2.0	195	84	4.10	1	3
9. WB Wil T+R	150	62	2.0	3035	924	4.10	1	3
11. WB Wil LT	150	62	2.0	86	54	4.10	1	3
14. NB Gln AP	150	116	2.0	388	69	4.10	1	3
18. SB Gln T+LT	150	116	2.0	330	678	4.10	1	3
20. SB Gln R	150	98	2.0	263	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT) RUN: Site 3 BUILD 1 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	* CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1

1

JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT) RUN: Site 3 BUILD 1 AM

WIND ANGLE (DEGR)* | * CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	85	70	70	0	0	0	0	0	0	105	70	70

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JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT) RUN: Site 3 BUILD 1 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)* | * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.1	.1	.1	.0	.0	.0	.0
25.	*	.0	.1	.1	.1	.0	.0	.0	.0
30.	*	.0	.1	.1	.1	.0	.0	.0	.0
35.	*	.0	.1	.1	.1	.0	.0	.0	.0
40.	*	.0	.1	.1	.1	.1	.0	.0	.0
45.	*	.0	.1	.1	.1	.1	.0	.0	.0
50.	*	.0	.1	.1	.1	.1	.0	.0	.0
55.	*	.0	.1	.1	.1	.1	.0	.0	.0
60.	*	.0	.1	.1	.1	.1	.0	.0	.0
65.	*	.1	.1	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.0	.1	.0	.0	.0
75.	*	.1	.1	.1	.0	.0	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.1	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.1	.0	.0	.0	.0	.0
250.	*	.1	.1	.1	.0	.0	.0	.0	.0
255.	*	.1	.1	.1	.1	.0	.0	.0	.0
260.	*	.1	.1	.1	.1	.1	.0	.0	.0
265.	*	.0	.1	.1	.1	.1	.0	.0	.0
270.	*	.0	.1	.1	.1	.1	.0	.0	.0
275.	*	.0	.1	.1	.1	.1	.0	.0	.0
280.	*	.0	.1	.1	.1	.1	.0	.0	.0
285.	*	.0	.1	.1	.1	.1	.0	.0	.0
290.	*	.0	.1	.0	.1	.1	.0	.0	.0
295.	*	.0	.1	.0	.1	.1	.0	.0	.0
300.	*	.0	.1	.0	.1	.1	.0	.0	.0
305.	*	.0	.1	.1	.1	.1	.0	.0	.0
310.	*	.0	.1	.1	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.1	.1	.1	.1	.0	.0	.0
DEGR.	*	65	0	0	0	40	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT) RUN: Site 3 BUILD A1 PM
DATE: 03/22/2010 TIME: 10:51:05.37

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2704.	.8	.0	68.0		
2. EB Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2475.	.8	.0	68.0		
3. EB Wil T+R	475.0	663.0	-6932.5	-1620.1	7751.	253.	AG	16.	100.0	.0	48.0	****	393.8
4. EB Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	229.	.8	.0	44.0		
5. EB Wil LT	444.0	690.0	-819.9	301.9	1322.	253.	AG	19.	100.0	.0	24.0	****	67.2
6. EB Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2819.	.8	.0	68.0		
7. WB Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	2895.	.8	.0	68.0		
8. WB Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	2762.	.8	.0	68.0		
9. WB Wil T+R	540.0	760.0	3240.5	1622.1	2835.	72.	AG	23.	100.0	.0	48.0	1.54	144.0
10. WB Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	133.	.8	.0	32.0		
11. WB Wil LT	566.0	723.0	1695.7	1095.7	1190.	72.	AG	6.	100.0	.0	12.0	4.43	60.4
12. WB Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	3001.	.8	.0	68.0		
13. NB Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	870.	.9	.0	32.0		
14. NB Gln AP	564.0	640.0	3404.2	-7513.1	8634.	161.	AG	7.	100.0	.0	12.0	****	438.6
15. NB Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	988.	.9	.0	32.0		
16. SB Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	1004.	.9	.0	32.0		
17. SB Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	699.	.9	.0	44.0		
18. SB Gln T+LT	430.0	786.0	-420.8	1661.1	1220.	316.	AG	15.	100.0	.0	24.0	1.37	62.0
19. SB Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	305.	.9	.0	32.0		
20. SB Gln R	400.0	780.0	309.6	880.4	135.	318.	AG	6.	100.0	.0	12.0	.44	6.9
21. SB Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	665.	.9	.0	32.0		
22. SB Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	665.	.9	.0	32.0		

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JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT) RUN: Site 3 BUILD A1 PM
DATE: 03/22/2010 TIME: 10:51:05.37

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	150	56	2.0	2475	7	4.10	1	3
5. EB Wil LT	150	130	2.0	229	84	4.10	1	3
9. WB Wil T+R	150	78	2.0	2762	990	4.10	1	3
11. WB Wil LT	150	78	2.0	133	68	4.10	1	3
14. NB Gln AP	150	99	2.0	870	280	4.10	1	3
18. SB Gln T+LT	150	99	2.0	699	816	4.10	1	3
20. SB Gln R	150	81	2.0	305	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

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JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT) RUN: Site 3 BUILD A1 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT) RUN: Site 3 BUILD A1 PM

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.1	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	90	70	75	0	0	0	0	0	0	100	70	65

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JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT) RUN: Site 3 BUILD A1 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.2	.2	.1	.0	.0	.0	.0
25.	*	.0	.2	.2	.1	.0	.0	.0	.0
30.	*	.0	.2	.2	.1	.0	.0	.0	.0
35.	*	.0	.2	.2	.1	.1	.0	.0	.0
40.	*	.0	.2	.2	.1	.1	.0	.0	.0
45.	*	.0	.2	.2	.1	.1	.0	.0	.0
50.	*	.0	.2	.2	.1	.1	.0	.0	.0
55.	*	.0	.2	.1	.1	.1	.0	.0	.0
60.	*	.0	.2	.1	.2	.1	.0	.0	.0
65.	*	.1	.2	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.1	.1	.0	.0	.0
75.	*	.1	.0	.1	.0	.1	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT) RUN: Site 3 BUILD A1 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.0	.0	.0	.0	.0
250.	*	.1	.2	.2	.1	.0	.0	.0	.0
255.	*	.1	.2	.2	.1	.1	.0	.0	.0
260.	*	.1	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.2	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.0	.0	.0
285.	*	.0	.2	.2	.2	.1	.0	.0	.0
290.	*	.0	.2	.1	.2	.1	.0	.0	.0
295.	*	.0	.2	.1	.2	.1	.0	.0	.0
300.	*	.0	.2	.1	.2	.1	.0	.0	.0
305.	*	.0	.2	.1	.2	.1	.0	.0	.0
310.	*	.0	.1	.0	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.0	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.2	.2	.2	.2	.0	.0	.0
DEGR.	*	65	20	20	60	260	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT) RUN: Site 3 BUILD 2 AM
DATE: 03/22/2010 TIME: 11:01:39.59

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	*	323.0	617.0	-426.0	376.0	*	787.	252.	AG	2910.	.8	.0	68.0		
2. EB Wil T+R	*	323.0	616.0	531.0	681.0	*	218.	73.	AG	2733.	.8	.0	68.0		
3. EB Wil T+R	*	475.0	663.0	255.9	595.5	*	229.	253.	AG	11.	100.0	.0	48.0	.96	11.6
4. EB Wil LT	*	315.0	650.0	513.0	712.0	*	207.	73.	AG	177.	.8	.0	44.0		
5. EB Wil LT	*	444.0	690.0	-514.9	395.5	*	1003.	253.	AG	19.	100.0	.0	24.0	****	51.0
6. EB Wil DP	*	532.0	683.0	1471.0	989.0	*	988.	72.	AG	2513.	.8	.0	68.0		
7. WB Wil AP	*	756.0	830.0	1454.0	1051.0	*	732.	72.	AG	3134.	.8	.0	68.0		
8. WB Wil T+R	*	756.0	829.0	484.0	742.0	*	286.	252.	AG	3039.	.8	.0	68.0		
9. WB Wil T+R	*	540.0	760.0	2725.4	1457.7	*	2294.	72.	AG	18.	100.0	.0	48.0	1.34	116.5
10. WB Wil LT	*	767.0	790.0	513.0	706.0	*	268.	252.	AG	95.	.8	.0	32.0		
11. WB Wil LT	*	566.0	723.0	1284.0	959.9	*	756.	72.	AG	4.	100.0	.0	12.0	3.17	38.4
12. WB Wil DP	*	483.0	742.0	-451.0	441.0	*	981.	252.	AG	2846.	.8	.0	68.0		
13. NB Gln AP	*	542.0	703.0	861.0	-211.0	*	968.	161.	AG	382.	.9	.0	32.0		
14. NB Gln AP	*	564.0	640.0	1991.2	-3456.8	*	4338.	161.	AG	9.	100.0	.0	12.0	****	220.4
15. NB Gln DP	*	545.0	705.0	-160.0	1462.0	*	1034.	317.	AG	951.	.9	.0	32.0		
16. SB Gln AP	*	305.0	915.0	-182.0	1445.0	*	720.	317.	AG	604.	.9	.0	32.0		
17. SB Gln T+LT	*	305.0	915.0	479.0	736.0	*	250.	136.	AG	352.	.9	.0	44.0		
18. SB Gln T+LT	*	430.0	786.0	26.5	1201.1	*	579.	316.	AG	17.	100.0	.0	24.0	1.29	29.4
19. SB Gln R	*	300.0	890.0	443.0	732.0	*	213.	138.	AG	252.	.9	.0	32.0		
20. SB Gln R	*	400.0	780.0	308.7	881.4	*	136.	318.	AG	7.	100.0	.0	12.0	.50	6.9
21. SB Gln DP	*	478.0	734.0	548.0	638.0	*	119.	144.	AG	720.	.9	.0	32.0		
22. SB Gln DP	*	548.0	638.0	840.0	-220.0	*	906.	161.	AG	720.	.9	.0	32.0		

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JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT) RUN: Site 3 BUILD 2 AM
DATE: 03/22/2010 TIME: 11:01:39.59

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	*	150	39	2.0	2733	993	4.10	1	3
5. EB Wil LT	*	150	131	2.0	177	84	4.10	1	3
9. WB Wil T+R	*	150	60	2.0	3039	989	4.10	1	3
11. WB Wil LT	*	150	60	2.0	95	54	4.10	1	3
14. NB Gln AP	*	150	116	2.0	382	75	4.10	1	3
18. SB Gln T+LT	*	150	116	2.0	352	681	4.10	1	3
20. SB Gln R	*	150	99	2.0	252	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. SE MID S	*	685.0	365.0	5.0	*
2. SE 164 S	*	638.0	508.0	5.0	*
3. SE 82 S	*	611.0	586.0	5.0	*
4. SE CNR	*	595.0	659.0	5.0	*
5. SE 82 E	*	664.0	689.0	5.0	*
6. SE 164 E	*	742.0	713.0	5.0	*
7. SE MID E	*	849.0	747.0	5.0	*
8. NE MID E	*	793.0	878.0	5.0	*
9. NE 164 E	*	674.0	839.0	5.0	*
10. NE 82 E	*	595.0	813.0	5.0	*
11. NE CNR	*	515.0	792.0	5.0	*
12. NE 82 N	*	452.0	847.0	5.0	*
13. NE 164 N	*	396.0	907.0	5.0	*
14. NE MID N	*	319.0	990.0	5.0	*
15. NW MID N	*	190.0	983.0	5.0	*
16. NW 164 N	*	267.0	900.0	5.0	*
17. NW 82 N	*	323.0	841.0	5.0	*
18. NW CNR	*	381.0	759.0	5.0	*
19. NW 82 W	*	299.0	719.0	5.0	*
20. NW 164 W	*	222.0	694.0	5.0	*
21. NW MID W	*	107.0	658.0	5.0	*
22. SW MID W	*	213.0	548.0	5.0	*
23. SW 164 W	*	367.0	595.0	5.0	*
24. SW 82 W	*	447.0	619.0	5.0	*
25. SW CNR	*	518.0	634.0	5.0	*
26. SW 82 S	*	550.0	565.0	5.0	*
27. SW 164 S	*	577.0	487.0	5.0	*
28. SW MID S	*	622.0	354.0	5.0	*

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT) RUN: Site 3 BUILD 2 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT) RUN: Site 3 BUILD 2 AM

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	85	70	75	0	0	0	0	0	0	105	70	70

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JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT) RUN: Site 3 BUILD 2 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.1	.1	.1	.0	.0	.0	.0
25.	*	.0	.1	.1	.1	.0	.0	.0	.0
30.	*	.0	.1	.1	.1	.0	.0	.0	.0
35.	*	.0	.1	.1	.1	.0	.0	.0	.0
40.	*	.0	.1	.1	.1	.1	.0	.0	.0
45.	*	.0	.1	.1	.1	.1	.0	.0	.0
50.	*	.0	.1	.1	.1	.1	.0	.0	.0
55.	*	.0	.1	.1	.1	.1	.0	.0	.0
60.	*	.0	.1	.1	.1	.1	.0	.0	.0
65.	*	.1	.1	.1	.2	.1	.0	.0	.0
70.	*	.1	.1	.1	.0	.1	.0	.0	.0
75.	*	.1	.1	.1	.0	.0	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT) RUN: Site 3 BUILD 2 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.1	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.1	.0	.0	.0	.0	.0
250.	*	.1	.1	.1	.0	.0	.0	.0	.0
255.	*	.1	.1	.1	.1	.0	.0	.0	.0
260.	*	.1	.1	.1	.2	.1	.0	.0	.0
265.	*	.0	.1	.1	.1	.1	.0	.0	.0
270.	*	.0	.1	.1	.1	.1	.0	.0	.0
275.	*	.0	.1	.1	.1	.1	.0	.0	.0
280.	*	.0	.1	.1	.1	.1	.0	.0	.0
285.	*	.0	.1	.1	.1	.1	.0	.0	.0
290.	*	.0	.1	.0	.1	.1	.0	.0	.0
295.	*	.0	.1	.0	.1	.1	.0	.0	.0
300.	*	.0	.1	.0	.1	.1	.0	.0	.0
305.	*	.0	.1	.1	.1	.1	.0	.0	.0
310.	*	.0	.1	.1	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.1	.1	.2	.1	.0	.0	.0
DEGR.	*	65	0	0	65	40	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT) RUN: Site 3 BUILD A2 PM
DATE: 03/22/2010 TIME: 11:09:09.87

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB	Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2692.	.8	.0	68.0		
2. EB	Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2479.	.8	.0	68.0		
3. EB	Wil T+R	475.0	663.0	-7179.1	-1696.1	8009.	253.	AG	16.	100.0	.0	48.0	****	406.9
4. EB	Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	229.	.8	.0	44.0		
5. EB	Wil LT	444.0	690.0	-819.9	301.9	1322.	253.	AG	19.	100.0	.0	24.0	****	67.2
6. EB	Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2820.	.8	.0	68.0		
7. WB	Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	2921.	.8	.0	68.0		
8. WB	Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	2789.	.8	.0	68.0		
9. WB	Wil T+R	540.0	760.0	3249.6	1625.0	2844.	72.	AG	23.	100.0	.0	48.0	1.54	144.5
10. WB	Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	132.	.8	.0	32.0		
11. WB	Wil LT	566.0	723.0	1684.4	1092.0	1178.	72.	AG	6.	100.0	.0	12.0	4.40	59.8
12. WB	Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	3052.	.8	.0	68.0		
13. NB	Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	888.	.9	.0	32.0		
14. NB	Gln AP	564.0	640.0	3485.4	-7746.2	8881.	161.	AG	7.	100.0	.0	12.0	****	451.1
15. NB	Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	964.	.9	.0	32.0		
16. SB	Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	1003.	.9	.0	32.0		
17. SB	Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	706.	.9	.0	44.0		
18. SB	Gln T+LT	430.0	786.0	-408.5	1648.5	1203.	316.	AG	15.	100.0	.0	24.0	1.35	61.1
19. SB	Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	303.	.9	.0	32.0		
20. SB	Gln R	400.0	780.0	308.0	882.2	138.	318.	AG	6.	100.0	.0	12.0	.45	7.0
21. SB	Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	674.	.9	.0	32.0		
22. SB	Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	674.	.9	.0	32.0		

1 PAGE 2

JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT) RUN: Site 3 BUILD A2 PM
DATE: 03/22/2010 TIME: 11:09:09.87

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB	Wil T+R	150	56	2.0	2479	6	4.10	1	3
5. EB	Wil LT	150	130	2.0	229	84	4.10	1	3
9. WB	Wil T+R	150	77	2.0	2789	989	4.10	1	3
11. WB	Wil LT	150	77	2.0	132	66	4.10	1	3
14. NB	Gln AP	150	99	2.0	888	268	4.10	1	3
18. SB	Gln T+LT	150	99	2.0	706	833	4.10	1	3
20. SB	Gln R	150	83	2.0	303	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT) RUN: Site 3 BUILD A2 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT) RUN: Site 3 BUILD A2 PM

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.1	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	90	70	75	0	0	0	0	0	0	100	70	65

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JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT) RUN: Site 3 BUILD A2 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.2	.2	.1	.0	.0	.0	.0
25.	*	.0	.2	.2	.1	.0	.0	.0	.0
30.	*	.0	.2	.2	.1	.0	.0	.0	.0
35.	*	.0	.2	.2	.1	.1	.0	.0	.0
40.	*	.0	.2	.2	.1	.1	.0	.0	.0
45.	*	.0	.2	.2	.1	.1	.0	.0	.0
50.	*	.0	.2	.2	.1	.1	.0	.0	.0
55.	*	.0	.2	.1	.1	.1	.0	.0	.0
60.	*	.0	.2	.1	.2	.1	.0	.0	.0
65.	*	.1	.2	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.1	.1	.0	.0	.0
75.	*	.1	.0	.1	.0	.1	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT) RUN: Site 3 BUILD A2 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.0	.0	.0	.0	.0
250.	*	.1	.2	.2	.1	.0	.0	.0	.0
255.	*	.1	.2	.2	.1	.1	.0	.0	.0
260.	*	.1	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.2	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.0	.0	.0
285.	*	.0	.2	.2	.2	.1	.0	.0	.0
290.	*	.0	.2	.1	.2	.1	.0	.0	.0
295.	*	.0	.2	.1	.2	.1	.0	.0	.0
300.	*	.0	.2	.1	.2	.1	.0	.0	.0
305.	*	.0	.2	.1	.2	.1	.0	.0	.0
310.	*	.0	.1	.0	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.0	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.2	.2	.2	.2	.0	.0	.0
DEGR.	*	65	20	20	60	260	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT) RUN: Site 3 BUILD 3 AM
DATE: 03/22/2010 TIME: 11:19:24.60

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2883.	.8	.0	68.0		
2. EB Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2678.	.8	.0	68.0		
3. EB Wil T+R	475.0	663.0	278.8	602.5	205.	253.	AG	11.	100.0	.0	48.0	.94	10.4
4. EB Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	205.	.8	.0	44.0		
5. EB Wil LT	444.0	690.0	-659.3	351.2	1154.	253.	AG	19.	100.0	.0	24.0	****	58.6
6. EB Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2652.	.8	.0	68.0		
7. WB Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	3101.	.8	.0	68.0		
8. WB Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	3005.	.8	.0	68.0		
9. WB Wil T+R	540.0	760.0	2777.7	1474.4	2349.	72.	AG	18.	100.0	.0	48.0	1.36	119.3
10. WB Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	96.	.8	.0	32.0		
11. WB Wil LT	566.0	723.0	1295.5	963.7	768.	72.	AG	5.	100.0	.0	12.0	3.20	39.0
12. WB Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2818.	.8	.0	68.0		
13. NB Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	316.	.9	.0	32.0		
14. NB Gln AP	564.0	640.0	1794.0	-2890.9	3739.	161.	AG	9.	100.0	.0	12.0	****	189.9
15. NB Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	885.	.9	.0	32.0		
16. SB Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	570.	.9	.0	32.0		
17. SB Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	340.	.9	.0	44.0		
18. SB Gln T+LT	430.0	786.0	135.4	1089.1	423.	316.	AG	17.	100.0	.0	24.0	1.17	21.5
19. SB Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	230.	.9	.0	32.0		
20. SB Gln R	400.0	780.0	318.4	870.7	122.	318.	AG	7.	100.0	.0	12.0	.44	6.2
21. SB Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	698.	.9	.0	32.0		
22. SB Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	698.	.9	.0	32.0		

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JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT) RUN: Site 3 BUILD 3 AM
DATE: 03/22/2010 TIME: 11:19:24.60

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	150	39	2.0	2678	994	4.10	1	3
5. EB Wil LT	150	129	2.0	205	84	4.10	1	3
9. WB Wil T+R	150	62	2.0	3005	990	4.10	1	3
11. WB Wil LT	150	62	2.0	96	54	4.10	1	3
14. NB Gln AP	150	116	2.0	316	46	4.10	1	3
18. SB Gln T+LT	150	116	2.0	340	727	4.10	1	3
20. SB Gln R	150	97	2.0	230	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT) RUN: Site 3 BUILD 3 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1

1

JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT) RUN: Site 3 BUILD 3 AM

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	85	70	70	0	0	0	0	0	0	105	70	70

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JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT) RUN: Site 3 BUILD 3 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.1	.1	.1	.0	.0	.0	.0
25.	*	.0	.1	.1	.1	.0	.0	.0	.0
30.	*	.0	.1	.1	.1	.0	.0	.0	.0
35.	*	.0	.1	.1	.1	.0	.0	.0	.0
40.	*	.0	.1	.1	.1	.1	.0	.0	.0
45.	*	.0	.1	.1	.1	.1	.0	.0	.0
50.	*	.0	.1	.1	.1	.1	.0	.0	.0
55.	*	.0	.1	.1	.1	.1	.0	.0	.0
60.	*	.0	.1	.1	.2	.1	.0	.0	.0
65.	*	.1	.1	.1	.2	.1	.0	.0	.0
70.	*	.1	.1	.1	.1	.1	.0	.0	.0
75.	*	.1	.1	.1	.0	.1	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT) RUN: Site 3 BUILD 3 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.1	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.1	.0	.0	.0	.0	.0
250.	*	.1	.1	.1	.0	.0	.0	.0	.0
255.	*	.1	.1	.1	.1	.0	.0	.0	.0
260.	*	.1	.1	.1	.1	.1	.0	.0	.0
265.	*	.0	.1	.1	.1	.1	.0	.0	.0
270.	*	.0	.1	.1	.1	.1	.0	.0	.0
275.	*	.0	.1	.1	.1	.1	.0	.0	.0
280.	*	.0	.1	.1	.1	.1	.0	.0	.0
285.	*	.0	.1	.1	.1	.1	.0	.0	.0
290.	*	.0	.1	.0	.1	.1	.0	.0	.0
295.	*	.0	.1	.0	.1	.1	.0	.0	.0
300.	*	.0	.1	.0	.1	.1	.0	.0	.0
305.	*	.0	.1	.1	.1	.1	.0	.0	.0
310.	*	.0	.1	.1	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.1	.1	.2	.1	.0	.0	.0
DEGR.	*	65	0	0	60	40	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT) RUN: Site 3 BUILD A3 PM
DATE: 03/22/2010 TIME: 12:13:22.02

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB	Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2689.	.8	.0	68.0		
2. EB	Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2449.	.8	.0	68.0		
3. EB	Wil T+R	475.0	663.0	-6860.2	-1597.9	7676.	253.	AG	16.	100.0	.0	48.0	****	389.9
4. EB	Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	240.	.8	.0	44.0		
5. EB	Wil LT	444.0	690.0	-868.9	286.8	1373.	253.	AG	19.	100.0	.0	24.0	****	69.8
6. EB	Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2786.	.8	.0	68.0		
7. WB	Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	2876.	.8	.0	68.0		
8. WB	Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	2744.	.8	.0	68.0		
9. WB	Wil T+R	540.0	760.0	3261.3	1628.8	2857.	72.	AG	23.	100.0	.0	48.0	1.55	145.1
10. WB	Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	132.	.8	.0	32.0		
11. WB	Wil LT	566.0	723.0	1685.8	1092.5	1179.	72.	AG	6.	100.0	.0	12.0	4.40	59.9
12. WB	Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2979.	.8	.0	68.0		
13. NB	Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	855.	.9	.0	32.0		
14. NB	Gln AP	564.0	640.0	3371.0	-7417.9	8533.	161.	AG	7.	100.0	.0	12.0	****	433.5
15. NB	Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	973.	.9	.0	32.0		
16. SB	Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	998.	.9	.0	32.0		
17. SB	Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	708.	.9	.0	44.0		
18. SB	Gln T+LT	430.0	786.0	-472.1	1713.8	1294.	316.	AG	15.	100.0	.0	24.0	1.40	65.7
19. SB	Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	290.	.9	.0	32.0		
20. SB	Gln R	400.0	780.0	315.1	874.3	127.	318.	AG	6.	100.0	.0	12.0	.41	6.4
21. SB	Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	680.	.9	.0	32.0		
22. SB	Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	680.	.9	.0	32.0		

1 PAGE 2

JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT) RUN: Site 3 BUILD A3 PM
DATE: 03/22/2010 TIME: 12:13:22.02

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB	Wil T+R	150	56	2.0	2449	7	4.10	1	3
5. EB	Wil LT	150	129	2.0	240	84	4.10	1	3
9. WB	Wil T+R	150	79	2.0	2744	991	4.10	1	3
11. WB	Wil LT	150	79	2.0	132	68	4.10	1	3
14. NB	Gln AP	150	99	2.0	855	262	4.10	1	3
18. SB	Gln T+LT	150	99	2.0	708	808	4.10	1	3
20. SB	Gln R	150	80	2.0	290	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT) RUN: Site 3 BUILD A3 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT) RUN: Site 3 BUILD A3 PM

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.1	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	65	90	70	75	0	0	0	0	0	0	105	70	65

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JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT) RUN: Site 3 BUILD A3 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.2	.2	.1	.0	.0	.0	.0
25.	*	.0	.2	.2	.1	.0	.0	.0	.0
30.	*	.0	.2	.2	.1	.0	.0	.0	.0
35.	*	.0	.2	.2	.1	.1	.0	.0	.0
40.	*	.0	.2	.2	.1	.1	.0	.0	.0
45.	*	.0	.2	.2	.1	.1	.0	.0	.0
50.	*	.0	.2	.2	.1	.1	.0	.0	.0
55.	*	.0	.2	.1	.1	.1	.0	.0	.0
60.	*	.0	.2	.1	.2	.1	.0	.0	.0
65.	*	.1	.2	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.1	.1	.0	.0	.0
75.	*	.1	.0	.1	.0	.1	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT) RUN: Site 3 BUILD A3 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.0	.0	.0	.0	.0
250.	*	.1	.2	.2	.1	.0	.0	.0	.0
255.	*	.1	.2	.2	.1	.1	.0	.0	.0
260.	*	.1	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.2	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.0	.0	.0
285.	*	.0	.2	.2	.2	.1	.0	.0	.0
290.	*	.0	.2	.1	.2	.1	.0	.0	.0
295.	*	.0	.2	.1	.2	.1	.0	.0	.0
300.	*	.0	.2	.1	.2	.1	.0	.0	.0
305.	*	.0	.2	.1	.2	.1	.0	.0	.0
310.	*	.0	.1	.0	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.0	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.2	.2	.2	.2	.0	.0	.0
DEGR.	*	65	20	20	60	260	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 65 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT) RUN: Site 3 BUILD 4 AM
DATE: 03/22/2010 TIME: 11:38:57.92

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2883.	.8	.0	68.0		
2. EB Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2701.	.8	.0	68.0		
3. EB Wil T+R	475.0	663.0	270.0	599.8	214.	253.	AG	11.	100.0	.0	48.0	.95	10.9
4. EB Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	182.	.8	.0	44.0		
5. EB Wil LT	444.0	690.0	-550.2	384.7	1040.	253.	AG	19.	100.0	.0	24.0	****	52.8
6. EB Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2517.	.8	.0	68.0		
7. WB Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	3126.	.8	.0	68.0		
8. WB Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	3030.	.8	.0	68.0		
9. WB Wil T+R	540.0	760.0	2705.6	1451.4	2273.	72.	AG	18.	100.0	.0	48.0	1.34	115.5
10. WB Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	96.	.8	.0	32.0		
11. WB Wil LT	566.0	723.0	1294.5	963.4	767.	72.	AG	4.	100.0	.0	12.0	3.20	39.0
12. WB Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2821.	.8	.0	68.0		
13. NB Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	371.	.9	.0	32.0		
14. NB Gln AP	564.0	640.0	1976.7	-3415.2	4294.	161.	AG	9.	100.0	.0	12.0	****	218.1
15. NB Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	928.	.9	.0	32.0		
16. SB Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	583.	.9	.0	32.0		
17. SB Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	363.	.9	.0	44.0		
18. SB Gln T+LT	430.0	786.0	-4.5	1232.9	623.	316.	AG	17.	100.0	.0	24.0	1.32	31.7
19. SB Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	220.	.9	.0	32.0		
20. SB Gln R	400.0	780.0	320.3	868.5	119.	318.	AG	7.	100.0	.0	12.0	.44	6.1
21. SB Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	697.	.9	.0	32.0		
22. SB Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	697.	.9	.0	32.0		

1 PAGE 2

JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT) RUN: Site 3 BUILD 4 AM
DATE: 03/22/2010 TIME: 11:38:57.92

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	150	39	2.0	2701	994	4.10	1	3
5. EB Wil LT	150	131	2.0	182	84	4.10	1	3
9. WB Wil T+R	150	60	2.0	3030	990	4.10	1	3
11. WB Wil LT	150	60	2.0	96	53	4.10	1	3
14. NB Gln AP	150	116	2.0	371	64	4.10	1	3
18. SB Gln T+LT	150	116	2.0	363	689	4.10	1	3
20. SB Gln R	150	99	2.0	220	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT) RUN: Site 3 BUILD 4 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT) RUN: Site 3 BUILD 4 AM

WIND ANGLE (DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
	* CONCENTRATION (PPM)																			
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	85	70	75	0	0	0	0	0	0	105	70	70

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JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT) RUN: Site 3 BUILD 4 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
	* CONCENTRATION (PPM)							
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.1	.1	.1	.0	.0	.0	.0
25.	*	.0	.1	.1	.1	.0	.0	.0	.0
30.	*	.0	.1	.1	.1	.0	.0	.0	.0
35.	*	.0	.1	.1	.1	.0	.0	.0	.0
40.	*	.0	.1	.1	.1	.1	.0	.0	.0
45.	*	.0	.1	.1	.1	.1	.0	.0	.0
50.	*	.0	.1	.1	.1	.1	.0	.0	.0
55.	*	.0	.1	.1	.1	.1	.0	.0	.0
60.	*	.0	.1	.1	.1	.1	.0	.0	.0
65.	*	.1	.1	.1	.2	.1	.0	.0	.0
70.	*	.1	.1	.1	.0	.1	.0	.0	.0
75.	*	.1	.1	.1	.0	.0	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT) RUN: Site 3 BUILD 4 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.1	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.1	.0	.0	.0	.0	.0
250.	*	.1	.1	.1	.0	.0	.0	.0	.0
255.	*	.1	.1	.1	.1	.0	.0	.0	.0
260.	*	.1	.1	.1	.1	.1	.0	.0	.0
265.	*	.0	.1	.1	.1	.1	.0	.0	.0
270.	*	.0	.1	.1	.1	.1	.0	.0	.0
275.	*	.0	.1	.1	.1	.1	.0	.0	.0
280.	*	.0	.1	.1	.1	.1	.0	.0	.0
285.	*	.0	.1	.1	.1	.1	.0	.0	.0
290.	*	.0	.1	.0	.1	.1	.0	.0	.0
295.	*	.0	.1	.0	.1	.1	.0	.0	.0
300.	*	.0	.1	.0	.1	.1	.0	.0	.0
305.	*	.0	.1	.1	.1	.1	.0	.0	.0
310.	*	.0	.1	.1	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.1	.1	.2	.1	.0	.0	.0
DEGR.	*	65	0	0	65	40	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT) RUN: Site 3 BUILD A4 PM
DATE: 03/22/2010 TIME: 11:53:49.19

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	*	323.0	617.0	-426.0	376.0	*	787.	252.	AG	2660.	.8	.0	68.0		
2. EB Wil T+R	*	323.0	616.0	531.0	681.0	*	218.	73.	AG	2445.	.8	.0	68.0		
3. EB Wil T+R	*	475.0	663.0	-6848.2	-1594.2	*	7663.	253.	AG	16.	100.0	.0	48.0	****	389.3
4. EB Wil LT	*	315.0	650.0	513.0	712.0	*	207.	73.	AG	205.	.8	.0	44.0		
5. EB Wil LT	*	444.0	690.0	-679.4	345.0	*	1175.	253.	AG	19.	100.0	.0	24.0	****	59.7
6. EB Wil DP	*	532.0	683.0	1471.0	989.0	*	988.	72.	AG	2820.	.8	.0	68.0		
7. WB Wil AP	*	756.0	830.0	1454.0	1051.0	*	732.	72.	AG	2950.	.8	.0	68.0		
8. WB Wil T+R	*	756.0	829.0	484.0	742.0	*	286.	252.	AG	2818.	.8	.0	68.0		
9. WB Wil T+R	*	540.0	760.0	3310.0	1644.3	*	2908.	72.	AG	23.	100.0	.0	48.0	1.55	147.7
10. WB Wil LT	*	767.0	790.0	513.0	706.0	*	268.	252.	AG	132.	.8	.0	32.0		
11. WB Wil LT	*	566.0	723.0	1684.4	1092.0	*	1178.	72.	AG	6.	100.0	.0	12.0	4.40	59.8
12. WB Wil DP	*	483.0	742.0	-451.0	441.0	*	981.	252.	AG	3022.	.8	.0	68.0		
13. NB Gln AP	*	542.0	703.0	861.0	-211.0	*	968.	161.	AG	880.	.9	.0	32.0		
14. NB Gln AP	*	564.0	640.0	3436.0	-7604.3	*	8730.	161.	AG	7.	100.0	.0	12.0	****	443.5
15. NB Gln DP	*	545.0	705.0	-160.0	1462.0	*	1034.	317.	AG	1010.	.9	.0	32.0		
16. SB Gln AP	*	305.0	915.0	-182.0	1445.0	*	720.	317.	AG	1034.	.9	.0	32.0		
17. SB Gln T+LT	*	305.0	915.0	479.0	736.0	*	250.	136.	AG	727.	.9	.0	44.0		
18. SB Gln T+LT	*	430.0	786.0	-574.2	1818.9	*	1441.	316.	AG	15.	100.0	.0	24.0	1.46	73.2
19. SB Gln R	*	300.0	890.0	443.0	732.0	*	213.	138.	AG	307.	.9	.0	32.0		
20. SB Gln R	*	400.0	780.0	307.9	882.3	*	138.	318.	AG	6.	100.0	.0	12.0	.45	7.0
21. SB Gln DP	*	478.0	734.0	548.0	638.0	*	119.	144.	AG	672.	.9	.0	32.0		
22. SB Gln DP	*	548.0	638.0	840.0	-220.0	*	906.	161.	AG	672.	.9	.0	32.0		

JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT) RUN: Site 3 BUILD A4 PM
DATE: 03/22/2010 TIME: 11:53:49.19

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	*	150	56	2.0	2445	7	4.10	1	3
5. EB Wil LT	*	150	131	2.0	205	84	4.10	1	3
9. WB Wil T+R	*	150	77	2.0	2818	990	4.10	1	3
11. WB Wil LT	*	150	77	2.0	132	66	4.10	1	3
14. NB Gln AP	*	150	99	2.0	880	282	4.10	1	3
18. SB Gln T+LT	*	150	99	2.0	727	794	4.10	1	3
20. SB Gln R	*	150	82	2.0	307	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. SE MID S	*	685.0	365.0	5.0	*
2. SE 164 S	*	638.0	508.0	5.0	*
3. SE 82 S	*	611.0	586.0	5.0	*
4. SE CNR	*	595.0	659.0	5.0	*
5. SE 82 E	*	664.0	689.0	5.0	*
6. SE 164 E	*	742.0	713.0	5.0	*
7. SE MID E	*	849.0	747.0	5.0	*
8. NE MID E	*	793.0	878.0	5.0	*
9. NE 164 E	*	674.0	839.0	5.0	*
10. NE 82 E	*	595.0	813.0	5.0	*
11. NE CNR	*	515.0	792.0	5.0	*
12. NE 82 N	*	452.0	847.0	5.0	*
13. NE 164 N	*	396.0	907.0	5.0	*
14. NE MID N	*	319.0	990.0	5.0	*
15. NW MID N	*	190.0	983.0	5.0	*
16. NW 164 N	*	267.0	900.0	5.0	*
17. NW 82 N	*	323.0	841.0	5.0	*
18. NW CNR	*	381.0	759.0	5.0	*
19. NW 82 W	*	299.0	719.0	5.0	*
20. NW 164 W	*	222.0	694.0	5.0	*
21. NW MID W	*	107.0	658.0	5.0	*
22. SW MID W	*	213.0	548.0	5.0	*
23. SW 164 W	*	367.0	595.0	5.0	*
24. SW 82 W	*	447.0	619.0	5.0	*
25. SW CNR	*	518.0	634.0	5.0	*
26. SW 82 S	*	550.0	565.0	5.0	*
27. SW 164 S	*	577.0	487.0	5.0	*
28. SW MID S	*	622.0	354.0	5.0	*

JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT) RUN: Site 3 BUILD A4 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1

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WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.1	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	90	70	75	0	0	0	0	0	0	100	70	65

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.2	.2	.1	.0	.0	.0	.0
25.	*	.0	.2	.2	.1	.0	.0	.0	.0
30.	*	.0	.2	.2	.1	.0	.0	.0	.0
35.	*	.0	.2	.2	.1	.1	.0	.0	.0
40.	*	.0	.2	.2	.1	.1	.0	.0	.0
45.	*	.0	.2	.2	.1	.1	.0	.0	.0
50.	*	.0	.2	.2	.1	.1	.0	.0	.0
55.	*	.0	.2	.1	.1	.1	.0	.0	.0
60.	*	.0	.2	.1	.2	.1	.0	.0	.0
65.	*	.1	.2	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.1	.1	.0	.0	.0
75.	*	.1	.0	.1	.0	.1	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT) RUN: Site 3 BUILD A4 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.0	.0	.0	.0	.0
250.	*	.1	.2	.2	.1	.0	.0	.0	.0
255.	*	.1	.2	.2	.1	.1	.0	.0	.0
260.	*	.1	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.2	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.0	.0	.0
285.	*	.0	.2	.1	.2	.1	.0	.0	.0
290.	*	.0	.2	.1	.2	.1	.0	.0	.0
295.	*	.0	.2	.1	.2	.1	.0	.0	.0
300.	*	.0	.2	.1	.2	.1	.0	.0	.0
305.	*	.0	.2	.1	.2	.1	.0	.0	.0
310.	*	.0	.1	.0	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.0	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.2	.2	.2	.2	.0	.0	.0
DEGR.	*	65	20	20	60	260	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT) RUN: Site 3 BUILD 5 AM
DATE: 03/22/2010 TIME: 11:45:12.84

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2901.	.8	.0	68.0		
2. EB Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2690.	.8	.0	68.0		
3. EB Wil T+R	475.0	663.0	148.6	562.4	342.	253.	AG	13.	100.0	.0	48.0	1.01	17.4
4. EB Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	211.	.8	.0	44.0		
5. EB Wil LT	444.0	690.0	-792.4	310.3	1293.	253.	AG	20.	100.0	.0	24.0	****	65.7
6. EB Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2446.	.8	.0	68.0		
7. WB Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	3128.	.8	.0	68.0		
8. WB Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	3032.	.8	.0	68.0		
9. WB Wil T+R	540.0	760.0	2715.5	1454.5	2284.	72.	AG	18.	100.0	.0	48.0	1.34	116.0
10. WB Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	96.	.8	.0	32.0		
11. WB Wil LT	566.0	723.0	1294.5	963.4	767.	72.	AG	4.	100.0	.0	12.0	3.20	39.0
12. WB Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2795.	.8	.0	68.0		
13. NB Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	374.	.9	.0	32.0		
14. NB Gln AP	564.0	640.0	1847.0	-3043.1	3900.	161.	AG	8.	100.0	.0	12.0	****	198.1
15. NB Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	975.	.9	.0	32.0		
16. SB Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	574.	.9	.0	32.0		
17. SB Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	367.	.9	.0	44.0		
18. SB Gln T+LT	430.0	786.0	251.4	969.7	256.	316.	AG	16.	100.0	.0	24.0	1.05	13.0
19. SB Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	207.	.9	.0	32.0		
20. SB Gln R	400.0	780.0	325.0	863.3	112.	318.	AG	7.	100.0	.0	12.0	.41	5.7
21. SB Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	761.	.9	.0	32.0		
22. SB Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	761.	.9	.0	32.0		

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JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT) RUN: Site 3 BUILD 5 AM
DATE: 03/22/2010 TIME: 11:45:12.84

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	150	45	2.0	2690	992	4.10	1	3
5. EB Wil LT	150	137	2.0	211	84	4.10	1	3
9. WB Wil T+R	150	60	2.0	3032	989	4.10	1	3
11. WB Wil LT	150	60	2.0	96	53	4.10	1	3
14. NB Gln AP	150	110	2.0	374	141	4.10	1	3
18. SB Gln T+LT	150	110	2.0	367	733	4.10	1	3
20. SB Gln R	150	99	2.0	207	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

1 PAGE 3

JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT) RUN: Site 3 BUILD 5 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	* CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT) RUN: Site 3 BUILD 5 AM

WIND ANGLE (DEGR)* | * CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	85	70	75	0	0	0	0	0	0	105	70	70

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JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT) RUN: Site 3 BUILD 5 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)* | * CONCENTRATION (PPM)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.1	.1	.1	.0	.0	.0	.0
25.	*	.0	.1	.1	.1	.0	.0	.0	.0
30.	*	.0	.1	.1	.1	.0	.0	.0	.0
35.	*	.0	.1	.1	.1	.0	.0	.0	.0
40.	*	.0	.1	.1	.1	.1	.0	.0	.0
45.	*	.0	.2	.1	.1	.1	.0	.0	.0
50.	*	.0	.2	.1	.1	.1	.0	.0	.0
55.	*	.0	.2	.1	.1	.1	.0	.0	.0
60.	*	.0	.1	.1	.1	.1	.0	.0	.0
65.	*	.1	.1	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.0	.1	.0	.0	.0
75.	*	.1	.1	.1	.0	.0	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT) RUN: Site 3 BUILD 5 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.1	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.1	.0	.0	.0	.0	.0
250.	*	.1	.1	.1	.0	.0	.0	.0	.0
255.	*	.1	.1	.1	.1	.0	.0	.0	.0
260.	*	.1	.1	.1	.2	.1	.0	.0	.0
265.	*	.0	.1	.1	.1	.1	.0	.0	.0
270.	*	.0	.1	.1	.2	.1	.0	.0	.0
275.	*	.0	.1	.1	.2	.1	.0	.0	.0
280.	*	.0	.1	.1	.1	.1	.0	.0	.0
285.	*	.0	.1	.1	.1	.1	.0	.0	.0
290.	*	.0	.1	.0	.1	.1	.0	.0	.0
295.	*	.0	.1	.0	.1	.1	.0	.0	.0
300.	*	.0	.1	.0	.1	.1	.0	.0	.0
305.	*	.0	.1	.1	.1	.1	.0	.0	.0
310.	*	.0	.1	.1	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.1	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.2	.1	.2	.1	.0	.0	.0
DEGR.	*	65	45	0	260	40	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT) RUN: Site 3 BUILD A5 PM
DATE: 03/22/2010 TIME: 12:01:57.15

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2699.	.8	.0	68.0		
2. EB Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	2469.	.8	.0	68.0		
3. EB Wil T+R	475.0	663.0	-6920.5	-1616.4	7739.	253.	AG	16.	100.0	.0	48.0	****	393.1
4. EB Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	230.	.8	.0	44.0		
5. EB Wil LT	444.0	690.0	-831.6	298.3	1334.	253.	AG	19.	100.0	.0	24.0	****	67.8
6. EB Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2814.	.8	.0	68.0		
7. WB Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	2904.	.8	.0	68.0		
8. WB Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	2772.	.8	.0	68.0		
9. WB Wil T+R	540.0	760.0	3270.5	1631.7	2866.	72.	AG	23.	100.0	.0	48.0	1.55	145.6
10. WB Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	132.	.8	.0	32.0		
11. WB Wil LT	566.0	723.0	1685.1	1092.2	1178.	72.	AG	6.	100.0	.0	12.0	4.40	59.9
12. WB Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2979.	.8	.0	68.0		
13. NB Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	881.	.9	.0	32.0		
14. NB Gln AP	564.0	640.0	3435.5	-7602.9	8729.	161.	AG	7.	100.0	.0	12.0	9.90	443.4
15. NB Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	1031.	.9	.0	32.0		
16. SB Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	1010.	.9	.0	32.0		
17. SB Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	705.	.9	.0	44.0		
18. SB Gln T+LT	430.0	786.0	-471.2	1712.9	1293.	316.	AG	15.	100.0	.0	24.0	1.40	65.7
19. SB Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	305.	.9	.0	32.0		
20. SB Gln R	400.0	780.0	309.6	880.4	135.	318.	AG	6.	100.0	.0	12.0	.44	6.9
21. SB Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	670.	.9	.0	32.0		
22. SB Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	670.	.9	.0	32.0		

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JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT) RUN: Site 3 BUILD A5 PM
DATE: 03/22/2010 TIME: 12:01:57.15

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	150	56	2.0	2469	7	4.10	1	3
5. EB Wil LT	150	130	2.0	230	84	4.10	1	3
9. WB Wil T+R	150	78	2.0	2772	989	4.10	1	3
11. WB Wil LT	150	78	2.0	132	68	4.10	1	3
14. NB Gln AP	150	99	2.0	881	285	4.10	1	3
18. SB Gln T+LT	150	99	2.0	705	804	4.10	1	3
20. SB Gln R	150	81	2.0	305	1600	4.10	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

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JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT) RUN: Site 3 BUILD A5 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
50. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
55. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
60. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
65. *	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
70. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1
75. *	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
80. *	.0	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
85. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
90. *	.0	.0	.0	.0	.0	.0	.0	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
95. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
100. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
105. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
110. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
115. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
120. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
125. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
130. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
135. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
140. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
145. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
150. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
155. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
160. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
165. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
170. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
175. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
180. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
185. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
190. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
195. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
200. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
205. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1

1

JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT) RUN: Site 3 BUILD A5 PM

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
215. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
220. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
225. *	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
230. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
235. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
245. *	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
250. *	.0	.0	.0	.0	.0	.1	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
255. *	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
260. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
265. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300. *	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360. *	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
MAX *	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
DEGR. *	0	0	0	0	0	0	0	70	90	70	75	0	0	0	0	0	0	105	70	65

1

JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT) RUN: Site 3 BUILD A5 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.1	.1	.1	.0	.0	.0	.0

5.	*	.0	.1	.1	.1	.0	.0	.0	.0
10.	*	.0	.1	.1	.1	.0	.0	.0	.0
15.	*	.0	.1	.1	.1	.0	.0	.0	.0
20.	*	.0	.2	.2	.1	.0	.0	.0	.0
25.	*	.0	.2	.2	.1	.0	.0	.0	.0
30.	*	.0	.2	.2	.1	.0	.0	.0	.0
35.	*	.0	.2	.2	.1	.1	.0	.0	.0
40.	*	.0	.2	.2	.1	.1	.0	.0	.0
45.	*	.0	.2	.2	.1	.1	.0	.0	.0
50.	*	.0	.2	.2	.1	.1	.0	.0	.0
55.	*	.0	.2	.1	.1	.1	.0	.0	.0
60.	*	.0	.2	.1	.2	.1	.0	.0	.0
65.	*	.1	.2	.1	.1	.1	.0	.0	.0
70.	*	.1	.1	.1	.1	.1	.0	.0	.0
75.	*	.1	.0	.1	.0	.1	.0	.0	.0
80.	*	.1	.0	.0	.0	.0	.0	.0	.0
85.	*	.1	.0	.0	.0	.0	.0	.0	.0
90.	*	.1	.0	.0	.0	.0	.0	.0	.0
95.	*	.1	.0	.0	.0	.0	.0	.0	.0
100.	*	.1	.0	.0	.0	.0	.0	.0	.0
105.	*	.1	.0	.0	.0	.0	.0	.0	.0
110.	*	.1	.0	.0	.0	.0	.0	.0	.0
115.	*	.1	.0	.0	.0	.0	.0	.0	.0
120.	*	.1	.0	.0	.0	.0	.0	.0	.0
125.	*	.1	.0	.0	.0	.0	.0	.0	.0
130.	*	.1	.0	.0	.0	.0	.0	.0	.0
135.	*	.1	.0	.0	.0	.0	.0	.0	.0
140.	*	.1	.0	.0	.0	.0	.0	.0	.0
145.	*	.1	.0	.0	.0	.0	.0	.0	.0
150.	*	.1	.0	.0	.0	.0	.0	.0	.0
155.	*	.1	.0	.0	.0	.0	.0	.0	.0
160.	*	.1	.0	.0	.0	.0	.0	.0	.0
165.	*	.1	.0	.0	.0	.0	.0	.0	.0
170.	*	.1	.0	.0	.0	.0	.0	.0	.0
175.	*	.1	.0	.0	.0	.0	.0	.0	.0
180.	*	.1	.0	.0	.0	.0	.0	.0	.0
185.	*	.1	.0	.0	.0	.0	.0	.0	.0
190.	*	.1	.0	.0	.0	.0	.0	.0	.0
195.	*	.1	.0	.0	.0	.0	.0	.0	.0
200.	*	.1	.0	.0	.0	.0	.0	.0	.0
205.	*	.1	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT) RUN: Site 3 BUILD A5 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.1	.0	.0	.0	.0	.0	.0	.0
215.	*	.1	.0	.0	.0	.0	.0	.0	.0
220.	*	.1	.0	.0	.0	.0	.0	.0	.0
225.	*	.1	.0	.0	.0	.0	.0	.0	.0
230.	*	.1	.0	.0	.0	.0	.0	.0	.0
235.	*	.1	.0	.0	.0	.0	.0	.0	.0
240.	*	.1	.0	.0	.0	.0	.0	.0	.0
245.	*	.1	.1	.0	.0	.0	.0	.0	.0
250.	*	.1	.2	.2	.1	.0	.0	.0	.0
255.	*	.1	.2	.2	.1	.1	.0	.0	.0
260.	*	.1	.2	.2	.2	.2	.0	.0	.0
265.	*	.0	.2	.2	.2	.2	.0	.0	.0
270.	*	.0	.2	.2	.2	.2	.0	.0	.0
275.	*	.0	.2	.2	.2	.2	.0	.0	.0
280.	*	.0	.2	.2	.2	.1	.0	.0	.0
285.	*	.0	.2	.2	.2	.1	.0	.0	.0
290.	*	.0	.2	.1	.2	.1	.0	.0	.0
295.	*	.0	.2	.1	.2	.1	.0	.0	.0
300.	*	.0	.2	.1	.2	.1	.0	.0	.0
305.	*	.0	.2	.1	.2	.1	.0	.0	.0
310.	*	.0	.1	.0	.1	.1	.0	.0	.0
315.	*	.0	.1	.1	.1	.1	.0	.0	.0
320.	*	.0	.1	.1	.1	.1	.0	.0	.0
325.	*	.0	.1	.1	.1	.1	.0	.0	.0
330.	*	.0	.1	.1	.1	.1	.0	.0	.0
335.	*	.0	.1	.1	.1	.1	.0	.0	.0
340.	*	.0	.1	.1	.1	.1	.0	.0	.0
345.	*	.0	.1	.1	.1	.1	.0	.0	.0
350.	*	.0	.1	.1	.1	.1	.0	.0	.0
355.	*	.0	.1	.1	.1	.0	.0	.0	.0
360.	*	.0	.1	.1	.1	.0	.0	.0	.0
MAX	*	.1	.2	.2	.2	.2	.0	.0	.0
DEGR.	*	65	20	20	60	260	0	0	0

THE HIGHEST CONCENTRATION IS .30 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 70 DEGREES FROM REC10.

Site 3

Existing with Project

Input & Output Files

```
Site 3 Glendon & Wilsh (S3EXWPAM.DAT)   60.0321.0.0000.000280.30480000
1    1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 Existing WITH PROJ AM            22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2208 3.3  0.  68
30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    1947 3.3  0.  68
30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
      150        33       2.0 1947   20.5 1002 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     261 3.3  0.  44
30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
      150       125       2.0  261   20.5 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    1899 3.3  0.  68
30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2420 3.3  0.  68
30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2354 3.3  0.  68
30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
      150        60       2.0 2354   20.5  992 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      66 3.3  0.  32
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30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
       150        60       2.0   66   20.5  102 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2165 3.3  0.  68
30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     176 3.5  0.  32
30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       122       2.0  176   20.5 1139 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     710 3.5  0.  32
30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     226 3.5  0.  32
30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     116 3.5  0.  44
30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       122       2.0  116   20.5  816 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     110 3.5  0.  32
30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        99       2.0  110   20.5 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     256 3.5  0.  32
30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     256 3.5  0.  32
30.
1.0   04 1000.   0Y  5  0 72
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JOB: Site 3 Glendon & Wilsh (S3EXWPAM.DAT) RUN: Site 3 Existing WITH PROJ AM
DATE: 07/13/2011 TIME: 12:03:17.67

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Wil AP	*	323.0	617.0	-426.0	376.0	*	787.	252.	AG	2208.	3.3	.0	68.0		
2. EB Wil T+R	*	323.0	616.0	531.0	681.0	*	218.	73.	AG	1947.	3.3	.0	68.0		
3. EB Wil T+R	*	475.0	663.0	391.2	637.2	*	88.	253.	AG	48.	100.0	.0	48.0	.64	4.5
4. EB Wil LT	*	315.0	650.0	513.0	712.0	*	207.	73.	AG	261.	3.3	.0	44.0		
5. EB Wil LT	*	444.0	690.0	338.8	657.7	*	110.	253.	AG	92.	100.0	.0	24.0	.86	5.6
6. EB Wil DP	*	532.0	683.0	1471.0	989.0	*	988.	72.	AG	1899.	3.3	.0	68.0		
7. WB Wil AP	*	756.0	830.0	1454.0	1051.0	*	732.	72.	AG	2420.	3.3	.0	68.0		
8. WB Wil T+R	*	756.0	829.0	484.0	742.0	*	286.	252.	AG	2354.	3.3	.0	68.0		
9. WB Wil T+R	*	540.0	760.0	1025.8	915.1	*	510.	72.	AG	88.	100.0	.0	48.0	1.04	25.9
10. WB Wil LT	*	767.0	790.0	513.0	706.0	*	268.	252.	AG	66.	3.3	.0	32.0		
11. WB Wil LT	*	566.0	723.0	701.7	767.8	*	143.	72.	AG	22.	100.0	.0	12.0	1.14	7.3
12. WB Wil DP	*	483.0	742.0	-451.0	441.0	*	981.	252.	AG	2165.	3.3	.0	68.0		
13. NB Gln AP	*	542.0	703.0	861.0	-211.0	*	968.	161.	AG	176.	3.5	.0	32.0		
14. NB Gln AP	*	564.0	640.0	619.6	480.4	*	169.	161.	AG	45.	100.0	.0	12.0	.97	8.6
15. NB Gln DP	*	545.0	705.0	-160.0	1462.0	*	1034.	317.	AG	710.	3.5	.0	32.0		
16. SB Gln AP	*	305.0	915.0	-182.0	1445.0	*	720.	317.	AG	226.	3.5	.0	32.0		
17. SB Gln T+LT	*	305.0	915.0	479.0	736.0	*	250.	136.	AG	116.	3.5	.0	44.0		
18. SB Gln T+LT	*	430.0	786.0	403.0	813.7	*	39.	316.	AG	89.	100.0	.0	24.0	.45	2.0
19. SB Gln R	*	300.0	890.0	443.0	732.0	*	213.	138.	AG	110.	3.5	.0	32.0		
20. SB Gln R	*	400.0	780.0	360.2	824.3	*	60.	318.	AG	36.	100.0	.0	12.0	.35	3.0
21. SB Gln DP	*	478.0	734.0	548.0	638.0	*	119.	144.	AG	256.	3.5	.0	32.0		
22. SB Gln DP	*	548.0	638.0	840.0	-220.0	*	906.	161.	AG	256.	3.5	.0	32.0		

JOB: Site 3 Glendon & Wilsh (S3EXWPAM.DAT) RUN: Site 3 Existing WITH PROJ AM
DATE: 07/13/2011 TIME: 12:03:17.67

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB Wil T+R	*	150	33	2.0	1947	1002	20.50	1	3
5. EB Wil LT	*	150	125	2.0	261	1084	20.50	1	3
9. WB Wil T+R	*	150	60	2.0	2354	992	20.50	1	3
11. WB Wil LT	*	150	60	2.0	66	102	20.50	1	3
14. NB Gln AP	*	150	122	2.0	176	1139	20.50	1	3
18. SB Gln T+LT	*	150	122	2.0	116	816	20.50	1	3
20. SB Gln R	*	150	99	2.0	110	1000	20.50	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. SE MID S	*	685.0	365.0	5.0	*
2. SE 164 S	*	638.0	508.0	5.0	*
3. SE 82 S	*	611.0	586.0	5.0	*
4. SE CNR	*	595.0	659.0	5.0	*
5. SE 82 E	*	664.0	689.0	5.0	*
6. SE 164 E	*	742.0	713.0	5.0	*
7. SE MID E	*	849.0	747.0	5.0	*
8. NE MID E	*	793.0	878.0	5.0	*
9. NE 164 E	*	674.0	839.0	5.0	*
10. NE 82 E	*	595.0	813.0	5.0	*
11. NE CNR	*	515.0	792.0	5.0	*
12. NE 82 N	*	452.0	847.0	5.0	*
13. NE 164 N	*	396.0	907.0	5.0	*
14. NE MID N	*	319.0	990.0	5.0	*
15. NW MID N	*	190.0	983.0	5.0	*
16. NW 164 N	*	267.0	900.0	5.0	*
17. NW 82 N	*	323.0	841.0	5.0	*
18. NW CNR	*	381.0	759.0	5.0	*
19. NW 82 W	*	299.0	719.0	5.0	*
20. NW 164 W	*	222.0	694.0	5.0	*
21. NW MID W	*	107.0	658.0	5.0	*
22. SW MID W	*	213.0	548.0	5.0	*
23. SW 164 W	*	367.0	595.0	5.0	*
24. SW 82 W	*	447.0	619.0	5.0	*
25. SW CNR	*	518.0	634.0	5.0	*
26. SW 82 S	*	550.0	565.0	5.0	*
27. SW 164 S	*	577.0	487.0	5.0	*
28. SW MID S	*	622.0	354.0	5.0	*

JOB: Site 3 Glendon & Wilsh (S3EXWPAM.DAT) RUN: Site 3 Existing WITH PROJ AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE	* CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
5. *	.0	.3	.3	.4	.4	.5	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
10. *	.0	.2	.3	.4	.4	.5	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
15. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0
20. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0
25. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0
30. *	.0	.3	.2	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
35. *	.0	.3	.3	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
40. *	.0	.2	.3	.5	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
45. *	.0	.2	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
50. *	.0	.2	.3	.5	.5	.5	.5	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1
55. *	.0	.1	.2	.5	.5	.5	.4	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
60. *	.0	.0	.2	.5	.5	.5	.4	.3	.3	.3	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
65. *	.0	.0	.1	.4	.5	.4	.4	.3	.3	.3	.3	.0	.0	.0	.0	.0	.0	.3	.3	.2
70. *	.0	.0	.1	.3	.4	.3	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.3	.4	.4
75. *	.0	.0	.0	.2	.2	.2	.2	.6	.6	.7	.6	.2	.0	.0	.0	.0	.0	.5	.6	.5
80. *	.0	.0	.0	.1	.2	.1	.1	.7	.8	.7	.8	.2	.0	.0	.0	.0	.2	.5	.5	.6
85. *	.0	.0	.0	.1	.1	.1	.1	.8	.8	.8	.8	.3	.1	.0	.0	.0	.2	.5	.6	.7
90. *	.0	.0	.0	.0	.1	.1	.1	.8	.8	.9	.8	.4	.2	.0	.0	.1	.4	.4	.6	.6
95. *	.0	.0	.0	.0	.1	.0	.0	.8	.8	.8	.7	.4	.3	.0	.0	.1	.3	.4	.6	.5
100. *	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.7	.3	.2	.0	.0	.2	.3	.4	.6	.5
105. *	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.7	.3	.3	.1	.0	.3	.3	.4	.5	.5
110. *	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.6	.3	.3	.1	.0	.2	.3	.4	.5	.5
115. *	.0	.0	.0	.0	.0	.0	.0	.7	.6	.7	.6	.3	.3	.1	.0	.1	.2	.3	.4	.4
120. *	.0	.0	.0	.0	.0	.0	.0	.7	.6	.7	.5	.3	.3	.1	.0	.0	.1	.3	.4	.3
125. *	.0	.0	.0	.0	.0	.0	.0	.7	.6	.6	.5	.3	.3	.1	.0	.0	.1	.3	.4	.4
130. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.2	.0	.0	.0	.1	.3	.4	.3
135. *	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.5	.3	.1	.0	.0	.0	.1	.4	.4	.3
140. *	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.2	.1	.0	.1	.1	.4	.4	.3
145. *	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.2	.1	.0	.1	.2	.4	.4	.3
150. *	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1	.1	.0	.1	.2	.4	.4	.3
155. *	.0	.0	.0	.0	.0	.0	.0	.5	.5	.6	.4	.2	.1	.1	.0	.1	.3	.4	.3	.3
160. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.3	.2	.2	.1	.0	.1	.3	.4	.3	.3
165. *	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.3	.4	.2	.1	.0	.1	.2	.4	.4	.3
170. *	.0	.0	.1	.1	.0	.0	.0	.5	.5	.6	.4	.3	.2	.2	.0	.1	.1	.4	.3	.3
175. *	.0	.0	.1	.1	.0	.0	.0	.5	.5	.5	.4	.3	.2	.2	.0	.1	.1	.4	.3	.3
180. *	.0	.0	.1	.1	.0	.0	.0	.5	.5	.5	.4	.3	.2	.2	.0	.1	.1	.4	.3	.3
185. *	.0	.0	.1	.1	.0	.0	.0	.5	.5	.5	.4	.3	.2	.2	.1	.1	.1	.4	.3	.3
190. *	.0	.0	.1	.1	.0	.0	.0	.5	.6	.5	.4	.3	.2	.2	.1	.2	.2	.4	.3	.3
195. *	.0	.0	.1	.1	.0	.0	.0	.6	.6	.6	.4	.5	.2	.2	.1	.2	.2	.4	.3	.3
200. *	.0	.0	.1	.1	.0	.0	.0	.7	.6	.6	.5	.5	.2	.2	.1	.2	.2	.4	.3	.3
205. *	.0	.0	.1	.1	.0	.0	.0	.7	.7	.7	.5	.4	.2	.2	.1	.2	.2	.4	.3	.3

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JOB: Site 3 Glendon & Wilson (S3EXWPAM.DAT) RUN: Site 3 Existing WITH PROJ AM

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.0	.1	.1	.0	.0	.0	.7	.7	.7	.5	.3	.3	.2	.1	.2	.2	.3	.4	.4
215. *	.0	.1	.1	.1	.0	.0	.0	.7	.7	.6	.5	.4	.3	.2	.1	.2	.2	.3	.4	.4
220. *	.0	.1	.1	.1	.0	.0	.0	.7	.7	.6	.5	.4	.3	.2	.0	.2	.2	.3	.4	.4
225. *	.0	.1	.1	.1	.0	.0	.0	.8	.7	.7	.7	.4	.3	.2	.0	.2	.2	.3	.4	.4
230. *	.0	.1	.1	.1	.0	.0	.0	.8	.7	.7	.7	.4	.3	.1	.0	.1	.2	.4	.4	.4
235. *	.0	.1	.1	.0	.0	.1	.1	.7	.8	.8	.6	.4	.2	.1	.0	.1	.2	.4	.4	.4
240. *	.0	.1	.1	.0	.1	.1	.1	.7	.7	.5	.5	.4	.2	.1	.0	.0	.1	.4	.4	.4
245. *	.0	.1	.1	.2	.2	.1	.1	.6	.7	.6	.5	.2	.1	.1	.0	.0	.1	.3	.4	.4
250. *	.0	.1	.1	.2	.4	.3	.2	.6	.4	.6	.5	.2	.1	.1	.0	.0	.0	.3	.4	.4
255. *	.0	.1	.2	.3	.4	.4	.3	.4	.4	.4	.4	.1	.1	.1	.0	.0	.0	.2	.3	.3
260. *	.0	.1	.2	.4	.5	.5	.3	.4	.3	.2	.2	.1	.1	.1	.0	.0	.0	.1	.2	.2
265. *	.0	.2	.3	.4	.5	.3	.5	.3	.1	.2	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1
270. *	.0	.2	.3	.5	.4	.4	.6	.0	.1	.1	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1
275. *	.0	.3	.4	.4	.4	.4	.4	.0	.1	.0	.2	.1	.1	.1	.0	.0	.0	.0	.1	.1
280. *	.0	.3	.3	.4	.4	.5	.4	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
285. *	.0	.2	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
290. *	.0	.2	.3	.3	.3	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
295. *	.0	.2	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
300. *	.0	.3	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
305. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
310. *	.0	.3	.3	.4	.4	.4	.5	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
315. *	.0	.1	.2	.4	.4	.4	.4	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320. *	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
325. *	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330. *	.0	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335. *	.0	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340. *	.0	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
350. *	.0	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
355. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
360. *	.0	.3	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
MAX *	.0	.3	.4	.5	.5	.5	.6	.8	.8	.9	.8	.5	.3	.2	.1	.3	.4	.5	.6	.7
DEGR. *	0	0	275	40	30	5	270	85	235	90	80	195	95	170	185	105	90	75	75	85

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JOB: Site 3 Glendon & Wilson (S3EXWPAM.DAT) RUN: Site 3 Existing WITH PROJ AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0. *	.0	.3	.4	.5	.2	.2	.2	.0

5.	*	.0	.3	.4	.4	.3	.3	.4	.0
10.	*	.0	.3	.4	.4	.4	.3	.4	.0
15.	*	.0	.3	.4	.5	.4	.4	.4	.0
20.	*	.0	.3	.4	.5	.4	.4	.3	.0
25.	*	.0	.3	.5	.4	.4	.4	.3	.0
30.	*	.0	.4	.5	.5	.4	.4	.3	.0
35.	*	.0	.4	.5	.5	.4	.4	.3	.0
40.	*	.0	.4	.6	.6	.5	.3	.4	.0
45.	*	.0	.4	.6	.6	.5	.4	.3	.0
50.	*	.1	.5	.5	.6	.5	.4	.3	.0
55.	*	.1	.5	.6	.7	.5	.3	.2	.0
60.	*	.1	.5	.7	.6	.4	.3	.1	.0
65.	*	.2	.5	.7	.6	.4	.2	.1	.0
70.	*	.2	.4	.5	.4	.3	.2	.1	.0
75.	*	.3	.4	.3	.2	.2	.1	.1	.0
80.	*	.4	.2	.2	.2	.1	.1	.1	.0
85.	*	.3	.1	.1	.2	.1	.1	.1	.0
90.	*	.3	.1	.1	.0	.0	.1	.0	.0
95.	*	.4	.1	.0	.0	.0	.1	.0	.0
100.	*	.4	.0	.0	.0	.1	.1	.0	.0
105.	*	.4	.0	.0	.0	.1	.1	.0	.0
110.	*	.4	.0	.0	.0	.1	.1	.0	.0
115.	*	.3	.0	.0	.0	.1	.1	.0	.0
120.	*	.3	.0	.0	.0	.1	.1	.0	.0
125.	*	.3	.0	.0	.0	.1	.1	.0	.0
130.	*	.3	.0	.0	.0	.1	.1	.0	.0
135.	*	.3	.0	.0	.0	.1	.1	.0	.0
140.	*	.3	.0	.0	.0	.1	.1	.0	.0
145.	*	.3	.0	.0	.0	.1	.0	.0	.0
150.	*	.3	.0	.0	.0	.0	.0	.0	.0
155.	*	.3	.0	.0	.0	.0	.0	.0	.0
160.	*	.3	.0	.0	.0	.0	.0	.0	.0
165.	*	.3	.0	.0	.0	.0	.0	.0	.0
170.	*	.3	.0	.0	.0	.0	.0	.0	.0
175.	*	.3	.0	.0	.0	.0	.0	.0	.0
180.	*	.3	.0	.0	.0	.0	.0	.0	.0
185.	*	.3	.0	.0	.0	.0	.0	.0	.0
190.	*	.3	.0	.0	.0	.0	.0	.0	.0
195.	*	.3	.0	.0	.0	.0	.0	.0	.0
200.	*	.3	.0	.0	.0	.0	.0	.0	.0
205.	*	.3	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 3 Glendon & Wilson (S3EXWPAM.DAT) RUN: Site 3 Existing WITH PROJ AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.4	.0	.0	.0	.0	.0	.0	.0
215.	*	.4	.0	.0	.0	.0	.0	.0	.0
220.	*	.4	.0	.0	.0	.0	.0	.0	.0
225.	*	.4	.1	.0	.0	.0	.0	.0	.0
230.	*	.4	.1	.0	.0	.0	.0	.0	.0
235.	*	.4	.1	.1	.1	.0	.0	.0	.0
240.	*	.4	.2	.1	.2	.0	.0	.0	.0
245.	*	.4	.2	.3	.2	.2	.0	.0	.0
250.	*	.4	.3	.3	.2	.2	.0	.0	.0
255.	*	.2	.4	.4	.5	.3	.1	.0	.0
260.	*	.2	.5	.5	.5	.5	.1	.0	.0
265.	*	.1	.5	.5	.5	.5	.2	.1	.0
270.	*	.1	.5	.5	.5	.6	.2	.1	.0
275.	*	.1	.4	.4	.5	.6	.2	.2	.0
280.	*	.0	.4	.4	.5	.5	.3	.2	.0
285.	*	.0	.4	.4	.5	.5	.3	.2	.0
290.	*	.0	.4	.3	.5	.5	.2	.2	.0
295.	*	.0	.4	.3	.5	.5	.2	.1	.0
300.	*	.0	.4	.3	.5	.5	.3	.1	.0
305.	*	.0	.3	.4	.5	.5	.3	.1	.0
310.	*	.0	.3	.4	.5	.4	.3	.2	.0
315.	*	.0	.3	.4	.5	.3	.2	.2	.0
320.	*	.0	.3	.3	.5	.3	.2	.2	.0
325.	*	.0	.3	.3	.5	.3	.2	.1	.0
330.	*	.0	.3	.3	.5	.4	.2	.1	.0
335.	*	.0	.3	.4	.5	.4	.1	.0	.0
340.	*	.0	.3	.4	.5	.4	.1	.0	.0
345.	*	.0	.3	.4	.5	.3	.2	.0	.0
350.	*	.0	.3	.4	.5	.3	.1	.0	.0
355.	*	.0	.3	.4	.5	.3	.2	.2	.0
360.	*	.0	.3	.4	.5	.2	.2	.2	.0
MAX	*	.4	.5	.7	.7	.6	.4	.4	.0
DEGR.	*	80	50	60	55	270	15	5	0

THE HIGHEST CONCENTRATION IS .90 PPM AT 90 DEGREES FROM REC10.
THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 235 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS .80 PPM AT 85 DEGREES FROM REC8 .

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Site 3 Glendon & Wilsh (S3EXWPPM.DAT)   60.0321.0.0000.000280.30480000
1    1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 Existing WITH PROJ PM            22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2010 3.3  0.  68
30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    1835 3.3  0.  68
30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.       0.  48   4
      150        56       2.0 1835   20.5 1008 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     175 3.3  0.  44
30.
  2
EB        Wil LT    AG   444.   690.   317.   651.       0.  24   2
      150       133       2.0  175     20.5 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2133 3.3  0.  68
30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2121 3.3  0.  68
30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2042 3.3  0.  68
30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.       0.  48   4
      150        75       2.0 2042   20.5  994 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      79 3.3  0.  32
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30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
       150        75       2.0   79   20.5  102 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2176 3.3  0.  68
30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     366 3.5  0.  32
30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150        99       2.0  366   20.5  557 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     532 3.5  0.  32
30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     792 3.5  0.  32
30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     530 3.5  0.  44
30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150        99       2.0  530   20.5  840 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     262 3.5  0.  32
30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        84       2.0  262   20.5 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     448 3.5  0.  32
30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     448 3.5  0.  32
30.
1.0   04 1000.   0Y  5  0 72
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JOB: Site 3 Glendon & Wilsh (S3EXWPPM.DAT) RUN: Site 3 Existing WITH PROJ PM
DATE: 07/13/2011 TIME: 12:17:47.91

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB	Wil AP	323.0	617.0	-426.0	376.0	787.	252.	AG	2010.	3.3	.0	68.0		
2. EB	Wil T+R	323.0	616.0	531.0	681.0	218.	73.	AG	1835.	3.3	.0	68.0		
3. EB	Wil T+R	475.0	663.0	341.0	621.7	140.	253.	AG	82.	100.0	.0	48.0	.76	7.1
4. EB	Wil LT	315.0	650.0	513.0	712.0	207.	73.	AG	175.	3.3	.0	44.0		
5. EB	Wil LT	444.0	690.0	-21.1	547.2	486.	253.	AG	1.	100.0	.0	24.0	1.98	24.7
6. EB	Wil DP	532.0	683.0	1471.0	989.0	988.	72.	AG	2133.	3.3	.0	68.0		
7. WB	Wil AP	756.0	830.0	1454.0	1051.0	732.	72.	AG	2121.	3.3	.0	68.0		
8. WB	Wil T+R	756.0	829.0	484.0	742.0	286.	252.	AG	2042.	3.3	.0	68.0		
9. WB	Wil T+R	540.0	760.0	1223.3	978.2	717.	72.	AG	110.	100.0	.0	48.0	1.09	36.4
10. WB	Wil LT	767.0	790.0	513.0	706.0	268.	252.	AG	79.	3.3	.0	32.0		
11. WB	Wil LT	566.0	723.0	939.6	846.3	393.	72.	AG	27.	100.0	.0	12.0	1.65	20.0
12. WB	Wil DP	483.0	742.0	-451.0	441.0	981.	252.	AG	2176.	3.3	.0	68.0		
13. NB	Gln AP	542.0	703.0	861.0	-211.0	968.	161.	AG	366.	3.5	.0	32.0		
14. NB	Gln AP	564.0	640.0	1295.4	-1459.4	2223.	161.	AG	36.	100.0	.0	12.0	2.10	112.9
15. NB	Gln DP	545.0	705.0	-160.0	1462.0	1034.	317.	AG	532.	3.5	.0	32.0		
16. SB	Gln AP	305.0	915.0	-182.0	1445.0	720.	317.	AG	792.	3.5	.0	32.0		
17. SB	Gln T+LT	305.0	915.0	479.0	736.0	250.	136.	AG	530.	3.5	.0	44.0		
18. SB	Gln T+LT	430.0	786.0	260.8	960.0	243.	316.	AG	73.	100.0	.0	24.0	1.01	12.3
19. SB	Gln R	300.0	890.0	443.0	732.0	213.	138.	AG	262.	3.5	.0	32.0		
20. SB	Gln R	400.0	780.0	319.5	869.4	120.	318.	AG	31.	100.0	.0	12.0	.63	6.1
21. SB	Gln DP	478.0	734.0	548.0	638.0	119.	144.	AG	448.	3.5	.0	32.0		
22. SB	Gln DP	548.0	638.0	840.0	-220.0	906.	161.	AG	448.	3.5	.0	32.0		

JOB: Site 3 Glendon & Wilsh (S3EXWPPM.DAT) RUN: Site 3 Existing WITH PROJ PM
DATE: 07/13/2011 TIME: 12:17:47.91

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3. EB	Wil T+R	150	56	2.0	1835	1008	20.50	1	3
5. EB	Wil LT	150	133	2.0	175	510	.20	4	1
9. WB	Wil T+R	150	75	2.0	2042	994	20.50	1	3
11. WB	Wil LT	150	75	2.0	79	102	20.50	1	3
14. NB	Gln AP	150	99	2.0	366	557	20.50	1	3
18. SB	Gln T+LT	150	99	2.0	530	840	20.50	1	3
20. SB	Gln R	150	84	2.0	262	1000	20.50	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	685.0	365.0	5.0
2. SE 164 S	638.0	508.0	5.0
3. SE 82 S	611.0	586.0	5.0
4. SE CNR	595.0	659.0	5.0
5. SE 82 E	664.0	689.0	5.0
6. SE 164 E	742.0	713.0	5.0
7. SE MID E	849.0	747.0	5.0
8. NE MID E	793.0	878.0	5.0
9. NE 164 E	674.0	839.0	5.0
10. NE 82 E	595.0	813.0	5.0
11. NE CNR	515.0	792.0	5.0
12. NE 82 N	452.0	847.0	5.0
13. NE 164 N	396.0	907.0	5.0
14. NE MID N	319.0	990.0	5.0
15. NW MID N	190.0	983.0	5.0
16. NW 164 N	267.0	900.0	5.0
17. NW 82 N	323.0	841.0	5.0
18. NW CNR	381.0	759.0	5.0
19. NW 82 W	299.0	719.0	5.0
20. NW 164 W	222.0	694.0	5.0
21. NW MID W	107.0	658.0	5.0
22. SW MID W	213.0	548.0	5.0
23. SW 164 W	367.0	595.0	5.0
24. SW 82 W	447.0	619.0	5.0
25. SW CNR	518.0	634.0	5.0
26. SW 82 S	550.0	565.0	5.0
27. SW 164 S	577.0	487.0	5.0
28. SW MID S	622.0	354.0	5.0

JOB: Site 3 Glendon & Wilsh (S3EXWPPM.DAT) RUN: Site 3 Existing WITH PROJ PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

S3EXWPPM

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.1	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
5.	.1	.2	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
10.	.1	.2	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
15.	.1	.2	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
20.	.1	.2	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
25.	.1	.2	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.3	.3	.1	.1	.0
30.	.1	.2	.2	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.3	.3	.1	.1	.0
35.	.0	.3	.2	.5	.7	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.3	.3	.1	.1	.0
40.	.0	.3	.3	.5	.6	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.3	.3	.1	.1	.0
45.	.0	.3	.3	.7	.6	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.3	.3	.1	.1	.0
50.	.0	.2	.3	.6	.6	.6	.5	.1	.0	.0	.0	.0	.0	.0	.1	.3	.3	.1	.1	.1
55.	.0	.1	.3	.6	.6	.5	.5	.2	.1	.2	.1	.0	.0	.0	.1	.3	.3	.1	.1	.1
60.	.0	.0	.3	.5	.5	.5	.5	.2	.3	.3	.2	.0	.0	.0	.1	.2	.3	.2	.2	.1
65.	.0	.0	.1	.5	.5	.5	.5	.4	.4	.4	.4	.0	.0	.0	.1	.2	.3	.3	.2	.3
70.	.0	.0	.1	.4	.5	.5	.4	.4	.6	.6	.4	.1	.0	.0	.1	.2	.3	.3	.5	.3
75.	.0	.0	.0	.2	.2	.2	.2	.7	.7	.8	.7	.2	.0	.0	.1	.2	.4	.6	.5	.4
80.	.0	.0	.0	.1	.2	.2	.2	.8	.8	.8	.8	.2	.1	.0	.1	.2	.5	.6	.5	.5
85.	.0	.0	.0	.1	.1	.1	.1	.8	.8	.9	.8	.3	.2	.0	.1	.3	.7	.5	.6	.5
90.	.0	.0	.0	.0	.1	.1	.1	.8	1.0	.9	.9	.5	.2	.0	.1	.3	.6	.4	.6	.6
95.	.0	.0	.0	.0	.1	.0	.0	.8	.8	.8	.7	.5	.3	.1	.2	.4	.7	.4	.5	.5
100.	.0	.0	.0	.0	.0	.0	.0	.8	.8	.8	.7	.4	.2	.1	.3	.5	.7	.5	.5	.5
105.	.0	.0	.0	.0	.0	.0	.0	.8	.8	.7	.6	.4	.2	.1	.3	.5	.6	.5	.5	.5
110.	.0	.0	.0	.0	.0	.0	.0	.8	.8	.7	.6	.4	.3	.1	.3	.5	.6	.4	.5	.5
115.	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.6	.3	.3	.1	.3	.4	.6	.3	.4	.5
120.	.0	.0	.0	.0	.0	.0	.0	.6	.7	.7	.6	.3	.3	.1	.1	.2	.2	.3	.4	.4
125.	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.3	.1	.1	.1	.3	.3	.4	.3
130.	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.3	.1	.1	.1	.3	.3	.4	.3
135.	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.2	.0	.1	.1	.2	.4	.4	.3
140.	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.5	.3	.1	.0	.1	.1	.1	.4	.4	.3
145.	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.1	.2	.0	.1	.2	.4	.4	.3
150.	.0	.0	.0	.0	.0	.0	.0	.6	.6	.6	.4	.2	.1	.2	.0	.1	.3	.4	.4	.3
155.	.1	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.2	.1	.2	.0	.1	.3	.4	.4	.3
160.	.1	.1	.1	.1	.0	.0	.0	.6	.6	.6	.5	.2	.3	.2	.0	.1	.3	.4	.3	.3
165.	.2	.1	.1	.1	.0	.0	.0	.6	.6	.6	.4	.2	.3	.2	.0	.1	.2	.4	.3	.3
170.	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.3	.3	.3	.0	.1	.1	.4	.3	.3
175.	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.3	.3	.3	.0	.1	.1	.4	.3	.3
180.	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.3	.3	.3	.0	.1	.1	.4	.3	.3
185.	.2	.2	.2	.1	.0	.0	.0	.6	.6	.6	.3	.4	.3	.3	.1	.1	.1	.4	.3	.3
190.	.2	.1	.1	.1	.0	.0	.0	.6	.6	.6	.3	.4	.3	.3	.1	.1	.1	.4	.3	.3
195.	.2	.1	.1	.1	.0	.0	.0	.6	.6	.6	.3	.4	.3	.3	.1	.1	.2	.4	.3	.3
200.	.1	.1	.1	.1	.0	.0	.0	.6	.6	.6	.5	.4	.3	.3	.1	.2	.2	.3	.3	.3
205.	.1	.1	.1	.1	.0	.0	.0	.7	.6	.6	.5	.3	.3	.3	.1	.2	.2	.3	.3	.3

1

JOB: Site 3 Glendon & Wilsh (S3EXWPPM.DAT) RUN: Site 3 Existing WITH PROJ PM

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.8	.7	.7	.4	.3	.4	.3	.1	.2	.2	.3	.4	.4
215.	.1	.1	.1	.1	.0	.0	.0	.8	.7	.6	.4	.3	.4	.3	.1	.2	.2	.3	.4	.4
220.	.1	.1	.1	.1	.0	.0	.0	.8	.8	.6	.4	.4	.4	.3	.0	.2	.2	.3	.4	.4
225.	.1	.1	.1	.0	.0	.0	.0	.7	.8	.8	.5	.4	.4	.3	.0	.1	.2	.3	.4	.4
230.	.1	.1	.1	.0	.0	.0	.0	.8	.7	.7	.6	.4	.4	.2	.0	.1	.2	.4	.4	.4
235.	.1	.1	.1	.0	.1	.1	.1	.8	.7	.7	.4	.4	.3	.2	.0	.1	.2	.4	.4	.4
240.	.1	.1	.1	.0	.1	.1	.1	.9	.8	.6	.4	.4	.3	.2	.0	.0	.1	.4	.4	.4
245.	.1	.1	.1	.2	.1	.1	.1	.7	.6	.6	.4	.3	.2	.2	.0	.0	.1	.3	.4	.4
250.	.1	.1	.1	.3	.4	.3	.2	.5	.5	.6	.4	.3	.2	.1	.0	.0	.0	.3	.4	.4
255.	.1	.1	.2	.4	.6	.4	.3	.5	.4	.3	.2	.2	.2	.1	.0	.0	.0	.2	.3	.3
260.	.1	.1	.2	.5	.6	.3	.4	.4	.3	.2	.1	.2	.2	.1	.0	.0	.0	.1	.2	.2
265.	.1	.1	.3	.5	.5	.3	.6	.2	.2	.2	.2	.2	.2	.2	.0	.0	.0	.1	.1	.1
270.	.1	.2	.3	.4	.4	.4	.6	.0	.1	.2	.1	.2	.2	.2	.0	.0	.0	.0	.1	.1
275.	.1	.3	.5	.4	.4	.6	.5	.0	.0	.1	.2	.2	.2	.2	.0	.0	.0	.0	.1	.1
280.	.1	.3	.4	.4	.3	.6	.5	.0	.0	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
285.	.1	.2	.4	.3	.4	.5	.5	.0	.0	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
290.	.1	.2	.4	.3	.3	.4	.6	.0	.0	.1	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
295.	.1	.2	.4	.3	.4	.4	.5	.0	.0	.0	.2	.2	.3	.2	.0	.0	.0	.0	.0	.0
300.	.1	.3	.3	.4	.4	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
305.	.1	.3	.3	.4	.4	.4	.5	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.0	.0	.0
310.	.2	.3	.3	.5	.4	.4	.6	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0
315.	.2	.1	.2	.4	.4	.4	.5	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.2	.1	.0	.4	.4	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0
325.	.2	.1	.1	.4	.4	.5	.4	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0
330.	.2	.1	.2	.4	.4	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0
335.	.1	.0	.2	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0
340.	.1	.1	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0
345.	.0	.2	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
350.	.0	.3	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
355.	.1	.3	.3	.4	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.0	.0
360.	.1	.2	.3	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.2	.1	.0
MAX DEGR.	.2 165	.3 35	.5 275	.7 45	.7 35	.6 35	.6 35	.9 240	1.0 90	.9 85	.9 90	.5 90	.4 210	.3 170	.3 100	.5 100	.7 85	.6 75	.6 85	.6 90

1

JOB: Site 3 Glendon & Wilsh (S3EXWPPM.DAT) RUN: Site 3 Existing WITH PROJ PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.3	.5	.5	.3	.3	.4	.2

5.	*	.0	.3	.5	.5	.5	.4	.4	.3
10.	*	.0	.3	.5	.5	.5	.4	.4	.3
15.	*	.0	.3	.5	.5	.4	.4	.4	.3
20.	*	.0	.3	.6	.6	.4	.4	.4	.3
25.	*	.0	.3	.6	.5	.4	.5	.4	.3
30.	*	.0	.3	.6	.6	.4	.5	.4	.4
35.	*	.0	.3	.6	.6	.6	.4	.4	.4
40.	*	.0	.3	.8	.6	.6	.4	.4	.2
45.	*	.0	.3	.7	.6	.5	.4	.5	.2
50.	*	.1	.4	.8	.7	.6	.4	.3	.1
55.	*	.1	.6	.7	.8	.6	.4	.3	.2
60.	*	.1	.7	.7	.8	.5	.4	.3	.2
65.	*	.3	.6	.6	.6	.4	.3	.2	.2
70.	*	.3	.6	.5	.4	.4	.3	.2	.2
75.	*	.5	.6	.5	.3	.2	.2	.2	.2
80.	*	.5	.2	.3	.2	.1	.2	.2	.2
85.	*	.5	.1	.2	.2	.1	.2	.2	.2
90.	*	.3	.1	.1	.0	.0	.1	.2	.2
95.	*	.3	.0	.0	.0	.0	.1	.2	.2
100.	*	.4	.0	.0	.0	.0	.2	.2	.2
105.	*	.4	.0	.0	.0	.0	.2	.2	.2
110.	*	.4	.0	.0	.0	.1	.2	.2	.2
115.	*	.4	.0	.0	.0	.1	.2	.2	.2
120.	*	.3	.0	.0	.0	.1	.2	.2	.2
125.	*	.3	.0	.0	.0	.1	.2	.2	.2
130.	*	.3	.0	.0	.0	.2	.2	.2	.2
135.	*	.3	.0	.0	.0	.2	.2	.2	.2
140.	*	.3	.0	.0	.0	.2	.2	.2	.2
145.	*	.3	.0	.0	.0	.2	.2	.2	.2
150.	*	.3	.0	.0	.0	.2	.2	.2	.2
155.	*	.3	.0	.0	.0	.2	.2	.2	.2
160.	*	.3	.0	.0	.0	.1	.2	.2	.2
165.	*	.3	.0	.0	.0	.0	.2	.2	.2
170.	*	.3	.0	.0	.0	.0	.0	.0	.0
175.	*	.3	.0	.0	.0	.0	.0	.0	.0
180.	*	.3	.0	.0	.0	.0	.0	.0	.0
185.	*	.3	.0	.0	.0	.0	.0	.0	.0
190.	*	.3	.0	.0	.0	.0	.0	.0	.0
195.	*	.3	.0	.0	.0	.0	.0	.0	.0
200.	*	.3	.0	.0	.0	.0	.0	.0	.0
205.	*	.3	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 3 Glendon & Wilson (S3EXWPPM.DAT) RUN: Site 3 Existing WITH PROJ PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	*	.4	.0	.0	.0	.0	.0	.0	.0
215.	*	.4	.0	.0	.0	.0	.0	.0	.0
220.	*	.4	.0	.0	.0	.0	.0	.0	.0
225.	*	.4	.1	.0	.0	.0	.0	.0	.0
230.	*	.4	.1	.0	.0	.0	.0	.0	.0
235.	*	.4	.1	.1	.0	.0	.0	.0	.0
240.	*	.4	.1	.1	.2	.0	.0	.0	.0
245.	*	.4	.2	.2	.2	.2	.0	.0	.0
250.	*	.3	.3	.3	.3	.3	.0	.0	.0
255.	*	.2	.4	.4	.4	.4	.1	.0	.0
260.	*	.2	.4	.4	.5	.5	.1	.0	.0
265.	*	.1	.4	.4	.6	.6	.2	.0	.0
270.	*	.1	.4	.4	.6	.6	.2	.1	.0
275.	*	.1	.4	.4	.6	.6	.2	.2	.0
280.	*	.0	.4	.4	.6	.5	.2	.2	.0
285.	*	.0	.4	.4	.6	.5	.3	.2	.0
290.	*	.0	.4	.4	.6	.5	.3	.1	.0
295.	*	.0	.3	.4	.6	.4	.3	.1	.0
300.	*	.0	.3	.4	.6	.4	.3	.1	.0
305.	*	.0	.3	.4	.6	.4	.3	.1	.0
310.	*	.0	.3	.5	.5	.4	.3	.3	.0
315.	*	.0	.3	.4	.5	.4	.3	.3	.0
320.	*	.0	.3	.4	.5	.4	.3	.3	.0
325.	*	.0	.3	.5	.5	.4	.2	.1	.0
330.	*	.0	.3	.5	.5	.4	.2	.1	.0
335.	*	.0	.3	.5	.6	.3	.1	.0	.0
340.	*	.0	.3	.5	.6	.3	.1	.0	.0
345.	*	.0	.3	.5	.6	.3	.1	.0	.1
350.	*	.0	.3	.5	.6	.3	.1	.1	.2
355.	*	.0	.3	.5	.5	.4	.2	.1	.2
360.	*	.0	.3	.5	.5	.3	.3	.4	.2
MAX	*	.5	.7	.8	.8	.6	.5	.5	.4
DEGR.	*	75	60	40	60	35	25	45	30

THE HIGHEST CONCENTRATION IS 1.00 PPM AT 90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS .90 PPM AT 240 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS .90 PPM AT 85 DEGREES FROM REC10.

Site 4 – Beverly & La Cienega
Input Files

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Site 4 Bev & La Cien (S4EXAM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 Existing AM                      33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     699 3.3   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     699 3.3   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     699 3.3   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     565 3.3   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  565   20.5 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      53 3.3   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   53   20.5 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      81 3.3   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   81   20.5 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     837 3.3   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1325 3.3   0  44   30.
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  1
WB        Bev T+R   AG   683.   690.   443.   689.    1055 3.3   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.       0.  24   2
      120         68       2.0 1055   20.5 1556 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     270 3.3   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.       0.  24   2
      120        110       2.0  270   20.5 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1331 3.3   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1331 3.3   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1331 3.3   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1331 3.3   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1116 3.3   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.     815 3.3   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.       0.  24   2
      120         79       2.0  815   20.5 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     202 3.3   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.       0.  12   1
      120         71       2.0  202   20.5 1353 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 3.3   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.       0.  12   1
      120         72       2.0   99   20.5  165 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.     965 3.3   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1513 3.3   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1443 3.3   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.       0.  36   3
      120         80       2.0 1443   20.5 1448 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      70 3.3   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.       0.  12   1
      120         75       2.0   70   20.5  264 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1520 3.3   0  56   30.
1.0   04 1000.   0Y  5  0 72
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Site 4 Bev & La Cien (S4EXPM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 Existing PM                      33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1694 3.3   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1694 3.3   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1694 3.3   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1324 3.3   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
      120         70       2.0 1324   20.5 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.     104 3.3   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
      120         63       2.0  104   20.5 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     266 3.3   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
      120        110       2.0  266   20.5 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    1846 3.3   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1139 3.3   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     881 3.3   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  881   20.5 1510 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     258 3.3   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  258   20.5 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.     945 3.3   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.     945 3.3   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.     945 3.3   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.     945 3.3   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1787 3.3   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1271 3.3   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        80       2.0 1271   20.5 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     427 3.3   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        72       2.0  427   20.5 1117 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      89 3.3   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        73       2.0   89   20.5  210 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1669 3.3   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1144 3.3   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1049 3.3   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1049   20.5 1451 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      95 3.3   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        73       2.0   95   20.5  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1304 3.3   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4NBAM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 No Build AM                      33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     727 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     727 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     727 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     582 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  582   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      63 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   63   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     925 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1616 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1242 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
      120         68       2.0 1242   04.1 1565 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     374 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
      120        110       2.0  374   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1503 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1503 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1503 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1503 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1534 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1111 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
      120         76       2.0 1111   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     324 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
      120         68       2.0  324   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
      120         69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1248 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2181 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2162 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
      120         80       2.0 2162   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
      120         78       2.0   19   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2382 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4NBPM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 No Build PM                      33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1848 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1848 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1848 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1625 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
       120        70       2.0 1625   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      57 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
       120        63       2.0   57   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     166 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
       120       110       2.0  166   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2075 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1213 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     763 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  763   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     450 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  450   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1281 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1281 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1281 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1281 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2649 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1806 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1806   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     438 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  438   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     405 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        68       2.0  405   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1973 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1517 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1505 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1505   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1898 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M1AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 MOS 1 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     754 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     754 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     754 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     612 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  612   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      59 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   59   04.1 1324 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      83 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   83   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     960 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1591 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1229 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1229   04.1 1572 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     362 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  362   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1513 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1513 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1513 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1513 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1534 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1144 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76       2.0 1144   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     329 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68       2.0  329   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        70       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1259 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2228 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2209 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        79       2.0 2209   04.1 1477 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   19   04.1  167 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2413 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M1PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 MOS 1 PM                          33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1828 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1828 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1828 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1618 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
      120         70       2.0 1618   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      53 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
      120         63       2.0   53   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     157 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
      120        110       2.0  157   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2103 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1235 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     771 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  771   04.1 1547 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     464 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  464   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1222 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1222 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1222 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1222 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2714 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1849 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1849   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     473 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  473   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     392 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        68       2.0  392   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    2063 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1532 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1520 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1520   04.1 1467 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1921 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M2AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 MOS 2 AM                          33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     742 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     742 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     742 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     594 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  594   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      66 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   66   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     936 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1619 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1269 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.       0.  24   2
       120        68       2.0 1269   04.1 1565 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     350 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.       0.  24   2
       120       110       2.0  350   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1530 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1530 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1530 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1530 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1551 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1129 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.       0.  24   2
       120        76       2.0 1129   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     323 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.       0.  12   1
       120        68       2.0  323   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.       0.  12   1
       120        69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1265 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2176 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2157 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.       0.  36   3
       120        80       2.0 2157   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.       0.  12   1
       120        78       2.0   19   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2357 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M2PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 MOS 2 PM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1835 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1835 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1835 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1599 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
      120         70       2.0 1599   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.     105 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
      120         63       2.0  105   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     131 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
      120        110       2.0  131   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2064 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1250 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     786 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  786   04.1 1548 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     464 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  464   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1248 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1248 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1248 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1248 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2679 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1820 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1820   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     453 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  453   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     406 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        68       2.0  406   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    2008 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1499 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1487 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1487   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1943 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B1AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 1 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     734 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     734 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     734 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     588 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  588   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      64 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   64   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     942 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1596 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1223 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1223   04.1 1573 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     373 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  373   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1508 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1508 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1508 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1508 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1570 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1137 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76       2.0 1137   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     334 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68       2.0  334   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1249 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2170 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2150 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 2150   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        78       2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2371 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B1PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 1 PM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1849 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1849 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1849 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1604 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
      120         70       2.0 1604   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      54 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
      120         63       2.0   54   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     191 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
      120        110       2.0  191   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2094 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1210 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     749 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  749   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     461 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  461   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1256 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1256 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1256 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1256 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2656 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1785 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1785   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     478 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  478   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     393 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0  393   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1977 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1537 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1525 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1525   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1925 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B2AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 2 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     740 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     740 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     740 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     581 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  581   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      76 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   76   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      83 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   83   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     935 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1595 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1225 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1225   04.1 1574 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     370 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  370   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1511 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1511 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1511 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1511 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1586 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1152 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76       2.0 1152   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     335 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68       2.0  335   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1263 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2128 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2109 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 2109   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        78       2.0   19   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2340 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B2PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 Build 2 PM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1802 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1802 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1802 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1617 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
      120         70       2.0 1617   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      58 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
      120         63       2.0   58   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     127 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
      120        110       2.0  127   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2068 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1211 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     760 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  760   04.1 1546 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     451 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  451   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1216 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1216 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1216 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1216 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2227 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1814 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1814   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     439 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  439   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     401 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0  401   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1998 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1536 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1524 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1524   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1921 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B3AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 Build 3 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     746 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     746 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     746 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     597 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
      120        69       2.0  597   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      67 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
      120        62       2.0   67   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
      120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     941 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1594 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1219 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
      120         68       2.0 1219   04.1 1564 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     375 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
      120        110       2.0  375   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1480 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1480 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1480 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1480 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1568 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1145 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
      120         76       2.0 1145   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     324 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
      120         68       2.0  324   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
      120         69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1282 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2151 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2131 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
      120         80       2.0 2131   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
      120         78       2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2356 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B3PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 3 PM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1841 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1841 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1841 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1599 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
      120         70       2.0 1599   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.     105 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
      120         63       2.0  105   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     137 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
      120        110       2.0  137   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2076 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1239 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     788 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  788   04.1 1548 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     451 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  451   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1241 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1241 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1241 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1241 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2670 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1806 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1806   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     465 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  465   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     399 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0  399   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    2000 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1517 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1505 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1505   04.1 1469 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1950 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B4AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 4 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     726 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     726 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     726 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     581 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  581   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      62 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   62   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      83 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   83   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     933 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1587 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1220 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
      120         68       2.0 1220   04.1 1573 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     367 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
      120        110       2.0  367   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1507 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1507 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1507 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1507 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1558 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1127 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
      120         76       2.0 1127   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     332 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
      120         68       2.0  332   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
      120         69       2.0   99   04.1   99 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1239 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2153 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2133 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
      120         80       2.0 2133   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
      120         78       2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2345 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B4PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 Build 4 PM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1853 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1853 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1853 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1610 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
      120         70       2.0 1610   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      54 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
      120         63       2.0   54   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     189 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
      120        110       2.0  189   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2090 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1239 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     781 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  781   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     458 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  458   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1288 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1288 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1288 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1288 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2624 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1767 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1767   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     468 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  468   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     389 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0  389   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1957 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1510 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1498 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1498   04.1 1465 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1891 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B5AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 5 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     740 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     740 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     740 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     594 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
      120        69       2.0  594   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      64 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
      120        62       2.0   64   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
      120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     933 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1594 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1240 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.       0.  24   2
       120        68       2.0 1240   04.1 1574 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     354 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.       0.  24   2
       120       110       2.0  354   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1527 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1527 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1527 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1527 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1552 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1134 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.       0.  24   2
       120        76       2.0 1134   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     319 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.       0.  12   1
       120        68       2.0  319   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.       0.  12   1
       120        69       2.0   99   04.1   99 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1245 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2130 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2110 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.       0.  36   3
       120        80       2.0 2110   04.1 1475 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.       0.  12   1
       120        78       2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2311 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B5PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 5 PM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1813 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1813 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1813 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1594 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
      120         70       2.0 1594   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      55 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
      120         63       2.0   55   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     164 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
      120        110       2.0  164   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2070 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1216 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     760 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  760   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     456 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  456   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1265 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1265 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1265 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1265 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2653 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1811 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        77       2.0 1811   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     448 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        69       2.0  448   04.1 1114 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     394 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        70       2.0  394   04.1  156 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1976 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1544 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1516 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1516   04.1 1469 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      28 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        76       2.0   28   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1915 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

Site 4 – Beverly & La Cienega
Output Files

JOB: Site 4 Bev & La Cien (S4EXAM.DAT) RUN: Site 4 Existing AM
DATE: 03/19/2010 TIME: 15:03:19.87

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	699.	3.3	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	699.	3.3	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	699.	3.3	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	565.	3.3	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	247.6	641.0	106.	270.	AG	63.	100.0	.0	24.0	.45	5.4
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	53.	3.3	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	336.0	624.9	18.	270.	AG	28.	100.0	.0	12.0	.09	.9
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	81.	3.3	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	319.0	663.8	34.	270.	AG	103.	100.0	.0	24.0	.78	1.7
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	837.	3.3	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1325.	3.3	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1055.	3.3	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	707.4	690.1	212.	90.	AG	62.	100.0	.0	24.0	.85	10.8
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	270.	3.3	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	1236.6	670.1	738.	90.	AG	101.	100.0	.0	24.0	1.78	37.5
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1331.	3.3	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1331.	3.3	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1331.	3.3	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1331.	3.3	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1116.	3.3	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	815.	3.3	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	452.6	398.4	192.	178.	AG	72.	100.0	.0	24.0	.83	9.7
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	202.	3.3	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	467.3	512.6	78.	178.	AG	33.	100.0	.0	12.0	.40	4.0
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	3.3	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	441.7	103.6	485.	179.	AG	33.	100.0	.0	12.0	1.65	24.7
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	965.	3.3	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1513.	3.3	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1443.	3.3	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	397.0	1521.3	785.	360.	AG	110.	100.0	.0	36.0	1.11	39.9
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	70.	3.3	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	423.7	772.9	38.	360.	AG	34.	100.0	.0	12.0	.78	1.9
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1520.	3.3	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4EXAM.DAT) RUN: Site 4 Existing AM
DATE: 03/19/2010 TIME: 15:03:19.87

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	69	2.0	565	1584	20.50	1	3
7.	EB Bev RT Q	120	62	2.0	53	1325	20.50	1	3
9.	EB Bev LT Q	120	112	2.0	81	1536	20.50	1	3
13.	WB Bev T+R Q	120	68	2.0	1055	1556	20.50	1	3
15.	WB Bev LT Q	120	110	2.0	270	1536	20.50	1	3
22.	NB Cin THR Q	120	79	2.0	815	1584	20.50	1	3
24.	NB Cin RT Q	120	71	2.0	202	1353	20.50	1	3
26.	NB Cin LT Q	120	72	2.0	99	165	20.50	1	3
30.	SB Cin T+R Q	120	80	2.0	1443	1448	20.50	1	3
32.	SB Cin LT Q	120	75	2.0	70	264	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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JOB: Site 4 Bev & La Cien (S4EXAM.DAT) RUN: Site 4 Existing AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.2	.1	.2	.5	.5	.5	.4	.0	.0	.0	.2	.2	.3	.3	.5	.5	.5	.3	.1	.0
5.	.0	.1	.1	.4	.5	.5	.4	.0	.0	.0	.2	.2	.2	.2	.6	.5	.5	.4	.1	.0
10.	.0	.0	.1	.4	.5	.4	.4	.0	.0	.0	.1	.1	.1	.0	.8	.7	.8	.6	.1	.1
15.	.0	.1	.1	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.8	.7	.7	.7	.1	.1
20.	.0	.1	.1	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.8	.7	.7	.1	.1
25.	.0	.1	.1	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.6	.3	.1
30.	.0	.1	.2	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.6	.3	.1
35.	.1	.1	.2	.5	.5	.5	.4	.0	.0	.0	.0	.0	.0	.0	.7	.6	.6	.6	.3	.1
40.	.1	.1	.1	.5	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.6	.6	.6	.2	.1
45.	.1	.1	.1	.5	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.6	.6	.6	.2	.1
50.	.0	.1	.1	.5	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
55.	.0	.1	.1	.5	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
60.	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
65.	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
70.	.0	.1	.1	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
75.	.0	.0	.1	.4	.4	.4	.4	.1	.1	.0	.0	.0	.0	.0	.5	.5	.5	.3	.2	.1
80.	.0	.0	.1	.4	.4	.4	.4	.2	.2	.2	.1	.0	.0	.0	.5	.5	.5	.3	.2	.1
85.	.0	.0	.1	.2	.4	.3	.3	.2	.2	.4	.3	.0	.0	.0	.6	.5	.5	.4	.3	.2
90.	.0	.0	.0	.2	.2	.2	.2	.3	.3	.4	.4	.0	.0	.0	.6	.5	.5	.5	.3	.2
95.	.0	.0	.0	.1	.2	.2	.2	.4	.5	.5	.5	.1	.0	.0	.6	.5	.6	.5	.3	.2
100.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.7	.7	.1	.0	.0	.5	.5	.6	.5	.3	.2
105.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.7	.6	.1	.0	.0	.5	.6	.6	.7	.3	.3
110.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.7	.6	.1	.1	.0	.5	.6	.6	.5	.2	.2
115.	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.6	.1	.1	.0	.5	.6	.6	.5	.1	.2
120.	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.6	.2	.1	.0	.7	.6	.6	.3	.1	.3
125.	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.5	.2	.1	.1	.7	.6	.6	.2	.2	.3
130.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.5	.2	.1	.1	.8	.7	.6	.2	.3	.2
135.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.5	.2	.1	.1	.8	.7	.7	.2	.3	.3
140.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.3	.2	.1	.1	.8	.7	.5	.3	.3	.3
145.	.0	.0	.0	.0	.0	.0	.0	.4	.6	.5	.3	.2	.1	.1	.7	.6	.4	.3	.4	.3
150.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.5	.3	.2	.1	.1	.7	.6	.4	.3	.4	.2
155.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.5	.2	.2	.1	.0	.7	.5	.4	.4	.4	.2
160.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.5	.2	.1	.1	.0	.7	.5	.3	.4	.3	.1
165.	.1	.0	.0	.0	.0	.0	.0	.4	.6	.5	.1	.1	.0	.0	.7	.5	.3	.4	.3	.1
170.	.1	.0	.0	.0	.0	.0	.0	.4	.5	.5	.1	.0	.0	.0	.5	.5	.4	.3	.3	.1
175.	.1	.1	.0	.0	.0	.0	.0	.3	.5	.5	.3	.1	.1	.1	.6	.3	.3	.2	.2	.1
180.	.3	.2	.1	.2	.0	.0	.0	.3	.5	.5	.4	.2	.2	.1	.4	.3	.3	.2	.2	.1
185.	.3	.2	.3	.3	.0	.0	.0	.4	.5	.5	.4	.2	.2	.2	.3	.3	.3	.3	.2	.1
190.	.3	.3	.3	.3	.0	.0	.0	.4	.5	.6	.5	.2	.2	.3	.2	.0	.1	.3	.2	.1
195.	.3	.2	.4	.3	.1	.0	.0	.4	.5	.6	.5	.2	.4	.3	.2	.0	.1	.3	.2	.1
200.	.3	.2	.4	.4	.1	.0	.0	.4	.5	.6	.4	.2	.3	.4	.0	.0	.1	.3	.2	.1
205.	.3	.4	.5	.6	.1	.0	.0	.4	.5	.7	.3	.3	.3	.4	.0	.0	.1	.3	.1	.1

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JOB: Site 4 Bev & La Cien (S4EXAM.DAT) RUN: Site 4 Existing AM

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.2	.4	.5	.5	.2	.0	.0	.4	.5	.7	.3	.2	.3	.4	.0	.0	.1	.3	.1	.1
215.	.2	.4	.5	.5	.2	.0	.0	.4	.6	.6	.3	.3	.4	.4	.0	.0	.1	.3	.1	.1
220.	.2	.3	.5	.4	.2	.0	.0	.4	.6	.5	.4	.4	.4	.4	.0	.0	.1	.3	.1	.1
225.	.2	.3	.4	.4	.2	.0	.0	.5	.6	.5	.4	.4	.4	.4	.0	.0	.1	.3	.1	.1
230.	.2	.3	.4	.3	.2	.0	.0	.5	.6	.5	.4	.4	.4	.4	.0	.0	.1	.2	.1	.1
235.	.2	.3	.5	.3	.2	.0	.0	.5	.6	.4	.4	.4	.4	.4	.0	.0	.1	.1	.2	.1
240.	.2	.3	.5	.3	.2	.0	.0	.6	.6	.3	.4	.4	.4	.4	.0	.0	.1	.1	.2	.1
245.	.2	.4	.5	.3	.2	.0	.0	.5	.6	.2	.3	.5	.4	.4	.0	.0	.0	.1	.2	.1
250.	.2	.4	.5	.3	.2	.0	.0	.6	.5	.3	.3	.5	.4	.4	.0	.0	.0	.1	.2	.1
255.	.2	.4	.5	.3	.1	.0	.0	.5	.5	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
260.	.2	.4	.5	.2	.1	.0	.0	.4	.3	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
265.	.2	.4	.5	.2	.1	.0	.1	.4	.3	.2	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
270.	.2	.4	.5	.2	.0	.1	.2	.4	.2	.2	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
275.	.1	.4	.5	.2	.1	.1	.2	.2	.2	.3	.4	.4	.4	.4	.0	.0	.0	.1	.1	.0
280.	.1	.4	.5	.2	.2	.2	.2	.1	.2	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
285.	.2	.4	.5	.3	.2	.2	.4	.0	.1	.2	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0
290.	.2	.4	.5	.3	.2	.2	.4	.1	.1	.2	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0
295.	.2	.4	.5	.4	.2	.2	.4	.1	.1	.2	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0
300.	.2	.4	.5	.4	.2	.5	.4	.1	.1	.2	.3	.4	.4	.3	.0	.0	.0	.0	.0	.0
305.	.2	.4	.4	.3	.2	.6	.5	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
310.	.2	.4	.4	.3	.4	.6	.5	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
315.	.2	.4	.4	.3	.5	.6	.6	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
320.	.2	.4	.4	.3	.6	.6	.5	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
325.	.3	.4	.4	.4	.6	.6	.5	.1	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
330.	.4	.4	.5	.4	.6	.6	.5	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
335.	.3	.5	.5	.4	.6	.6	.4	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
340.	.3	.4	.4	.5	.6	.6	.4	.0	.1	.1	.4	.4	.5	.4	.1	.0	.0	.0	.0	.0
345.	.4	.3	.4	.5	.6	.6	.4	.0	.1	.1	.4	.4	.4	.4	.1	.1	.1	.1	.0	.0
350.	.4	.3	.3	.5	.6	.5	.4	.0	.0	.1	.4	.4	.4	.4	.3	.1	.2	.1	.0	.0
355.	.3	.2	.2	.4	.6	.5	.4	.0	.0	.1	.3	.3	.3	.3	.3	.4	.3	.3	.0	.0
360.	.2	.1	.2	.5	.5	.5	.4	.0	.0	.0	.2	.2	.3	.3	.5	.5	.5	.3	.1	.0
MAX	.4	.5	.5	.6	.6	.6	.6	.6	.7	.7	.7	.5	.5	.4	.8	.8	.8	.7	.4	.3
DEGR.	330	335	205	205	320	305	315	240	115	205	100	245	340	200	10	20	10	15	145	105

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JOB: Site 4 Bev & La Cien (S4EXAM.DAT) RUN: Site 4 Existing AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.4	.5	.3	.3	.3
5.	.0	.1	.2	.4	.4	.4	.3	.3
10.	.0	.1	.3	.4	.5	.5	.3	.4
15.	.0	.1	.3	.4	.5	.5	.3	.3
20.	.0	.1	.3	.5	.5	.3	.3	.3
25.	.0	.3	.3	.6	.5	.2	.3	.5
30.	.1	.3	.3	.6	.5	.2	.3	.5
35.	.1	.3	.3	.6	.3	.2	.3	.5
40.	.1	.3	.4	.6	.2	.2	.4	.5
45.	.1	.3	.4	.6	.1	.3	.5	.4
50.	.1	.2	.4	.5	.1	.4	.4	.3
55.	.1	.2	.4	.4	.2	.4	.4	.2
60.	.1	.1	.3	.2	.3	.3	.4	.2
65.	.1	.1	.3	.3	.4	.3	.3	.1
70.	.1	.1	.3	.3	.4	.3	.3	.1
75.	.1	.1	.3	.2	.3	.3	.2	.1
80.	.1	.1	.2	.3	.3	.4	.3	.2
85.	.1	.1	.2	.3	.3	.4	.3	.2
90.	.2	.1	.1	.2	.3	.3	.3	.2
95.	.2	.0	.1	.2	.2	.3	.3	.2
100.	.2	.0	.0	.1	.1	.2	.2	.2
105.	.2	.0	.0	.1	.2	.2	.2	.1
110.	.2	.0	.0	.2	.2	.2	.2	.2
115.	.1	.0	.0	.2	.2	.2	.3	.3
120.	.1	.0	.0	.2	.2	.3	.3	.3
125.	.1	.0	.0	.2	.2	.3	.2	.3
130.	.1	.0	.1	.2	.2	.3	.2	.3
135.	.1	.0	.1	.1	.2	.3	.2	.3
140.	.1	.0	.1	.1	.3	.3	.3	.3
145.	.1	.0	.1	.1	.3	.4	.3	.3
150.	.2	.0	.1	.1	.3	.4	.3	.3
155.	.2	.0	.1	.1	.3	.3	.3	.3
160.	.2	.0	.0	.1	.2	.2	.3	.3
165.	.1	.0	.0	.1	.2	.2	.3	.3
170.	.1	.0	.0	.1	.2	.2	.3	.3
175.	.1	.0	.0	.0	.1	.2	.2	.2
180.	.1	.0	.0	.0	.1	.2	.2	.2
185.	.1	.0	.0	.0	.1	.1	.1	.1
190.	.1	.0	.0	.0	.0	.1	.1	.1
195.	.1	.0	.0	.0	.0	.1	.1	.1
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0
250.	.1	.0	.0	.0	.0	.0	.0	.0
255.	.1	.0	.0	.0	.0	.0	.0	.0
260.	.1	.0	.0	.0	.0	.0	.0	.0
265.	.2	.0	.0	.0	.0	.0	.0	.0
270.	.2	.0	.0	.0	.0	.0	.0	.0
275.	.2	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.1	.0	.0	.0
285.	.0	.0	.0	.1	.1	.0	.0	.0
290.	.0	.0	.0	.1	.3	.0	.0	.0
295.	.0	.0	.0	.2	.3	.0	.0	.0
300.	.0	.0	.0	.3	.3	.0	.0	.0
305.	.0	.1	.2	.3	.3	.0	.0	.0
310.	.0	.1	.2	.3	.3	.0	.0	.0
315.	.0	.1	.2	.3	.3	.0	.0	.0
320.	.0	.2	.2	.3	.4	.0	.0	.0
325.	.0	.2	.2	.3	.4	.1	.0	.0
330.	.0	.2	.2	.3	.3	.1	.0	.0
335.	.0	.2	.2	.3	.3	.1	.0	.0
340.	.0	.2	.1	.3	.3	.0	.0	.1
345.	.0	.2	.1	.3	.3	.1	.1	.1
350.	.0	.2	.2	.3	.4	.2	.2	.1
355.	.0	.2	.2	.3	.5	.3	.2	.2
360.	.0	.2	.2	.4	.5	.3	.3	.3
MAX	.2	.3	.4	.6	.5	.5	.5	.5
DEGR.	90	25	40	25	0	10	45	25

THE HIGHEST CONCENTRATION IS .80 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 20 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .80 PPM AT 10 DEGREES FROM REC17.

JOB: Site 4 Bev & La Cien (S4EXPM.DAT) RUN: Site 4 Existing PM
DATE: 03/19/2010 TIME: 15:14:27.10

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1694.	3.3	.0	44.0		
2. EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1694.	3.3	.0	44.0		
3. EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1694.	3.3	.0	44.0		
4. EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1324.	3.3	.0	44.0		
5. EB Bev THR Q	354.0	641.0	-571.4	641.0	925.	270.	AG	64.	100.0	.0	24.0	1.09	47.0
6. EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	104.	3.3	.0	32.0		
7. EB Bev RT Q	354.0	625.0	318.2	624.8	36.	270.	AG	29.	100.0	.0	12.0	.23	1.8
8. EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	266.	3.3	.0	44.0		
9. EB Bev LT Q	353.0	664.0	-362.6	660.7	716.	270.	AG	101.	100.0	.0	24.0	1.75	36.4
10. EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	1846.	3.3	.0	44.0		
11. WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1139.	3.3	.0	44.0		
12. WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	881.	3.3	.0	44.0		
13. WB Bev T+R Q	495.0	689.0	663.4	689.9	168.	90.	AG	64.	100.0	.0	24.0	.76	8.6
14. WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	258.	3.3	.0	44.0		
15. WB Bev LT Q	499.0	666.0	1170.6	669.7	672.	90.	AG	101.	100.0	.0	24.0	1.70	34.1
16. WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	945.	3.3	.0	44.0		
17. WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	945.	3.3	.0	44.0		
18. WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	945.	3.3	.0	44.0		
19. WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	945.	3.3	.0	44.0		
20. NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1787.	3.3	.0	56.0		
21. NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1271.	3.3	.0	44.0		
22. NB Cin THR Q	447.0	590.0	504.8	-1403.4	1994.	178.	AG	73.	100.0	.0	24.0	1.34	101.3
23. NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	427.	3.3	.0	32.0		
24. NB Cin RT Q	465.0	591.0	478.3	143.1	448.	178.	AG	33.	100.0	.0	12.0	1.04	22.8
25. NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	89.	3.3	.0	32.0		
26. NB Cin LT Q	431.0	589.0	435.9	365.4	224.	179.	AG	33.	100.0	.0	12.0	1.19	11.4
27. NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1669.	3.3	.0	44.0		
28. SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1144.	3.3	.0	44.0		
29. SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1049.	3.3	.0	56.0		
30. SB Cin T+R Q	403.0	736.0	401.8	898.7	163.	360.	AG	110.	100.0	.0	36.0	.80	8.3
31. SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	95.	3.3	.0	32.0		
32. SB Cin LT Q	424.0	735.0	420.5	1177.5	443.	360.	AG	33.	100.0	.0	12.0	1.58	22.5
33. SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1304.	3.3	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4EXPM.DAT) RUN: Site 4 Existing PM
DATE: 03/19/2010 TIME: 15:14:27.10

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5. EB Bev THR Q	120	70	2.0	1324	1584	20.50	1	3
7. EB Bev RT Q	120	63	2.0	104	1048	20.50	1	3
9. EB Bev LT Q	120	110	2.0	266	1536	20.50	1	3
13. WB Bev T+R Q	120	70	2.0	881	1510	20.50	1	3
15. WB Bev LT Q	120	110	2.0	258	1536	20.50	1	3
22. NB Cin THR Q	120	80	2.0	1271	1584	20.50	1	3
24. NB Cin RT Q	120	72	2.0	427	1117	20.50	1	3
26. NB Cin LT Q	120	73	2.0	89	210	20.50	1	3
30. SB Cin T+R Q	120	80	2.0	1049	1451	20.50	1	3
32. SB Cin LT Q	120	73	2.0	95	168	20.50	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. SE MID S	492.0	301.0	5.0
2. SE 164 S	488.0	448.0	5.0
3. SE 82 S	486.0	530.0	5.0
4. SE CNR	491.0	605.0	5.0
5. SE 82 E	564.0	612.0	5.0
6. SE 164 E	646.0	612.0	5.0
7. SE MID E	775.0	615.0	5.0
8. NE MID E	767.0	715.0	5.0
9. NE 164 E	637.0	714.0	5.0
10. NE 82 E	555.0	714.0	5.0
11. NE CNR	474.0	717.0	5.0
12. NE 82 N	473.0	796.0	5.0
13. NE 164 N	472.0	877.0	5.0
14. NE MID N	474.0	999.0	5.0
15. NW MID N	372.0	996.0	5.0
16. NW 164 N	367.0	884.0	5.0
17. NW 82 N	367.0	803.0	5.0
18. NW CNR	365.0	726.0	5.0
19. NW 82 W	287.0	721.0	5.0
20. NW 164 W	206.0	720.0	5.0
21. NW MID W	62.0	720.0	5.0
22. SW MID W	56.0	606.0	5.0
23. SW 164 W	209.0	606.0	5.0
24. SW 82 W	289.0	606.0	5.0
25. SW CNR	361.0	601.0	5.0
26. SW 82 S	376.0	526.0	5.0
27. SW 164 S	380.0	445.0	5.0
28. SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.4	.2	.2	.4	.5	.5	.5	.0	.0	.0	.2	.2	.2	.1	.2	.3	.3	.3	.0	.0
5.	.2	.2	.2	.4	.5	.5	.5	.0	.0	.0	.1	.1	.1	.1	.3	.3	.3	.4	.0	.0
10.	.0	.1	.2	.4	.5	.4	.5	.0	.0	.0	.1	.1	.1	.1	.3	.3	.3	.4	.0	.0
15.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.1	.1	.1	.0	.3	.3	.4	.4	.1	.0
20.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.4	.6	.1	.0
25.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.5	.6	.1	.0
30.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.6	.6	.2	.0
35.	.1	.2	.2	.5	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.4	.3	.6	.5	.2	.0
40.	.1	.2	.2	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.4	.2	.5	.5	.2	.0
45.	.0	.2	.2	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.3	.3	.5	.5	.2	.0
50.	.0	.2	.2	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.5	.4	.2	.1
55.	.0	.2	.2	.5	.4	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.5	.4	.2	.1
60.	.0	.2	.2	.5	.4	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.5	.4	.2	.1
65.	.0	.2	.2	.4	.6	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.5	.4	.2	.1
70.	.0	.2	.2	.4	.6	.6	.6	.0	.0	.0	.0	.0	.0	.0	.2	.4	.5	.4	.2	.1
75.	.0	.0	.2	.4	.6	.6	.6	.1	.0	.0	.0	.0	.0	.0	.2	.4	.5	.3	.2	.1
80.	.0	.0	.2	.4	.6	.5	.5	.1	.2	.1	.1	.0	.0	.0	.2	.4	.5	.3	.2	.1
85.	.0	.0	.1	.3	.5	.4	.4	.2	.3	.5	.4	.0	.0	.0	.2	.4	.5	.4	.3	.1
90.	.0	.0	.0	.3	.3	.3	.3	.3	.3	.5	.4	.0	.0	.0	.2	.5	.5	.5	.3	.3
95.	.0	.0	.0	.2	.2	.2	.2	.5	.5	.6	.5	.1	.0	.0	.2	.5	.6	.5	.4	.3
100.	.0	.0	.0	.1	.1	.1	.1	.5	.5	.6	.5	.2	.0	.0	.2	.5	.7	.6	.3	.4
105.	.0	.0	.0	.0	.1	.1	.1	.5	.5	.7	.6	.2	.0	.0	.2	.5	.7	.6	.3	.4
110.	.0	.0	.0	.0	.0	.0	.0	.5	.5	.6	.6	.2	.1	.0	.2	.6	.7	.5	.3	.3
115.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.6	.2	.2	.0	.2	.7	.7	.5	.2	.3
120.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.6	.2	.2	.0	.2	.7	.7	.5	.3	.4
125.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.5	.3	.2	.0	.3	.7	.7	.4	.3	.5
130.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.5	.3	.2	.1	.4	.7	.7	.4	.3	.5
135.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.5	.3	.2	.1	.4	.6	.7	.3	.4	.5
140.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.4	.3	.1	.1	.4	.6	.6	.4	.5	.6
145.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.4	.3	.1	.1	.3	.5	.5	.5	.6	.6
150.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.4	.3	.1	.1	.4	.5	.4	.5	.6	.6
155.	.0	.0	.0	.0	.0	.0	.0	.4	.6	.6	.3	.3	.1	.0	.5	.5	.5	.5	.7	.6
160.	.1	.0	.0	.0	.0	.0	.0	.4	.6	.6	.3	.2	.1	.0	.4	.6	.4	.6	.7	.6
165.	.2	.1	.1	.0	.0	.0	.0	.4	.6	.6	.3	.2	.0	.0	.4	.5	.4	.5	.7	.6
170.	.2	.2	.1	.1	.0	.0	.0	.4	.6	.6	.4	.2	.2	.1	.5	.5	.4	.4	.7	.5
175.	.3	.3	.3	.1	.0	.0	.0	.4	.6	.6	.4	.3	.2	.2	.4	.4	.3	.4	.6	.5
180.	.5	.6	.7	.6	.1	.0	.0	.4	.6	.7	.6	.5	.3	.2	.3	.4	.3	.4	.5	.5
185.	.7	.7	.7	.6	.1	.0	.0	.4	.7	.7	.6	.5	.4	.4	.2	.2	.2	.5	.5	.5
190.	.7	.7	.7	.6	.2	.1	.0	.4	.7	.7	.6	.5	.4	.3	.2	.0	.1	.3	.5	.5
195.	.7	.7	.6	.6	.1	.1	.0	.4	.7	.8	.6	.4	.4	.4	.0	.1	.1	.4	.5	.5
200.	.7	.7	.6	.6	.2	.1	.0	.4	.7	.8	.6	.3	.4	.4	.0	.1	.1	.4	.5	.5
205.	.6	.6	.6	.6	.2	.1	.0	.4	.7	.9	.5	.3	.4	.5	.1	.1	.1	.4	.5	.5

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.6	.6	.6	.6	.2	.1	.0	.4	.7	.9	.6	.2	.4	.5	.1	.1	.2	.4	.5	.5
215.	.6	.6	.6	.6	.3	.1	.0	.4	.7	.9	.5	.3	.5	.5	.1	.1	.2	.5	.5	.5
220.	.6	.6	.6	.5	.3	.1	.0	.4	.7	.7	.4	.4	.6	.6	.1	.1	.2	.5	.5	.5
225.	.6	.6	.6	.4	.3	.1	.0	.4	.6	.5	.5	.5	.6	.6	.1	.1	.2	.5	.5	.4
230.	.6	.6	.6	.4	.2	.1	.0	.4	.6	.5	.5	.6	.6	.4	.1	.1	.2	.5	.5	.5
235.	.6	.6	.6	.3	.2	.1	.0	.4	.6	.5	.6	.6	.6	.4	.1	.1	.2	.5	.5	.5
240.	.6	.5	.5	.3	.2	.1	.0	.4	.6	.5	.6	.6	.6	.3	.0	.1	.2	.5	.5	.5
245.	.5	.5	.5	.3	.2	.0	.0	.4	.6	.4	.7	.7	.6	.3	.0	.1	.2	.5	.4	.5
250.	.5	.5	.5	.3	.2	.0	.0	.5	.5	.5	.7	.7	.6	.3	.0	.1	.2	.4	.4	.5
255.	.5	.5	.5	.3	.1	.0	.1	.5	.7	.6	.8	.7	.6	.3	.0	.0	.2	.4	.4	.5
260.	.5	.5	.5	.3	.1	.1	.1	.6	.6	.6	.7	.6	.5	.3	.0	.0	.1	.4	.4	.4
265.	.5	.5	.5	.5	.3	.2	.1	.6	.5	.6	.6	.6	.5	.3	.0	.0	.0	.3	.3	.3
270.	.6	.5	.5	.5	.3	.3	.4	.4	.3	.4	.6	.5	.5	.3	.0	.0	.0	.3	.3	.2
275.	.6	.5	.7	.5	.4	.4	.4	.0	.3	.3	.6	.5	.4	.3	.0	.0	.0	.1	.1	.1
280.	.6	.5	.7	.6	.5	.5	.4	.0	.1	.2	.5	.5	.4	.3	.0	.0	.0	.0	.0	.0
285.	.5	.6	.7	.6	.4	.4	.5	.0	.1	.2	.4	.5	.4	.3	.0	.0	.0	.0	.0	.0
290.	.5	.7	.7	.6	.3	.3	.5	.0	.1	.2	.4	.5	.4	.2	.0	.0	.0	.0	.0	.0
295.	.5	.7	.8	.6	.2	.3	.5	.0	.1	.2	.4	.5	.4	.2	.0	.0	.0	.0	.0	.0
300.	.5	.7	.8	.5	.4	.5	.5	.0	.2	.2	.4	.5	.3	.2	.0	.0	.0	.0	.0	.0
305.	.5	.8	.8	.3	.4	.5	.4	.0	.1	.2	.5	.5	.3	.2	.0	.0	.0	.0	.0	.0
310.	.6	.7	.7	.4	.5	.6	.4	.0	.1	.2	.5	.6	.4	.2	.0	.0	.0	.0	.0	.0
315.	.7	.7	.6	.4	.5	.7	.4	.0	.1	.2	.5	.6	.4	.3	.0	.0	.0	.0	.0	.0
320.	.6	.7	.5	.6	.6	.6	.5	.0	.1	.2	.6	.5	.4	.3	.0	.0	.0	.0	.0	.0
325.	.6	.6	.5	.5	.6	.6	.5	.0	.1	.1	.6	.5	.4	.3	.0	.0	.0	.0	.0	.0
330.	.6	.6	.4	.5	.7	.6	.5	.0	.1	.1	.6	.5	.4	.3	.0	.0	.0	.0	.0	.0
335.	.6	.6	.7	.5	.6	.6	.5	.0	.1	.1	.5	.5	.3	.3	.0	.0	.0	.0	.0	.0
340.	.6	.5	.7	.6	.6	.5	.5	.0	.0	.1	.6	.5	.3	.3	.0	.0	.0	.0	.0	.0
345.	.6	.5	.5	.5	.6	.5	.5	.0	.0	.1	.6	.4	.4	.3	.0	.0	.0	.0	.0	.0
350.	.4	.5	.5	.5	.6	.5	.5	.0	.0	.1	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
355.	.5	.5	.2	.3	.5	.5	.5	.0	.0	.1	.2	.2	.2	.3	.1	.0	.1	.2	.0	.0
360.	.4	.2	.2	.4	.5	.5	.5	.0	.0	.0	.2	.2	.2	.1	.2	.3	.3	.3	.0	.0
MAX	.7	.8	.8	.6	.7	.7	.6	.6	.7	.9	.8	.7	.6	.6	.5	.7	.7	.6	.7	.6
DEGR.	185	305	295	180	330	315	70	260	185	205	255	245	220	220	155	115	100	20	155	140

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.4	.4	.4	.5	.3	.2	.2
5.	.0	.4	.5	.4	.4	.4	.3	.3
10.	.0	.4	.5	.5	.4	.4	.3	.4
15.	.0	.4	.5	.7	.4	.3	.3	.4
20.	.0	.4	.5	.6	.4	.2	.5	.4
25.	.0	.4	.5	.6	.5	.3	.4	.4
30.	.0	.4	.5	.5	.5	.4	.4	.4
35.	.0	.4	.6	.5	.3	.4	.5	.4
40.	.0	.5	.7	.5	.3	.3	.6	.5
45.	.0	.6	.7	.5	.4	.4	.5	.5
50.	.0	.6	.7	.4	.4	.5	.5	.4
55.	.0	.6	.6	.4	.5	.5	.5	.3
60.	.0	.7	.4	.2	.4	.5	.5	.3
65.	.0	.7	.3	.4	.4	.5	.5	.3
70.	.0	.7	.4	.4	.4	.5	.5	.3
75.	.0	.5	.5	.3	.5	.5	.3	.3
80.	.0	.4	.5	.3	.5	.5	.3	.3
85.	.1	.5	.4	.4	.5	.5	.3	.3
90.	.3	.5	.3	.3	.4	.3	.3	.2
95.	.4	.2	.2	.3	.4	.3	.3	.3
100.	.4	.0	.0	.2	.4	.3	.3	.3
105.	.4	.0	.0	.1	.3	.3	.3	.3
110.	.5	.0	.0	.2	.3	.3	.3	.3
115.	.5	.0	.0	.2	.3	.3	.3	.3
120.	.5	.0	.0	.2	.3	.3	.3	.3
125.	.5	.0	.0	.2	.3	.3	.3	.3
130.	.5	.0	.1	.2	.3	.3	.3	.3
135.	.4	.0	.1	.2	.3	.4	.4	.4
140.	.5	.0	.1	.2	.3	.4	.4	.4
145.	.5	.0	.1	.2	.3	.4	.4	.4
150.	.5	.0	.1	.2	.3	.4	.5	.4
155.	.5	.0	.1	.2	.4	.4	.4	.4
160.	.5	.0	.1	.2	.4	.5	.4	.4
165.	.5	.0	.1	.2	.4	.4	.4	.4
170.	.5	.0	.0	.1	.3	.4	.4	.4
175.	.5	.0	.0	.1	.2	.4	.4	.4
180.	.5	.0	.0	.0	.2	.2	.4	.4
185.	.5	.0	.0	.0	.1	.2	.2	.2
190.	.5	.0	.0	.0	.0	.1	.1	.1
195.	.5	.0	.0	.0	.0	.0	.1	.1
200.	.5	.0	.0	.0	.0	.0	.0	.0
205.	.5	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.5	.0	.0	.0	.0	.0	.0	.0
215.	.5	.0	.0	.0	.0	.0	.0	.0
220.	.5	.0	.0	.0	.0	.0	.0	.0
225.	.5	.0	.0	.0	.0	.0	.0	.0
230.	.5	.0	.0	.0	.0	.0	.0	.0
235.	.5	.0	.0	.0	.0	.0	.0	.0
240.	.5	.0	.0	.0	.0	.0	.0	.0
245.	.5	.0	.0	.0	.0	.0	.0	.0
250.	.4	.0	.0	.0	.0	.0	.0	.0
255.	.5	.0	.0	.0	.0	.0	.0	.0
260.	.5	.1	.1	.1	.1	.0	.0	.0
265.	.3	.2	.2	.2	.2	.0	.0	.0
270.	.2	.2	.3	.3	.3	.0	.0	.0
275.	.1	.3	.4	.4	.3	.2	.0	.0
280.	.0	.4	.6	.5	.5	.2	.0	.0
285.	.0	.6	.6	.5	.5	.2	.0	.0
290.	.0	.6	.6	.5	.5	.2	.1	.0
295.	.0	.6	.6	.5	.5	.2	.2	.0
300.	.0	.6	.6	.5	.5	.2	.2	.0
305.	.0	.5	.5	.5	.6	.3	.2	.0
310.	.0	.5	.5	.6	.5	.3	.2	.1
315.	.0	.5	.5	.6	.5	.3	.2	.1
320.	.0	.5	.5	.6	.4	.3	.1	.1
325.	.0	.4	.4	.5	.4	.3	.1	.1
330.	.0	.4	.4	.4	.3	.3	.1	.0
335.	.0	.4	.4	.4	.3	.3	.1	.0
340.	.0	.4	.4	.4	.3	.2	.1	.0
345.	.0	.4	.5	.5	.3	.2	.1	.1
350.	.0	.4	.5	.5	.3	.2	.1	.1
355.	.0	.4	.4	.5	.4	.4	.1	.1
360.	.0	.4	.4	.4	.5	.3	.2	.2
MAX	.5	.7	.7	.7	.6	.5	.6	.5
DEGR.	110	60	40	15	305	50	40	40

THE HIGHEST CONCENTRATION IS .90 PPM AT 205 DEGREES FROM REC10.
THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 305 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .80 PPM AT 295 DEGREES FROM REC3 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 4 Bev & La Cien (S4NBAM.DAT) RUN: Site 4 No Build AM
DATE: 03/19/2010 TIME: 15:35:27.86

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	727.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	727.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	727.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	582.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	244.2	641.0	110.	270.	AG	13.	100.0	.0	24.0	.47	5.6
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	63.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	332.6	624.9	21.	270.	AG	6.	100.0	.0	12.0	.11	1.1
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	82.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	925.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1616.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1242.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	837.6	690.8	343.	90.	AG	12.	100.0	.0	24.0	.99	17.4
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	374.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	1808.8	673.3	1310.	90.	AG	20.	100.0	.0	24.0	2.46	66.5
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1503.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1503.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1503.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1503.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1534.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1111.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	465.1	-33.5	624.	178.	AG	14.	100.0	.0	24.0	1.05	31.7
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	324.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	468.6	470.6	120.	178.	AG	6.	100.0	.0	12.0	.60	6.1
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	441.6	105.3	484.	179.	AG	6.	100.0	.0	12.0	1.65	24.6
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1248.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2181.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2162.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	378.5	3953.7	3218.	360.	AG	22.	100.0	.0	36.0	1.63	163.5
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	19.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	423.9	743.1	8.	360.	AG	7.	100.0	.0	12.0	.35	.4
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2382.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4NBAM.DAT) RUN: Site 4 No Build AM
DATE: 03/19/2010 TIME: 15:35:27.86

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	69	2.0	582	1584	4.10	1	3
7.	EB Bev RT Q	120	62	2.0	63	1325	4.10	1	3
9.	EB Bev LT Q	120	112	2.0	82	1536	4.10	1	3
13.	WB Bev T+R Q	120	68	2.0	1242	1565	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	374	1536	4.10	1	3
22.	NB Cin THR Q	120	76	2.0	1111	1584	4.10	1	3
24.	NB Cin RT Q	120	68	2.0	324	1352	4.10	1	3
26.	NB Cin LT Q	120	69	2.0	99	155	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	2162	1476	4.10	1	3
32.	SB Cin LT Q	120	78	2.0	19	171	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	90	105	105	345	345	345	0	5	15	10	10	0	0

1

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.1	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.1	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX DEGR.	.0 0	.0 0	.0 0	.0 0	.1 120	.1 5	.1 0	.1 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 5 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

JOB: Site 4 Bev & La Cien (S4NBPM.DAT) RUN: Site 4 No Build PM
DATE: 03/19/2010 TIME: 15:47:05.53

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1848.	.8	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1848.	.8	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1848.	.8	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1625.	.8	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	-2134.8	641.0	2489.	270.	AG	13.	100.0	.0	24.0	1.34	126.4
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	57.	.8	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	334.4	624.9	20.	270.	AG	6.	100.0	.0	12.0	.12	1.0
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	166.	.8	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	187.6	663.2	165.	270.	AG	20.	100.0	.0	24.0	1.09	8.4
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	2075.	.8	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1213.	.8	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	763.	.8	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	640.8	689.8	146.	90.	AG	13.	100.0	.0	24.0	.63	7.4
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	450.	.8	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	2227.0	675.6	1728.	90.	AG	20.	100.0	.0	24.0	2.96	87.8
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1281.	.8	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1281.	.8	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1281.	.8	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1281.	.8	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	2649.	.8	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1806.	.8	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	566.4	-3530.3	4122.	178.	AG	14.	100.0	.0	24.0	1.67	209.4
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	438.	.8	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	472.0	357.3	234.	178.	AG	6.	100.0	.0	12.0	.96	11.9
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	405.	.8	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	514.3	-3200.7	3791.	179.	AG	6.	100.0	.0	12.0	6.64	192.6
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1973.	.8	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1517.	.8	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1505.	.8	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	395.9	1671.7	936.	360.	AG	22.	100.0	.0	36.0	1.14	47.5
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	12.	.8	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	424.0	740.1	5.	360.	AG	7.	100.0	.0	12.0	.22	.3
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1898.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4NBPM.DAT) RUN: Site 4 No Build PM
DATE: 03/19/2010 TIME: 15:47:05.53

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	70	2.0	1625	1584	4.10	1	3
7.	EB	Bev RT Q	120	63	2.0	57	1048	4.10	1	3
9.	EB	Bev LT Q	120	110	2.0	166	1536	4.10	1	3
13.	WB	Bev T+R Q	120	70	2.0	763	1583	4.10	1	3
15.	WB	Bev LT Q	120	110	2.0	450	1536	4.10	1	3
22.	NB	Cin THR Q	120	75	2.0	1806	1584	4.10	1	3
24.	NB	Cin RT Q	120	67	2.0	438	1113	4.10	1	3
26.	NB	Cin LT Q	120	68	2.0	405	153	4.10	1	3
30.	SB	Cin T+R Q	120	80	2.0	1505	1468	4.10	1	3
32.	SB	Cin LT Q	120	77	2.0	12	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	170	0	0	45	30	35	30	105	100	100	0	0	0	190	150	0	0	0	0	0

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REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.0	.1	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.0	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4NBPM.DAT) RUN: Site 4 No Build PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	150	15	5	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .10 PPM AT 170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 45 DEGREES FROM REC4 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

JOB: Site 4 Bev & La Cien (S4M1AM.DAT) RUN: Site 4 MOS 1 AM
DATE: 03/22/2010 TIME: 10:08:05.46

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	754.	.8	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	754.	.8	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	754.	.8	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	612.	.8	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	238.5	641.0	115.	270.	AG	13.	100.0	.0	24.0	.49	5.9
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	59.	.8	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	333.7	624.9	20.	270.	AG	6.	100.0	.0	12.0	.10	1.0
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	83.	.8	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	960.	.8	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1591.	.8	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1229.	.8	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	819.0	690.7	324.	90.	AG	12.	100.0	.0	24.0	.98	16.5
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	362.	.8	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	1742.8	672.9	1244.	90.	AG	20.	100.0	.0	24.0	2.38	63.2
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1513.	.8	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1513.	.8	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1513.	.8	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1513.	.8	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1534.	.8	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1144.	.8	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	470.2	-211.4	802.	178.	AG	14.	100.0	.0	24.0	1.09	40.7
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	329.	.8	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	468.6	468.7	122.	178.	AG	6.	100.0	.0	12.0	.61	6.2
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	441.9	94.4	495.	179.	AG	6.	100.0	.0	12.0	1.68	25.1
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1259.	.8	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2228.	.8	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2209.	.8	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	378.3	3987.4	3252.	360.	AG	22.	100.0	.0	36.0	1.62	165.2
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	19.	.8	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	423.9	743.0	8.	360.	AG	7.	100.0	.0	12.0	.35	.4
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2413.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4M1AM.DAT) RUN: Site 4 MOS 1 AM
DATE: 03/22/2010 TIME: 10:08:05.46

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	69	2.0	612	1584	4.10	1	3
7.	EB	Bev RT Q	120	63	2.0	59	1324	4.10	1	3
9.	EB	Bev LT Q	120	112	2.0	83	1536	4.10	1	3
13.	WB	Bev T+R Q	120	68	2.0	1229	1572	4.10	1	3
15.	WB	Bev LT Q	120	110	2.0	362	1536	4.10	1	3
22.	NB	Cin THR Q	120	76	2.0	1144	1584	4.10	1	3
24.	NB	Cin RT Q	120	68	2.0	329	1352	4.10	1	3
26.	NB	Cin LT Q	120	70	2.0	99	155	4.10	1	3
30.	SB	Cin T+R Q	120	79	2.0	2209	1477	4.10	1	3
32.	SB	Cin LT Q	120	77	2.0	19	167	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	95	105	105	0	0	345	0	5	15	10	10	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.1	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.1	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.1	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4M1AM.DAT) RUN: Site 4 MOS 1 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX DEGR.	.0 0	.0 0	.0 0	.0 0	.1 120	.1 5	.1 0	.1 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 5 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

JOB: Site 4 Bev & La Cien (S4M1PM.DAT) RUN: Site 4 MOS 1 PM
DATE: 03/19/2010 TIME: 16:22:52.29

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1828.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1828.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1828.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1618.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	-2103.5	641.0	2458.	270.	AG	13.	100.0	.0	24.0	1.33	124.8
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	53.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	335.7	624.9	18.	270.	AG	6.	100.0	.0	12.0	.11	.9
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	157.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	242.7	663.5	110.	270.	AG	20.	100.0	.0	24.0	1.03	5.6
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	2103.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1235.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	771.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	642.4	689.8	147.	90.	AG	13.	100.0	.0	24.0	.65	7.5
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	464.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	2304.0	676.0	1805.	90.	AG	20.	100.0	.0	24.0	3.05	91.7
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1222.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1222.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1222.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1222.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	2714.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1849.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	572.8	-3749.9	4342.	178.	AG	14.	100.0	.0	24.0	1.71	220.6
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	473.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	478.9	122.8	468.	178.	AG	6.	100.0	.0	12.0	1.04	23.8
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	392.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	511.2	-3059.8	3650.	179.	AG	6.	100.0	.0	12.0	6.43	185.4
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	2063.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1532.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1520.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	395.5	1724.3	988.	360.	AG	22.	100.0	.0	36.0	1.15	50.2
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	12.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	424.0	740.1	5.	360.	AG	7.	100.0	.0	12.0	.22	.3
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1921.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4M1PM.DAT) RUN: Site 4 MOS 1 PM
DATE: 03/19/2010 TIME: 16:22:52.29

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	70	2.0	1618	1584	4.10	1	3
7.	EB Bev RT Q	120	63	2.0	53	1048	4.10	1	3
9.	EB Bev LT Q	120	110	2.0	157	1536	4.10	1	3
13.	WB Bev T+R Q	120	70	2.0	771	1547	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	464	1536	4.10	1	3
22.	NB Cin THR Q	120	75	2.0	1849	1584	4.10	1	3
24.	NB Cin RT Q	120	67	2.0	473	1113	4.10	1	3
26.	NB Cin LT Q	120	68	2.0	392	153	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	1520	1467	4.10	1	3
32.	SB Cin LT Q	120	77	2.0	12	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.1	.0	.0	.0	.1	.0	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	170	0	0	45	0	35	30	105	100	100	0	0	0	190	150	0	0	0	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.0	.1	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.1	.1
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.0	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4M1PM.DAT) RUN: Site 4 MOS 1 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	150	15	5	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .10 PPM AT 170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 45 DEGREES FROM REC4 .

JOB: Site 4 Bev & La Cien (S4M2AM.DAT) RUN: Site 4 MOS 2 AM
DATE: 03/22/2010 TIME: 10:09:25.71

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	742.	.8	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	742.	.8	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	742.	.8	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	594.	.8	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	241.9	641.0	112.	270.	AG	13.	100.0	.0	24.0	.48	5.7
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	66.	.8	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	331.6	624.9	22.	270.	AG	6.	100.0	.0	12.0	.11	1.1
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	82.	.8	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	936.	.8	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1619.	.8	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1269.	.8	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	932.7	691.3	438.	90.	AG	12.	100.0	.0	24.0	1.01	22.2
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	350.	.8	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	1676.8	672.5	1178.	90.	AG	20.	100.0	.0	24.0	2.30	59.8
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1530.	.8	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1530.	.8	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1530.	.8	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1530.	.8	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1551.	.8	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1129.	.8	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	467.8	-127.7	718.	178.	AG	14.	100.0	.0	24.0	1.07	36.5
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	323.	.8	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	468.6	471.0	120.	178.	AG	6.	100.0	.0	12.0	.60	6.1
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	441.6	105.3	484.	179.	AG	6.	100.0	.0	12.0	1.65	24.6
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1265.	.8	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2176.	.8	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2157.	.8	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	378.6	3943.2	3207.	360.	AG	22.	100.0	.0	36.0	1.63	162.9
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	19.	.8	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	423.9	743.1	8.	360.	AG	7.	100.0	.0	12.0	.35	.4
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2357.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4M2AM.DAT) RUN: Site 4 MOS 2 AM
DATE: 03/22/2010 TIME: 10:09:25.71

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	69	2.0	594	1584	4.10	1	3
7.	EB	Bev RT Q	120	62	2.0	66	1325	4.10	1	3
9.	EB	Bev LT Q	120	112	2.0	82	1536	4.10	1	3
13.	WB	Bev T+R Q	120	68	2.0	1269	1565	4.10	1	3
15.	WB	Bev LT Q	120	110	2.0	350	1536	4.10	1	3
22.	NB	Cin THR Q	120	76	2.0	1129	1584	4.10	1	3
24.	NB	Cin RT Q	120	68	2.0	323	1352	4.10	1	3
26.	NB	Cin LT Q	120	69	2.0	99	155	4.10	1	3
30.	SB	Cin T+R Q	120	80	2.0	2157	1476	4.10	1	3
32.	SB	Cin LT Q	120	78	2.0	19	171	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	90	105	105	345	345	345	0	5	15	10	10	0	0

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.1	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX DEGR.	.0 0	.0 0	.0 0	.0 0	.1 125	.1 5	.1 0	.1 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 5 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

JOB: Site 4 Bev & La Cien (S4M2PM.DAT) RUN: Site 4 MOS 2 PM
DATE: 03/22/2010 TIME: 10:32:21.70

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1835.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1835.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1835.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1599.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	-1999.3	641.0	2353.	270.	AG	13.	100.0	.0	24.0	1.32	119.5
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	105.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	317.8	624.8	36.	270.	AG	6.	100.0	.0	12.0	.23	1.8
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	131.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	296.6	663.7	56.	270.	AG	20.	100.0	.0	24.0	.86	2.9
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	2064.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1250.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	786.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	645.4	689.8	150.	90.	AG	13.	100.0	.0	24.0	.66	7.6
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	464.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	2304.0	676.0	1805.	90.	AG	20.	100.0	.0	24.0	3.05	91.7
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1248.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1248.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1248.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1248.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	2679.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1820.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	568.6	-3603.5	4195.	178.	AG	14.	100.0	.0	24.0	1.68	213.1
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	453.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	473.0	323.5	268.	178.	AG	6.	100.0	.0	12.0	1.00	13.6
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	406.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	514.5	-3211.5	3801.	179.	AG	6.	100.0	.0	12.0	6.66	193.1
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	2008.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1499.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1487.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	396.4	1608.6	873.	360.	AG	22.	100.0	.0	36.0	1.13	44.3
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	12.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	424.0	740.1	5.	360.	AG	7.	100.0	.0	12.0	.22	.3
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1943.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4M2PM.DAT) RUN: Site 4 MOS 2 PM
DATE: 03/22/2010 TIME: 10:32:21.70

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	70	2.0	1599	1584	4.10	1	3
7.	EB Bev RT Q	120	63	2.0	105	1048	4.10	1	3
9.	EB Bev LT Q	120	110	2.0	131	1536	4.10	1	3
13.	WB Bev T+R Q	120	70	2.0	786	1548	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	464	1536	4.10	1	3
22.	NB Cin THR Q	120	75	2.0	1820	1584	4.10	1	3
24.	NB Cin RT Q	120	67	2.0	453	1113	4.10	1	3
26.	NB Cin LT Q	120	68	2.0	406	153	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	1487	1468	4.10	1	3
32.	SB Cin LT Q	120	77	2.0	12	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.0	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.2	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	170	0	0	45	35	35	35	105	100	100	0	0	0	190	150	0	0	0	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.1
90.	.0	.0	.0	.0	.0	.0	.0	.1
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4M2PM.DAT) RUN: Site 4 MOS 2 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	150	15	5	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 105 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 170 DEGREES FROM REC1 .

JOB: Site 4 Bev & La Cien (S4B1AM.DAT) RUN: Site 4 Build 1 AM
DATE: 03/22/2010 TIME: 10:43:00.54

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	734.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	734.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	734.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	588.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	243.1	641.0	111.	270.	AG	13.	100.0	.0	24.0	.47	5.6
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	64.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	332.3	624.9	22.	270.	AG	6.	100.0	.0	12.0	.11	1.1
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	82.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	942.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1596.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1223.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	811.4	690.7	316.	90.	AG	12.	100.0	.0	24.0	.97	16.1
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	373.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	1797.8	673.2	1299.	90.	AG	20.	100.0	.0	24.0	2.45	66.0
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1508.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1508.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1508.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1508.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1570.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1137.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	469.0	-169.6	760.	178.	AG	14.	100.0	.0	24.0	1.08	38.6
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	334.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	468.7	466.9	124.	178.	AG	6.	100.0	.0	12.0	.62	6.3
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	441.6	105.3	484.	179.	AG	6.	100.0	.0	12.0	1.65	24.6
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1249.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2170.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2150.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	378.9	3911.6	3176.	360.	AG	22.	100.0	.0	36.0	1.62	161.3
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	20.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	423.9	743.5	9.	360.	AG	7.	100.0	.0	12.0	.37	.4
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2371.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B1AM.DAT) RUN: Site 4 Build 1 AM
DATE: 03/22/2010 TIME: 10:43:00.54

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	69	2.0	588	1584	4.10	1	3
7.	EB Bev RT Q	120	62	2.0	64	1325	4.10	1	3
9.	EB Bev LT Q	120	112	2.0	82	1536	4.10	1	3
13.	WB Bev T+R Q	120	68	2.0	1223	1573	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	373	1536	4.10	1	3
22.	NB Cin THR Q	120	76	2.0	1137	1584	4.10	1	3
24.	NB Cin RT Q	120	68	2.0	334	1352	4.10	1	3
26.	NB Cin LT Q	120	69	2.0	99	155	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	2150	1476	4.10	1	3
32.	SB Cin LT Q	120	78	2.0	20	171	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	95	105	105	345	345	345	0	5	15	10	10	0	0

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.1	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.1	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX DEGR.	.0 0	.0 0	.0 0	.0 0	.1 120	.1 5	.1 0	.1 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 5 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

JOB: Site 4 Bev & La Cien (S4B1PM.DAT) RUN: Site 4 Build 1 PM
DATE: 03/22/2010 TIME: 10:51:31.95

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1849.	.8	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1849.	.8	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1849.	.8	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1604.	.8	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	-2030.6	641.0	2385.	270.	AG	13.	100.0	.0	24.0	1.32	121.1
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	54.	.8	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	335.4	624.9	19.	270.	AG	6.	100.0	.0	12.0	.12	.9
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	191.	.8	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	55.6	662.6	297.	270.	AG	20.	100.0	.0	24.0	1.25	15.1
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	2094.	.8	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1210.	.8	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	749.	.8	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	638.2	689.8	143.	90.	AG	13.	100.0	.0	24.0	.62	7.3
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	461.	.8	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	2282.0	675.9	1783.	90.	AG	20.	100.0	.0	24.0	3.03	90.6
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1256.	.8	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1256.	.8	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1256.	.8	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1256.	.8	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	2656.	.8	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1785.	.8	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	563.1	-3415.3	4007.	178.	AG	14.	100.0	.0	24.0	1.65	203.6
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	478.	.8	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	480.5	70.6	521.	178.	AG	6.	100.0	.0	12.0	1.05	26.4
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	393.	.8	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	512.0	-3096.6	3686.	179.	AG	6.	100.0	.0	12.0	6.66	187.3
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1977.	.8	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1537.	.8	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1525.	.8	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	395.3	1745.3	1009.	360.	AG	22.	100.0	.0	36.0	1.15	51.3
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	12.	.8	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	424.0	740.1	5.	360.	AG	7.	100.0	.0	12.0	.22	.3
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1925.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B1PM.DAT) RUN: Site 4 Build 1 PM
DATE: 03/22/2010 TIME: 10:51:31.95

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	70	2.0	1604	1584	4.10	1	3
7.	EB	Bev RT Q	120	63	2.0	54	1048	4.10	1	3
9.	EB	Bev LT Q	120	110	2.0	191	1536	4.10	1	3
13.	WB	Bev T+R Q	120	70	2.0	749	1583	4.10	1	3
15.	WB	Bev LT Q	120	110	2.0	461	1536	4.10	1	3
22.	NB	Cin THR Q	120	75	2.0	1785	1584	4.10	1	3
24.	NB	Cin RT Q	120	67	2.0	478	1113	4.10	1	3
26.	NB	Cin LT Q	120	69	2.0	393	153	4.10	1	3
30.	SB	Cin T+R Q	120	80	2.0	1525	1468	4.10	1	3
32.	SB	Cin LT Q	120	77	2.0	12	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

1

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	170	0	0	45	30	35	30	105	100	100	0	0	0	190	150	0	0	0	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.0	.1	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.1	.1
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	150	15	5	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .10 PPM AT 170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 45 DEGREES FROM REC4 .

JOB: Site 4 Bev & La Cien (S4B2AM.DAT) RUN: Site 4 Build 2 AM
DATE: 03/22/2010 TIME: 10:59:39.09

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	740.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	740.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	740.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	581.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	244.6	641.0	109.	270.	AG	13.	100.0	.0	24.0	.47	5.6
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	76.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	328.2	624.9	26.	270.	AG	6.	100.0	.0	12.0	.13	1.3
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	83.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	935.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1595.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1225.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	813.4	690.7	318.	90.	AG	12.	100.0	.0	24.0	.97	16.2
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	370.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	1786.8	673.2	1288.	90.	AG	20.	100.0	.0	24.0	2.43	65.4
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1511.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1511.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1511.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1511.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1586.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1152.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	471.4	-253.3	844.	178.	AG	14.	100.0	.0	24.0	1.09	42.9
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	335.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	468.7	466.5	125.	178.	AG	6.	100.0	.0	12.0	.62	6.3
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	441.6	105.3	484.	179.	AG	6.	100.0	.0	12.0	1.65	24.6
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1263.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2128.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2109.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	379.9	3775.0	3039.	360.	AG	22.	100.0	.0	36.0	1.59	154.4
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	19.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	423.9	743.1	8.	360.	AG	7.	100.0	.0	12.0	.35	.4
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2340.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B2AM.DAT) RUN: Site 4 Build 2 AM
DATE: 03/22/2010 TIME: 10:59:39.09

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	69	2.0	581	1584	4.10	1	3
7.	EB Bev RT Q	120	62	2.0	76	1325	4.10	1	3
9.	EB Bev LT Q	120	112	2.0	83	1536	4.10	1	3
13.	WB Bev T+R Q	120	68	2.0	1225	1574	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	370	1536	4.10	1	3
22.	NB Cin THR Q	120	76	2.0	1152	1584	4.10	1	3
24.	NB Cin RT Q	120	68	2.0	335	1352	4.10	1	3
26.	NB Cin LT Q	120	69	2.0	99	155	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	2109	1476	4.10	1	3
32.	SB Cin LT Q	120	78	2.0	19	171	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	95	105	105	345	345	345	0	10	15	10	10	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.1	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	125	5	0	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

JOB: Site 4 Bev & La Cien (S4B2PM.DAT) RUN: Site 4 Build 2 PM
DATE: 03/22/2010 TIME: 11:14:27.12

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	*	-543.0	891.0	-185.0	701.0	*	405.	118.	AG	1802.	.8	.0	44.0		
2.	EB Bev AP	*	-185.0	701.0	-55.0	655.0	*	138.	109.	AG	1802.	.8	.0	44.0		
3.	EB Bev AP	*	-55.0	655.0	123.0	646.0	*	178.	93.	AG	1802.	.8	.0	44.0		
4.	EB Bev THRU	*	124.0	641.0	417.0	641.0	*	293.	90.	AG	1617.	.8	.0	44.0		
5.	EB Bev THR Q	*	354.0	641.0	-2093.1	641.0	*	2447.	270.	AG	13.	100.0	.0	24.0	1.33	124.3
6.	EB Bev RT	*	126.0	624.0	402.0	626.0	*	276.	90.	AG	58.	.8	.0	32.0		
7.	EB Bev RT Q	*	354.0	625.0	334.0	624.9	*	20.	270.	AG	6.	100.0	.0	12.0	.13	1.0
8.	EB Bev LT	*	124.0	663.0	413.0	664.0	*	289.	90.	AG	127.	.8	.0	44.0		
9.	EB Bev LT Q	*	353.0	664.0	300.7	663.8	*	52.	270.	AG	20.	100.0	.0	24.0	.83	2.7
10.	EB Bev DP	*	418.0	641.0	1427.0	656.0	*	1009.	89.	AG	2068.	.8	.0	44.0		
11.	WB Bev AP	*	683.0	689.0	1428.0	687.0	*	745.	90.	AG	1211.	.8	.0	44.0		
12.	WB Bev T+R	*	683.0	690.0	443.0	689.0	*	240.	270.	AG	760.	.8	.0	44.0		
13.	WB Bev T+R Q	*	495.0	689.0	640.4	689.8	*	145.	90.	AG	13.	100.0	.0	24.0	.64	7.4
14.	WB Bev LT	*	685.0	667.0	445.0	665.0	*	240.	270.	AG	451.	.8	.0	44.0		
15.	WB Bev LT Q	*	499.0	666.0	2227.0	675.6	*	1728.	90.	AG	20.	100.0	.0	24.0	2.96	87.8
16.	WB Bev DP	*	442.0	689.0	75.0	687.0	*	367.	270.	AG	1216.	.8	.0	44.0		
17.	WB Bev DP	*	75.0	687.0	-43.0	699.0	*	119.	276.	AG	1216.	.8	.0	44.0		
18.	WB Bev DP	*	-43.0	699.0	-189.0	746.0	*	153.	288.	AG	1216.	.8	.0	44.0		
19.	WB Bev DP	*	-189.0	746.0	-533.0	933.0	*	392.	299.	AG	1216.	.8	.0	44.0		
20.	NB Cin AP	*	461.0	300.0	483.0	-335.0	*	635.	178.	AG	2227.	.8	.0	56.0		
21.	NB Cin THRU	*	456.0	301.0	445.0	652.0	*	351.	358.	AG	1814.	.8	.0	44.0		
22.	NB Cin THR Q	*	447.0	590.0	567.6	-3572.2	*	4164.	178.	AG	14.	100.0	.0	24.0	1.68	211.5
23.	NB Cin RT	*	474.0	302.0	463.0	648.0	*	346.	358.	AG	439.	.8	.0	32.0		
24.	NB Cin RT Q	*	465.0	591.0	472.0	355.3	*	236.	178.	AG	6.	100.0	.0	12.0	.97	12.0
25.	NB Cin LT	*	438.0	301.0	430.0	652.0	*	351.	359.	AG	401.	.8	.0	32.0		
26.	NB Cin LT Q	*	431.0	589.0	513.9	-3183.4	*	3773.	179.	AG	6.	100.0	.0	12.0	6.80	191.7
27.	NB Cin DP	*	445.0	652.0	431.0	1659.0	*	1007.	359.	AG	1998.	.8	.0	44.0		
28.	SB Cin AP	*	406.0	1039.0	398.0	1660.0	*	621.	359.	AG	1536.	.8	.0	44.0		
29.	SB Cin T+R	*	401.0	1038.0	404.0	661.0	*	377.	180.	AG	1524.	.8	.0	56.0		
30.	SB Cin T+R Q	*	403.0	736.0	395.3	1745.3	*	1009.	360.	AG	22.	100.0	.0	36.0	1.15	51.3
31.	SB Cin LT	*	422.0	1036.0	424.0	666.0	*	370.	180.	AG	12.	.8	.0	32.0		
32.	SB Cin LT Q	*	424.0	735.0	424.0	740.1	*	5.	360.	AG	7.	100.0	.0	12.0	.22	.3
33.	SB Cin DP	*	404.0	662.0	437.0	-338.0	*	1001.	178.	AG	1921.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B2PM.DAT) RUN: Site 4 Build 2 PM
DATE: 03/22/2010 TIME: 11:14:27.12

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	*	120	70	2.0	1617	1584	4.10	1	3
7.	EB Bev RT Q	*	120	63	2.0	58	1048	4.10	1	3
9.	EB Bev LT Q	*	120	110	2.0	127	1536	4.10	1	3
13.	WB Bev T+R Q	*	120	70	2.0	760	1546	4.10	1	3
15.	WB Bev LT Q	*	120	110	2.0	451	1536	4.10	1	3
22.	NB Cin THR Q	*	120	75	2.0	1814	1584	4.10	1	3
24.	NB Cin RT Q	*	120	67	2.0	439	1113	4.10	1	3
26.	NB Cin LT Q	*	120	69	2.0	401	153	4.10	1	3
30.	SB Cin T+R Q	*	120	80	2.0	1524	1468	4.10	1	3
32.	SB Cin LT Q	*	120	77	2.0	12	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	492.0	301.0	5.0	*
2.	SE 164 S	*	488.0	448.0	5.0	*
3.	SE 82 S	*	486.0	530.0	5.0	*
4.	SE CNR	*	491.0	605.0	5.0	*
5.	SE 82 E	*	564.0	612.0	5.0	*
6.	SE 164 E	*	646.0	612.0	5.0	*
7.	SE MID E	*	775.0	615.0	5.0	*
8.	NE MID E	*	767.0	715.0	5.0	*
9.	NE 164 E	*	637.0	714.0	5.0	*
10.	NE 82 E	*	555.0	714.0	5.0	*
11.	NE CNR	*	474.0	717.0	5.0	*
12.	NE 82 N	*	473.0	796.0	5.0	*
13.	NE 164 N	*	472.0	877.0	5.0	*
14.	NE MID N	*	474.0	999.0	5.0	*
15.	NW MID N	*	372.0	996.0	5.0	*
16.	NW 164 N	*	367.0	884.0	5.0	*
17.	NW 82 N	*	367.0	803.0	5.0	*
18.	NW CNR	*	365.0	726.0	5.0	*
19.	NW 82 W	*	287.0	721.0	5.0	*
20.	NW 164 W	*	206.0	720.0	5.0	*
21.	NW MID W	*	62.0	720.0	5.0	*
22.	SW MID W	*	56.0	606.0	5.0	*
23.	SW 164 W	*	209.0	606.0	5.0	*
24.	SW 82 W	*	289.0	606.0	5.0	*
25.	SW CNR	*	361.0	601.0	5.0	*
26.	SW 82 S	*	376.0	526.0	5.0	*
27.	SW 164 S	*	380.0	445.0	5.0	*
28.	SW MID S	*	385.0	307.0	5.0	*

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	175	0	0	45	35	35	35	105	100	100	0	0	0	190	150	0	0	0	0	0

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REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.0	.1	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.1	.1
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.0	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4B2PM.DAT) RUN: Site 4 Build 2 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	150	15	5	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .10 PPM AT 175 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 45 DEGREES FROM REC4 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 4 Bev & La Cien (S4B3AM.DAT) RUN: Site 4 Build 3 AM
DATE: 03/22/2010 TIME: 11:26:49.93

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	746.	.8	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	746.	.8	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	746.	.8	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	597.	.8	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	241.6	641.0	112.	270.	AG	13.	100.0	.0	24.0	.48	5.7
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	67.	.8	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	331.3	624.9	23.	270.	AG	6.	100.0	.0	12.0	.11	1.2
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	82.	.8	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	941.	.8	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1594.	.8	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1219.	.8	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	813.5	690.7	319.	90.	AG	12.	100.0	.0	24.0	.97	16.2
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	375.	.8	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	1808.8	673.3	1310.	90.	AG	20.	100.0	.0	24.0	2.46	66.5
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1480.	.8	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1480.	.8	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1480.	.8	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1480.	.8	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1568.	.8	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1145.	.8	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	470.2	-211.4	802.	178.	AG	14.	100.0	.0	24.0	1.09	40.7
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	324.	.8	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	468.6	470.6	120.	178.	AG	6.	100.0	.0	12.0	.60	6.1
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	441.6	105.3	484.	179.	AG	6.	100.0	.0	12.0	1.65	24.6
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1282.	.8	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2151.	.8	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2131.	.8	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	379.3	3848.6	3113.	360.	AG	22.	100.0	.0	36.0	1.61	158.1
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	20.	.8	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	423.9	743.5	9.	360.	AG	7.	100.0	.0	12.0	.37	.4
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2356.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B3AM.DAT) RUN: Site 4 Build 3 AM
DATE: 03/22/2010 TIME: 11:26:49.93

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	69	2.0	597	1584	4.10	1	3
7.	EB	Bev RT Q	120	62	2.0	67	1325	4.10	1	3
9.	EB	Bev LT Q	120	112	2.0	82	1536	4.10	1	3
13.	WB	Bev T+R Q	120	68	2.0	1219	1564	4.10	1	3
15.	WB	Bev LT Q	120	110	2.0	375	1536	4.10	1	3
22.	NB	Cin THR Q	120	76	2.0	1145	1584	4.10	1	3
24.	NB	Cin RT Q	120	68	2.0	324	1352	4.10	1	3
26.	NB	Cin LT Q	120	69	2.0	99	155	4.10	1	3
30.	SB	Cin T+R Q	120	80	2.0	2131	1476	4.10	1	3
32.	SB	Cin LT Q	120	78	2.0	20	171	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	95	105	105	345	345	345	0	10	15	10	10	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.1	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4B3AM.DAT) RUN: Site 4 Build 3 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX DEGR.	.0 0	.0 0	.0 0	.0 0	.1 125	.1 5	.1 0	.1 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

JOB: Site 4 Bev & La Cien (S4B3PM.DAT) RUN: Site 4 Build 3 PM
DATE: 03/22/2010 TIME: 11:41:44.23

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1841.	.8	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1841.	.8	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1841.	.8	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1599.	.8	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	-1999.3	641.0	2353.	270.	AG	13.	100.0	.0	24.0	1.32	119.5
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	105.	.8	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	317.8	624.8	36.	270.	AG	6.	100.0	.0	12.0	.23	1.8
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	137.	.8	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	289.7	663.7	63.	270.	AG	20.	100.0	.0	24.0	.89	3.2
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	2076.	.8	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1239.	.8	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	788.	.8	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	645.8	689.8	151.	90.	AG	13.	100.0	.0	24.0	.66	7.7
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	451.	.8	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	2227.0	675.6	1728.	90.	AG	20.	100.0	.0	24.0	2.96	87.8
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1241.	.8	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1241.	.8	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1241.	.8	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1241.	.8	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	2670.	.8	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1806.	.8	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	566.4	-3530.3	4122.	178.	AG	14.	100.0	.0	24.0	1.67	209.4
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	465.	.8	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	476.4	206.2	385.	178.	AG	6.	100.0	.0	12.0	1.02	19.6
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	399.	.8	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	513.4	-3161.7	3752.	179.	AG	6.	100.0	.0	12.0	6.76	190.6
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	2000.	.8	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1517.	.8	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1505.	.8	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	395.9	1671.7	936.	360.	AG	22.	100.0	.0	36.0	1.14	47.5
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	12.	.8	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	424.0	740.1	5.	360.	AG	7.	100.0	.0	12.0	.22	.3
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1950.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B3PM.DAT) RUN: Site 4 Build 3 PM
DATE: 03/22/2010 TIME: 11:41:44.23

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	70	2.0	1599	1584	4.10	1	3
7.	EB	Bev RT Q	120	63	2.0	105	1048	4.10	1	3
9.	EB	Bev LT Q	120	110	2.0	137	1536	4.10	1	3
13.	WB	Bev T+R Q	120	70	2.0	788	1548	4.10	1	3
15.	WB	Bev LT Q	120	110	2.0	451	1536	4.10	1	3
22.	NB	Cin THR Q	120	75	2.0	1806	1584	4.10	1	3
24.	NB	Cin RT Q	120	67	2.0	465	1113	4.10	1	3
26.	NB	Cin LT Q	120	69	2.0	399	153	4.10	1	3
30.	SB	Cin T+R Q	120	80	2.0	1505	1469	4.10	1	3
32.	SB	Cin LT Q	120	77	2.0	12	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	170	0	0	45	30	35	30	105	100	100	0	0	0	190	150	0	0	0	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.1
90.	.0	.0	.0	.0	.0	.0	.0	.1
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.1	.1	.1
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4B3PM.DAT) RUN: Site 4 Build 3 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	150	15	5	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .10 PPM AT 170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 45 DEGREES FROM REC4 .

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Site 4 Bev & La Cien (S4B4AM.DAT) RUN: Site 4 Build 4 AM
DATE: 03/22/2010 TIME: 11:50:02.46

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	726.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	726.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	726.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	581.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	244.6	641.0	109.	270.	AG	13.	100.0	.0	24.0	.47	5.6
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	62.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	333.0	624.9	21.	270.	AG	6.	100.0	.0	12.0	.10	1.1
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	83.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	933.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1587.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1220.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	809.5	690.7	314.	90.	AG	12.	100.0	.0	24.0	.97	16.0
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	367.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	1764.8	673.0	1266.	90.	AG	20.	100.0	.0	24.0	2.41	64.3
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1507.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1507.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1507.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1507.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1558.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1127.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	467.5	-117.2	708.	178.	AG	14.	100.0	.0	24.0	1.07	35.9
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	332.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	468.7	467.6	123.	178.	AG	6.	100.0	.0	12.0	.61	6.3
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	446.7	-127.3	717.	179.	AG	6.	100.0	.0	12.0	2.61	36.4
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1239.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2153.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2133.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	379.3	3859.1	3123.	360.	AG	22.	100.0	.0	36.0	1.61	158.7
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	20.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	423.9	743.5	9.	360.	AG	7.	100.0	.0	12.0	.37	.4
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2345.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B4AM.DAT) RUN: Site 4 Build 4 AM
DATE: 03/22/2010 TIME: 11:50:02.46

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	69	2.0	581	1584	4.10	1	3
7.	EB Bev RT Q	120	62	2.0	62	1325	4.10	1	3
9.	EB Bev LT Q	120	112	2.0	83	1536	4.10	1	3
13.	WB Bev T+R Q	120	68	2.0	1220	1573	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	367	1536	4.10	1	3
22.	NB Cin THR Q	120	76	2.0	1127	1584	4.10	1	3
24.	NB Cin RT Q	120	68	2.0	332	1352	4.10	1	3
26.	NB Cin LT Q	120	69	2.0	99	99	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	2133	1476	4.10	1	3
32.	SB Cin LT Q	120	78	2.0	20	171	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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JOB: Site 4 Bev & La Cien (S4B4AM.DAT) RUN: Site 4 Build 4 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4B4AM.DAT) RUN: Site 4 Build 4 AM

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	95	105	105	345	345	345	0	10	15	10	10	0	0

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JOB: Site 4 Bev & La Cien (S4B4AM.DAT) RUN: Site 4 Build 4 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.1	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 4 Bev & La Cien (S4B4AM.DAT) RUN: Site 4 Build 4 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	125	5	0	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

JOB: Site 4 Bev & La Cien (S4B4PM.DAT) RUN: Site 4 Build 4 PM
DATE: 03/22/2010 TIME: 11:56:42.98

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1853.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1853.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1853.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1610.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	-2061.8	641.0	2416.	270.	AG	13.	100.0	.0	24.0	1.33	122.7
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	54.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	335.4	624.9	19.	270.	AG	6.	100.0	.0	12.0	.12	.9
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	189.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	66.6	662.7	286.	270.	AG	20.	100.0	.0	24.0	1.24	14.5
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	2090.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1239.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	781.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	644.3	689.8	149.	90.	AG	13.	100.0	.0	24.0	.64	7.6
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	458.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	2271.0	675.8	1772.	90.	AG	20.	100.0	.0	24.0	3.01	90.0
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1288.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1288.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1288.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1288.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	2624.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1767.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	560.4	-3321.2	3913.	178.	AG	14.	100.0	.0	24.0	1.63	198.8
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	468.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	477.4	174.9	416.	178.	AG	6.	100.0	.0	12.0	1.03	21.1
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	389.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	511.0	-3053.2	3643.	179.	AG	6.	100.0	.0	12.0	6.59	185.1
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1957.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1510.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1498.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	396.0	1660.7	925.	360.	AG	22.	100.0	.0	36.0	1.14	47.0
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	12.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	424.0	740.1	5.	360.	AG	7.	100.0	.0	12.0	.22	.3
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1891.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B4PM.DAT) RUN: Site 4 Build 4 PM
DATE: 03/22/2010 TIME: 11:56:42.98

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	70	2.0	1610	1584	4.10	1	3
7.	EB Bev RT Q	120	63	2.0	54	1048	4.10	1	3
9.	EB Bev LT Q	120	110	2.0	189	1536	4.10	1	3
13.	WB Bev T+R Q	120	70	2.0	781	1583	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	458	1536	4.10	1	3
22.	NB Cin THR Q	120	75	2.0	1767	1584	4.10	1	3
24.	NB Cin RT Q	120	67	2.0	468	1113	4.10	1	3
26.	NB Cin LT Q	120	69	2.0	389	153	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	1498	1465	4.10	1	3
32.	SB Cin LT Q	120	77	2.0	12	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	170	0	0	45	30	35	30	105	100	100	0	0	190	190	150	0	0	0	0	0

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.0	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.0	.0	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.0	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX DEGR.	.0 0	.0 0	.0 0	.0 0	.1 150	.1 20	.1 5	.1 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .10 PPM AT 170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 45 DEGREES FROM REC4 .

JOB: Site 4 Bev & La Cien (S4B5AM.DAT) RUN: Site 4 Build 5 AM
DATE: 03/22/2010 TIME: 12:16:54.14

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	740.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	740.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	740.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	594.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	241.9	641.0	112.	270.	AG	13.	100.0	.0	24.0	.48	5.7
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	64.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	332.3	624.9	22.	270.	AG	6.	100.0	.0	12.0	.11	1.1
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	82.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	317.0	663.8	36.	270.	AG	21.	100.0	.0	24.0	.80	1.8
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	933.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1594.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1240.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	830.1	690.8	335.	90.	AG	12.	100.0	.0	24.0	.99	17.0
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	354.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	1698.8	672.7	1200.	90.	AG	20.	100.0	.0	24.0	2.33	60.9
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1527.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1527.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1527.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1527.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1552.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1134.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	468.7	-159.1	749.	178.	AG	14.	100.0	.0	24.0	1.08	38.1
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	319.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	468.5	472.4	119.	178.	AG	6.	100.0	.0	12.0	.59	6.0
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	446.7	-127.3	717.	179.	AG	6.	100.0	.0	12.0	2.61	36.4
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1245.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	2130.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	2110.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	379.9	3775.0	3039.	360.	AG	22.	100.0	.0	36.0	1.59	154.4
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	20.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	423.9	743.5	9.	360.	AG	7.	100.0	.0	12.0	.37	.4
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	2311.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B5AM.DAT) RUN: Site 4 Build 5 AM
DATE: 03/22/2010 TIME: 12:16:54.14

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	69	2.0	594	1584	4.10	1	3
7.	EB Bev RT Q	120	62	2.0	64	1325	4.10	1	3
9.	EB Bev LT Q	120	112	2.0	82	1536	4.10	1	3
13.	WB Bev T+R Q	120	68	2.0	1240	1574	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	354	1536	4.10	1	3
22.	NB Cin THR Q	120	76	2.0	1134	1584	4.10	1	3
24.	NB Cin RT Q	120	68	2.0	319	1352	4.10	1	3
26.	NB Cin LT Q	120	69	2.0	99	99	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	2110	1475	4.10	1	3
32.	SB Cin LT Q	120	78	2.0	20	171	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
45.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0
50.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
170.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.1	.0	.0
175.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.1	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.2	.2	.2	.2	.0	.0
DEGR.	180	0	0	0	0	0	0	95	105	105	345	345	345	0	10	15	10	10	0	0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.1	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.1	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.1	.1	.1
55.	.0	.0	.0	.0	.0	.1	.1	.1
60.	.0	.0	.0	.0	.0	.1	.1	.1
65.	.0	.0	.0	.0	.0	.1	.1	.1
70.	.0	.0	.0	.0	.0	.1	.1	.1
75.	.0	.0	.0	.0	.0	.1	.1	.1
80.	.0	.0	.0	.0	.0	.1	.1	.1
85.	.0	.0	.0	.0	.0	.1	.1	.1
90.	.0	.0	.0	.0	.0	.1	.1	.1
95.	.0	.0	.0	.0	.0	.1	.1	.1
100.	.0	.0	.0	.0	.0	.1	.1	.1
105.	.0	.0	.0	.0	.0	.1	.1	.1
110.	.0	.0	.0	.0	.0	.1	.1	.1
115.	.0	.0	.0	.0	.0	.1	.1	.1
120.	.0	.0	.0	.0	.0	.1	.1	.1
125.	.0	.0	.0	.0	.1	.1	.1	.1
130.	.0	.0	.0	.0	.1	.1	.1	.1
135.	.0	.0	.0	.0	.1	.1	.1	.1
140.	.0	.0	.0	.0	.1	.1	.1	.1
145.	.0	.0	.0	.0	.1	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.1	.1	.1	.1
175.	.0	.0	.0	.0	.1	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.1	.1
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.1
360.	.0	.0	.0	.0	.0	.0	.1	.1
MAX DEGR.	.0 0	.0 0	.0 0	.0 0	.1 125	.1 10	.1 0	.1 0

THE HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 10 DEGREES FROM REC17.

JOB: Site 4 Bev & La Cien (S4B5PM.DAT) RUN: Site 4 Build 5 PM
DATE: 03/22/2010 TIME: 12:17:08.91

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1813.	.8	.0	44.0		
2.	EB Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1813.	.8	.0	44.0		
3.	EB Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1813.	.8	.0	44.0		
4.	EB Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1594.	.8	.0	44.0		
5.	EB Bev THR Q	354.0	641.0	-1978.4	641.0	2332.	270.	AG	13.	100.0	.0	24.0	1.31	118.5
6.	EB Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	55.	.8	.0	32.0		
7.	EB Bev RT Q	354.0	625.0	335.1	624.9	19.	270.	AG	6.	100.0	.0	12.0	.12	1.0
8.	EB Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	164.	.8	.0	44.0		
9.	EB Bev LT Q	353.0	664.0	198.7	663.3	154.	270.	AG	20.	100.0	.0	24.0	1.08	7.8
10.	EB Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	2070.	.8	.0	44.0		
11.	WB Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1216.	.8	.0	44.0		
12.	WB Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	760.	.8	.0	44.0		
13.	WB Bev T+R Q	495.0	689.0	640.4	689.8	145.	90.	AG	13.	100.0	.0	24.0	.63	7.4
14.	WB Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	456.	.8	.0	44.0		
15.	WB Bev LT Q	499.0	666.0	2260.0	675.8	1761.	90.	AG	20.	100.0	.0	24.0	3.00	89.5
16.	WB Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1265.	.8	.0	44.0		
17.	WB Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1265.	.8	.0	44.0		
18.	WB Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1265.	.8	.0	44.0		
19.	WB Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1265.	.8	.0	44.0		
20.	NB Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	2653.	.8	.0	56.0		
21.	NB Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1811.	.8	.0	44.0		
22.	NB Cin THR Q	447.0	590.0	575.2	-3831.7	4424.	178.	AG	14.	100.0	.0	24.0	1.76	224.7
23.	NB Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	448.	.8	.0	32.0		
24.	NB Cin RT Q	465.0	591.0	476.6	199.5	392.	178.	AG	6.	100.0	.0	12.0	1.03	19.9
25.	NB Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	394.	.8	.0	32.0		
26.	NB Cin LT Q	431.0	589.0	512.3	-3109.6	3699.	179.	AG	6.	100.0	.0	12.0	6.68	187.9
27.	NB Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1976.	.8	.0	44.0		
28.	SB Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1544.	.8	.0	44.0		
29.	SB Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1516.	.8	.0	56.0		
30.	SB Cin T+R Q	403.0	736.0	395.6	1713.7	978.	360.	AG	22.	100.0	.0	36.0	1.15	49.7
31.	SB Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	28.	.8	.0	32.0		
32.	SB Cin LT Q	424.0	735.0	423.9	746.6	12.	360.	AG	7.	100.0	.0	12.0	.51	.6
33.	SB Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1915.	.8	.0	56.0		

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JOB: Site 4 Bev & La Cien (S4B5PM.DAT) RUN: Site 4 Build 5 PM
DATE: 03/22/2010 TIME: 12:17:08.91

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB Bev THR Q	120	70	2.0	1594	1584	4.10	1	3
7.	EB Bev RT Q	120	63	2.0	55	1048	4.10	1	3
9.	EB Bev LT Q	120	110	2.0	164	1536	4.10	1	3
13.	WB Bev T+R Q	120	70	2.0	760	1583	4.10	1	3
15.	WB Bev LT Q	120	110	2.0	456	1536	4.10	1	3
22.	NB Cin THR Q	120	77	2.0	1811	1584	4.10	1	3
24.	NB Cin RT Q	120	69	2.0	448	1114	4.10	1	3
26.	NB Cin LT Q	120	70	2.0	394	156	4.10	1	3
30.	SB Cin T+R Q	120	80	2.0	1516	1469	4.10	1	3
32.	SB Cin LT Q	120	76	2.0	28	168	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
35.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
40.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
90.	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
130.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
135.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
140.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
145.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
150.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
155.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
160.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
165.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
330.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
335.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
340.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.0	.0
MAX	.1	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.0	.0
DEGR.	170	0	0	45	30	35	35	105	100	100	0	0	0	190	150	0	0	0	0	0

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REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.0	.0	.0	.0	.0	.0	.1
5.	.0	.0	.0	.0	.0	.0	.1	.1
10.	.0	.0	.0	.0	.0	.0	.1	.1
15.	.0	.0	.0	.0	.0	.1	.1	.1
20.	.0	.0	.0	.0	.0	.1	.1	.1
25.	.0	.0	.0	.0	.0	.1	.1	.1
30.	.0	.0	.0	.0	.0	.1	.1	.1
35.	.0	.0	.0	.0	.0	.1	.1	.1
40.	.0	.0	.0	.0	.0	.1	.1	.1
45.	.0	.0	.0	.0	.0	.1	.1	.1
50.	.0	.0	.0	.0	.0	.0	.1	.1
55.	.0	.0	.0	.0	.0	.0	.0	.0
60.	.0	.0	.0	.0	.0	.0	.0	.0
65.	.0	.0	.0	.0	.0	.0	.0	.0
70.	.0	.0	.0	.0	.0	.0	.0	.0
75.	.0	.0	.0	.0	.0	.0	.0	.0
80.	.0	.0	.0	.0	.0	.0	.0	.0
85.	.0	.0	.0	.0	.0	.0	.0	.0
90.	.0	.0	.0	.0	.0	.0	.0	.0
95.	.0	.0	.0	.0	.0	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.0
125.	.0	.0	.0	.0	.0	.0	.1	.1
130.	.0	.0	.0	.0	.0	.1	.1	.1
135.	.0	.0	.0	.0	.0	.1	.1	.1
140.	.0	.0	.0	.0	.0	.1	.1	.1
145.	.0	.0	.0	.0	.0	.1	.1	.1
150.	.0	.0	.0	.0	.1	.1	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.1
165.	.0	.0	.0	.0	.1	.1	.1	.1
170.	.0	.0	.0	.0	.0	.1	.1	.1
175.	.0	.0	.0	.0	.0	.1	.1	.1
180.	.0	.0	.0	.0	.0	.1	.1	.1
185.	.0	.0	.0	.0	.0	.0	.0	.0
190.	.0	.0	.0	.0	.0	.0	.0	.0
195.	.0	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.0	.0	.0	.0	.0	.0	.0	.0
215.	.0	.0	.0	.0	.0	.0	.0	.0
220.	.0	.0	.0	.0	.0	.0	.0	.0
225.	.0	.0	.0	.0	.0	.0	.0	.0
230.	.0	.0	.0	.0	.0	.0	.0	.0
235.	.0	.0	.0	.0	.0	.0	.0	.0
240.	.0	.0	.0	.0	.0	.0	.0	.0
245.	.0	.0	.0	.0	.0	.0	.0	.0
250.	.0	.0	.0	.0	.0	.0	.0	.0
255.	.0	.0	.0	.0	.0	.0	.0	.0
260.	.0	.0	.0	.0	.0	.0	.0	.0
265.	.0	.0	.0	.0	.0	.0	.0	.0
270.	.0	.0	.0	.0	.0	.0	.0	.0
275.	.0	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.0	.0	.0	.0
285.	.0	.0	.0	.0	.0	.0	.0	.0
290.	.0	.0	.0	.0	.0	.0	.0	.0
295.	.0	.0	.0	.0	.0	.0	.0	.0
300.	.0	.0	.0	.0	.0	.0	.0	.0
305.	.0	.0	.0	.0	.0	.0	.0	.0
310.	.0	.0	.0	.0	.0	.0	.0	.0
315.	.0	.0	.0	.0	.0	.0	.0	.0
320.	.0	.0	.0	.0	.0	.0	.0	.0
325.	.0	.0	.0	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.1
MAX	.0	.0	.0	.0	.1	.1	.1	.1
DEGR.	0	0	0	0	150	15	5	0

THE HIGHEST CONCENTRATION IS .20 PPM AT 150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .10 PPM AT 170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS .10 PPM AT 45 DEGREES FROM REC4 .

Site 4

Existing with Project

Input & Output Files

```
Site 4 Bev & La Ci (S4EXWPAM.DAT)       60.0321.0.0000.000280.30480000
1    1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 Existing WITH PROJ AM            33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     710 3.3   0  44
30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     710 3.3   0  44
30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     710 3.3   0  44
30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     576 3.3   0  44
30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
      120        69       2.0  576   20.5 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      53 3.3   0  32
30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
      120        62       2.0   53   20.5 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      81 3.3   0  44
30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
      120       112       2.0   81   20.5 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     842 3.3   0  44
```

```
30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1304 3.3   0  44
30.
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1035 3.3   0  44
30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1035   20.5 1555 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     269 3.3   0  44
30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  269   20.5 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1330 3.3   0  44
30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1330 3.3   0  44
30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1330 3.3   0  44
30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1330 3.3   0  44
30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1087 3.3   0  56
30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.     792 3.3   0  44
30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        79       2.0  792   20.5 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     196 3.3   0  32
30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        71       2.0  196   20.5 1353 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 3.3   0  32
30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        72       2.0   99   20.5  165 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.     943 3.3   0  44
30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1523 3.3   0  44
30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1453 3.3   0  56
30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
```

```
       120        80       2.0 1453   20.5 1443 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      70 3.3   0  32
30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        75       2.0   70   20.5  284 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1509 3.3   0  56
30.
1.0   04 1000.   0Y  5  0 72
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JOB: Site 4 Bev & La Ci (S4EXWPAM.DAT) RUN: Site 4 Existing WITH PROJ AM
DATE: 07/13/2011 TIME: 13:18:25.13

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	710.	3.3	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	710.	3.3	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	710.	3.3	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	576.	3.3	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	245.3	641.0	109.	270.	AG	63.	100.0	.0	24.0	.46	5.5
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	53.	3.3	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	336.0	624.9	18.	270.	AG	28.	100.0	.0	12.0	.09	.9
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	81.	3.3	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	319.0	663.8	34.	270.	AG	103.	100.0	.0	24.0	.78	1.7
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	842.	3.3	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1304.	3.3	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	1035.	3.3	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	699.5	690.1	205.	90.	AG	62.	100.0	.0	24.0	.83	10.4
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	269.	3.3	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	1225.6	670.0	727.	90.	AG	101.	100.0	.0	24.0	1.76	36.9
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	1330.	3.3	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	1330.	3.3	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	1330.	3.3	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	1330.	3.3	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1087.	3.3	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	792.	3.3	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	452.3	408.1	182.	178.	AG	72.	100.0	.0	24.0	.81	9.2
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	196.	3.3	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	467.3	514.9	76.	178.	AG	33.	100.0	.0	12.0	.39	3.9
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	99.	3.3	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	441.7	103.6	485.	179.	AG	33.	100.0	.0	12.0	1.65	24.7
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	943.	3.3	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1523.	3.3	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1453.	3.3	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	396.6	1572.8	837.	360.	AG	110.	100.0	.0	36.0	1.12	42.5
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	70.	3.3	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	423.7	768.9	34.	360.	AG	34.	100.0	.0	12.0	.72	1.7
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1509.	3.3	.0	56.0		

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JOB: Site 4 Bev & La Ci (S4EXWPAM.DAT) RUN: Site 4 Existing WITH PROJ AM
DATE: 07/13/2011 TIME: 13:18:25.13

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	69	2.0	576	1584	20.50	1	3
7.	EB	Bev RT Q	120	62	2.0	53	1325	20.50	1	3
9.	EB	Bev LT Q	120	112	2.0	81	1536	20.50	1	3
13.	WB	Bev T+R Q	120	68	2.0	1035	1555	20.50	1	3
15.	WB	Bev LT Q	120	110	2.0	269	1536	20.50	1	3
22.	NB	Cin THR Q	120	79	2.0	792	1584	20.50	1	3
24.	NB	Cin RT Q	120	71	2.0	196	1353	20.50	1	3
26.	NB	Cin LT Q	120	72	2.0	99	165	20.50	1	3
30.	SB	Cin T+R Q	120	80	2.0	1453	1443	20.50	1	3
32.	SB	Cin LT Q	120	75	2.0	70	284	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.2	.1	.2	.5	.5	.5	.4	.0	.0	.0	.2	.2	.3	.3	.5	.5	.5	.4	.1	.0
5.	.0	.1	.1	.4	.5	.5	.4	.0	.0	.0	.2	.2	.2	.2	.6	.5	.5	.4	.1	.0
10.	.0	.0	.1	.4	.5	.4	.4	.0	.0	.0	.1	.1	.1	.0	.8	.7	.8	.6	.1	.1
15.	.0	.1	.1	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.9	.7	.7	.7	.1	.1
20.	.0	.1	.1	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.8	.7	.7	.2	.1
25.	.0	.1	.1	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.6	.3	.1
30.	.0	.1	.1	.4	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.7	.7	.6	.3	.1
35.	.1	.1	.1	.5	.5	.3	.4	.0	.0	.0	.0	.0	.0	.0	.7	.7	.6	.6	.3	.1
40.	.1	.1	.1	.5	.5	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.6	.6	.6	.2	.1
45.	.1	.1	.1	.5	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.7	.6	.6	.6	.2	.1
50.	.0	.1	.1	.5	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.6	.5	.4	.2	.1
55.	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
60.	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
65.	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
70.	.0	.1	.1	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.5	.5	.4	.2	.1
75.	.0	.0	.1	.4	.4	.4	.4	.1	.0	.0	.0	.0	.0	.0	.5	.5	.5	.3	.2	.1
80.	.0	.0	.1	.4	.4	.4	.4	.1	.2	.2	.1	.0	.0	.0	.6	.5	.5	.3	.2	.1
85.	.0	.0	.0	.2	.4	.3	.3	.2	.2	.4	.3	.0	.0	.0	.6	.5	.5	.4	.3	.2
90.	.0	.0	.0	.2	.2	.2	.2	.3	.3	.4	.4	.0	.0	.0	.6	.5	.5	.4	.3	.2
95.	.0	.0	.0	.2	.2	.2	.2	.4	.5	.5	.5	.1	.0	.0	.6	.5	.6	.5	.3	.2
100.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.7	.1	.0	.0	.5	.5	.6	.5	.3	.2
105.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.7	.6	.1	.0	.0	.5	.6	.6	.6	.3	.3
110.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.7	.6	.1	.1	.0	.5	.6	.6	.5	.2	.2
115.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.6	.1	.1	.0	.5	.6	.6	.4	.1	.2
120.	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.6	.2	.1	.0	.7	.6	.6	.3	.1	.3
125.	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.5	.2	.1	.1	.7	.6	.6	.2	.2	.3
130.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.5	.2	.1	.1	.8	.7	.7	.2	.3	.2
135.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.5	.2	.1	.1	.8	.7	.7	.2	.3	.3
140.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.3	.2	.1	.1	.8	.7	.5	.3	.3	.3
145.	.0	.0	.0	.0	.0	.0	.0	.4	.6	.6	.3	.2	.1	.1	.7	.6	.4	.3	.4	.3
150.	.0	.0	.0	.0	.0	.0	.0	.4	.6	.5	.3	.2	.1	.1	.7	.6	.4	.3	.4	.2
155.	.0	.0	.0	.0	.0	.0	.0	.4	.6	.5	.2	.2	.1	.0	.7	.5	.4	.4	.4	.2
160.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.5	.2	.1	.1	.0	.7	.5	.4	.4	.3	.1
165.	.1	.0	.0	.0	.0	.0	.0	.4	.6	.5	.1	.1	.0	.0	.6	.5	.3	.4	.3	.1
170.	.1	.0	.0	.0	.0	.0	.0	.4	.6	.5	.1	.0	.0	.0	.5	.5	.4	.3	.3	.1
175.	.1	.1	.0	.0	.0	.0	.0	.4	.5	.5	.3	.1	.1	.1	.6	.3	.3	.2	.2	.1
180.	.2	.2	.1	.2	.0	.0	.0	.3	.5	.5	.4	.2	.2	.1	.4	.3	.3	.2	.2	.1
185.	.3	.2	.3	.2	.0	.0	.0	.4	.5	.5	.4	.2	.2	.2	.3	.3	.3	.3	.2	.1
190.	.3	.3	.3	.3	.0	.0	.0	.4	.6	.6	.5	.2	.2	.3	.2	.0	.1	.3	.2	.1
195.	.3	.2	.4	.3	.1	.0	.0	.4	.6	.6	.5	.2	.4	.3	.2	.0	.1	.3	.2	.1
200.	.3	.2	.4	.4	.1	.0	.0	.4	.5	.6	.4	.2	.3	.4	.0	.0	.1	.3	.2	.1
205.	.3	.3	.4	.5	.1	.0	.0	.4	.5	.7	.3	.3	.3	.4	.0	.0	.1	.3	.1	.1

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.2	.4	.5	.5	.1	.0	.0	.4	.5	.7	.3	.2	.3	.4	.0	.0	.1	.3	.1	.1
215.	.2	.4	.5	.5	.2	.0	.0	.4	.6	.6	.3	.3	.4	.4	.0	.0	.1	.3	.1	.1
220.	.2	.3	.5	.4	.2	.0	.0	.4	.6	.5	.4	.4	.4	.4	.0	.0	.1	.3	.1	.1
225.	.2	.3	.4	.4	.2	.0	.0	.5	.6	.5	.4	.4	.4	.4	.0	.0	.1	.3	.1	.1
230.	.2	.3	.4	.3	.2	.0	.0	.5	.6	.5	.4	.4	.4	.4	.0	.0	.1	.2	.1	.1
235.	.2	.3	.4	.3	.2	.0	.0	.5	.6	.4	.4	.4	.4	.4	.0	.0	.1	.1	.2	.1
240.	.2	.3	.5	.3	.2	.0	.0	.6	.5	.3	.4	.4	.4	.4	.0	.0	.1	.1	.2	.1
245.	.2	.3	.5	.3	.2	.0	.0	.5	.6	.2	.3	.5	.4	.4	.0	.0	.0	.1	.2	.1
250.	.2	.4	.5	.3	.2	.0	.0	.6	.5	.3	.3	.5	.4	.4	.0	.0	.0	.1	.2	.1
255.	.2	.4	.5	.3	.1	.0	.0	.5	.5	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
260.	.2	.4	.5	.2	.1	.0	.0	.4	.3	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
265.	.2	.4	.5	.2	.1	.0	.1	.4	.3	.2	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
270.	.2	.4	.5	.2	.0	.1	.2	.4	.2	.2	.3	.4	.4	.4	.0	.0	.0	.1	.1	.1
275.	.1	.4	.5	.2	.1	.1	.2	.2	.2	.3	.4	.4	.4	.4	.0	.0	.0	.1	.1	.0
280.	.1	.4	.5	.2	.2	.2	.2	.0	.2	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
285.	.2	.4	.5	.3	.2	.2	.4	.0	.1	.2	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0
290.	.2	.4	.5	.3	.2	.2	.4	.1	.1	.2	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0
295.	.2	.4	.5	.4	.2	.2	.4	.1	.1	.2	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0
300.	.2	.4	.5	.4	.2	.5	.4	.1	.1	.2	.3	.4	.4	.3	.0	.0	.0	.0	.0	.0
305.	.2	.4	.4	.2	.2	.6	.5	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
310.	.2	.4	.4	.3	.4	.6	.5	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
315.	.2	.4	.4	.3	.4	.6	.5	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
320.	.2	.4	.4	.3	.6	.6	.5	.1	.1	.2	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
325.	.3	.4	.4	.4	.6	.6	.5	.1	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
330.	.3	.4	.5	.4	.6	.6	.5	.1	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
335.	.3	.5	.5	.4	.6	.6	.4	.0	.1	.1	.4	.4	.4	.4	.0	.0	.0	.0	.0	.0
340.	.3	.4	.4	.5	.6	.6	.4	.0	.1	.1	.4	.4	.5	.4	.1	.0	.0	.0	.0	.0
345.	.4	.3	.4	.5	.6	.6	.4	.0	.1	.1	.4	.4	.4	.4	.1	.1	.1	.1	.0	.0
350.	.4	.3	.3	.5	.6	.5	.4	.0	.0	.1	.4	.4	.4	.4	.3	.1	.2	.1	.0	.0
355.	.3	.2	.2	.4	.6	.5	.4	.0	.0	.1	.3	.3	.3	.3	.3	.4	.3	.3	.0	.0
360.	.2	.1	.2	.5	.5	.5	.4	.0	.0	.0	.2	.2	.3	.3	.5	.5	.5	.4	.1	.0
MAX	.4	.5	.5	.5	.6	.6	.5	.6	.7	.7	.7	.5	.5	.4	.9	.8	.8	.7	.4	.3
DEGR.	345	335	210	0	320	305	305	240	120	205	100	245	340	200	15	20	10	15	145	105

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.4	.5	.3	.3	.3
5.	.0	.1	.2	.4	.4	.4	.3	.3
10.	.0	.1	.3	.4	.5	.5	.3	.4
15.	.0	.1	.3	.4	.5	.5	.3	.3
20.	.0	.1	.3	.5	.5	.3	.3	.3
25.	.0	.3	.3	.6	.5	.2	.3	.5
30.	.1	.3	.3	.6	.5	.2	.3	.5
35.	.1	.3	.3	.6	.3	.2	.3	.5
40.	.1	.3	.4	.6	.2	.2	.4	.5
45.	.1	.3	.4	.6	.1	.3	.4	.4
50.	.1	.2	.4	.5	.1	.4	.4	.3
55.	.1	.2	.4	.4	.2	.4	.4	.2
60.	.1	.1	.3	.2	.3	.3	.4	.2
65.	.1	.1	.3	.3	.3	.3	.3	.1
70.	.1	.1	.3	.3	.4	.3	.3	.1
75.	.1	.1	.3	.2	.3	.3	.2	.1
80.	.1	.1	.2	.3	.3	.4	.3	.2
85.	.1	.1	.2	.3	.3	.4	.3	.2
90.	.2	.1	.1	.3	.3	.3	.3	.2
95.	.2	.0	.1	.2	.2	.3	.3	.2
100.	.2	.0	.0	.1	.1	.2	.2	.1
105.	.2	.0	.0	.1	.2	.2	.2	.1
110.	.2	.0	.0	.2	.2	.2	.2	.2
115.	.1	.0	.0	.2	.2	.2	.2	.3
120.	.1	.0	.0	.2	.2	.3	.2	.3
125.	.1	.0	.0	.2	.2	.3	.2	.3
130.	.1	.0	.1	.2	.2	.3	.2	.3
135.	.1	.0	.1	.1	.2	.3	.2	.3
140.	.1	.0	.1	.1	.3	.3	.3	.3
145.	.1	.0	.1	.1	.3	.4	.3	.3
150.	.2	.0	.1	.1	.3	.4	.3	.3
155.	.2	.0	.1	.1	.3	.3	.3	.3
160.	.2	.0	.0	.1	.2	.2	.3	.3
165.	.1	.0	.0	.1	.2	.2	.3	.3
170.	.1	.0	.0	.1	.2	.2	.3	.3
175.	.1	.0	.0	.0	.1	.2	.2	.2
180.	.1	.0	.0	.0	.1	.2	.2	.2
185.	.1	.0	.0	.0	.1	.1	.1	.1
190.	.1	.0	.0	.0	.0	.1	.1	.1
195.	.1	.0	.0	.0	.0	.1	.1	.1
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0
250.	.1	.0	.0	.0	.0	.0	.0	.0
255.	.1	.0	.0	.0	.0	.0	.0	.0
260.	.1	.0	.0	.0	.0	.0	.0	.0
265.	.2	.0	.0	.0	.0	.0	.0	.0
270.	.2	.0	.0	.0	.0	.0	.0	.0
275.	.2	.0	.0	.0	.0	.0	.0	.0
280.	.0	.0	.0	.0	.1	.0	.0	.0
285.	.0	.0	.0	.1	.2	.0	.0	.0
290.	.0	.0	.0	.1	.3	.0	.0	.0
295.	.0	.0	.0	.2	.3	.0	.0	.0
300.	.0	.1	.0	.3	.3	.0	.0	.0
305.	.0	.1	.2	.3	.3	.0	.0	.0
310.	.0	.1	.2	.3	.3	.0	.0	.0
315.	.0	.1	.2	.3	.3	.0	.0	.0
320.	.0	.2	.2	.3	.4	.0	.0	.0
325.	.0	.2	.2	.3	.4	.1	.0	.0
330.	.0	.2	.2	.3	.3	.1	.0	.0
335.	.0	.2	.2	.3	.3	.1	.0	.0
340.	.0	.2	.2	.3	.3	.0	.0	.0
345.	.0	.2	.2	.3	.4	.1	.1	.1
350.	.0	.2	.2	.3	.4	.2	.2	.1
355.	.0	.2	.2	.3	.5	.3	.2	.2
360.	.0	.2	.2	.4	.5	.3	.3	.3
MAX	.2	.3	.4	.6	.5	.5	.4	.5
DEGR.	90	25	40	25	0	10	40	25

THE HIGHEST CONCENTRATION IS .90 PPM AT 15 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 20 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS .80 PPM AT 10 DEGREES FROM REC17.

```
Site 4 Bev & La Ci (S4EXWPPM.DAT)       60.0321.0.0000.000280.30480000
1    1
SE MID S                   492.      301.       5.0
SE 164 S                   488.      448.       5.0
SE 82 S                    486.      530.       5.0
SE CNR                     491.      605.       5.0
SE 82 E                    564.      612.       5.0
SE 164 E                   646.      612.       5.0
SE MID E                   775.      615.       5.0
NE MID E                   767.      715.       5.0
NE 164 E                   637.      714.       5.0
NE 82 E                    555.      714.       5.0
NE CNR                     474.      717.       5.0
NE 82 N                    473.      796.       5.0
NE 164 N                   472.      877.       5.0
NE MID N                   474.      999.       5.0
NW MID N                   372.      996.       5.0
NW 164 N                   367.      884.       5.0
NW 82 N                    367.      803.       5.0
NW CNR                     365.      726.       5.0
NW 82 W                    287.      721.       5.0
NW 164 W                   206.      720.       5.0
NW MID W                    62.      720.       5.0
SW MID W                    56.      606.       5.0
SW 164 W                   209.      606.       5.0
SW 82 W                    289.      606.       5.0
SW CNR                     361.      601.       5.0
SW 82 S                    376.      526.       5.0
SW 164 S                   380.      445.       5.0
SW MID S                   385.      307.       5.0
Site 4 Existing WITH PROJ PM            33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1691 3.3   0  44
30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1691 3.3   0  44
30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1691 3.3   0  44
30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1333 3.3   0  44
30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.       0.  24   2
      120        70       2.0 1333   20.5 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.     104 3.3   0  32
30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.       0.  12   1
      120        63       2.0  104   20.5 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     254 3.3   0  44
30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.       0.  24   2
      120       110       2.0  254   20.5 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    1849 3.3   0  44
```

```
30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1130 3.3   0  44
30.
  1
WB        Bev T+R   AG   683.   690.   443.   689.     881 3.3   0  44
30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  881   20.5 1510 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     249 3.3   0  44
30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  249   20.5 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.     945 3.3   0  44
30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.     945 3.3   0  44
30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.     945 3.3   0  44
30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.     945 3.3   0  44
30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1784 3.3   0  56
30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1273 3.3   0  44
30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        80       2.0 1273   20.5 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     422 3.3   0  32
30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        72       2.0  422   20.5 1117 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      89 3.3   0  32
30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        73       2.0   89   20.5  224 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1659 3.3   0  44
30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1117 3.3   0  44
30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1023 3.3   0  56
30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
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```
       120        80       2.0 1023   20.5 1449 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      94 3.3   0  32
30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        73       2.0   94   20.5  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1269 3.3   0  56
30.
1.0   04 1000.   0Y  5  0 72
```

JOB: Site 4 Bev & La Ci (S4EXWPPM.DAT) RUN: Site 4 Existing WITH PROJ PM
DATE: 07/13/2011 TIME: 13:27:11.21

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Bev AP	-543.0	891.0	-185.0	701.0	405.	118.	AG	1691.	3.3	.0	44.0		
2.	EB	Bev AP	-185.0	701.0	-55.0	655.0	138.	109.	AG	1691.	3.3	.0	44.0		
3.	EB	Bev AP	-55.0	655.0	123.0	646.0	178.	93.	AG	1691.	3.3	.0	44.0		
4.	EB	Bev THRU	124.0	641.0	417.0	641.0	293.	90.	AG	1333.	3.3	.0	44.0		
5.	EB	Bev THR Q	354.0	641.0	-613.1	641.0	967.	270.	AG	64.	100.0	.0	24.0	1.10	49.1
6.	EB	Bev RT	126.0	624.0	402.0	626.0	276.	90.	AG	104.	3.3	.0	32.0		
7.	EB	Bev RT Q	354.0	625.0	318.2	624.8	36.	270.	AG	29.	100.0	.0	12.0	.23	1.8
8.	EB	Bev LT	124.0	663.0	413.0	664.0	289.	90.	AG	254.	3.3	.0	44.0		
9.	EB	Bev LT Q	353.0	664.0	-296.6	661.0	650.	270.	AG	101.	100.0	.0	24.0	1.67	33.0
10.	EB	Bev DP	418.0	641.0	1427.0	656.0	1009.	89.	AG	1849.	3.3	.0	44.0		
11.	WB	Bev AP	683.0	689.0	1428.0	687.0	745.	90.	AG	1130.	3.3	.0	44.0		
12.	WB	Bev T+R	683.0	690.0	443.0	689.0	240.	270.	AG	881.	3.3	.0	44.0		
13.	WB	Bev T+R Q	495.0	689.0	663.4	689.9	168.	90.	AG	64.	100.0	.0	24.0	.76	8.6
14.	WB	Bev LT	685.0	667.0	445.0	665.0	240.	270.	AG	249.	3.3	.0	44.0		
15.	WB	Bev LT Q	499.0	666.0	1115.5	669.4	617.	90.	AG	101.	100.0	.0	24.0	1.63	31.3
16.	WB	Bev DP	442.0	689.0	75.0	687.0	367.	270.	AG	945.	3.3	.0	44.0		
17.	WB	Bev DP	75.0	687.0	-43.0	699.0	119.	276.	AG	945.	3.3	.0	44.0		
18.	WB	Bev DP	-43.0	699.0	-189.0	746.0	153.	288.	AG	945.	3.3	.0	44.0		
19.	WB	Bev DP	-189.0	746.0	-533.0	933.0	392.	299.	AG	945.	3.3	.0	44.0		
20.	NB	Cin AP	461.0	300.0	483.0	-335.0	635.	178.	AG	1784.	3.3	.0	56.0		
21.	NB	Cin THRU	456.0	301.0	445.0	652.0	351.	358.	AG	1273.	3.3	.0	44.0		
22.	NB	Cin THR Q	447.0	590.0	505.1	-1413.9	2005.	178.	AG	73.	100.0	.0	24.0	1.34	101.8
23.	NB	Cin RT	474.0	302.0	463.0	648.0	346.	358.	AG	422.	3.3	.0	32.0		
24.	NB	Cin RT Q	465.0	591.0	476.8	195.4	396.	178.	AG	33.	100.0	.0	12.0	1.03	20.1
25.	NB	Cin LT	438.0	301.0	430.0	652.0	351.	359.	AG	89.	3.3	.0	32.0		
26.	NB	Cin LT Q	431.0	589.0	434.8	416.2	173.	179.	AG	33.	100.0	.0	12.0	1.11	8.8
27.	NB	Cin DP	445.0	652.0	431.0	1659.0	1007.	359.	AG	1659.	3.3	.0	44.0		
28.	SB	Cin AP	406.0	1039.0	398.0	1660.0	621.	359.	AG	1117.	3.3	.0	44.0		
29.	SB	Cin T+R	401.0	1038.0	404.0	661.0	377.	180.	AG	1023.	3.3	.0	56.0		
30.	SB	Cin T+R Q	403.0	736.0	401.8	892.5	157.	360.	AG	110.	100.0	.0	36.0	.79	8.0
31.	SB	Cin LT	422.0	1036.0	424.0	666.0	370.	180.	AG	94.	3.3	.0	32.0		
32.	SB	Cin LT Q	424.0	735.0	420.6	1166.6	432.	360.	AG	33.	100.0	.0	12.0	1.57	21.9
33.	SB	Cin DP	404.0	662.0	437.0	-338.0	1001.	178.	AG	1269.	3.3	.0	56.0		

1

JOB: Site 4 Bev & La Ci (S4EXWPPM.DAT) RUN: Site 4 Existing WITH PROJ PM
DATE: 07/13/2011 TIME: 13:27:11.21

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5.	EB	Bev THR Q	120	70	2.0	1333	1584	20.50	1	3
7.	EB	Bev RT Q	120	63	2.0	104	1048	20.50	1	3
9.	EB	Bev LT Q	120	110	2.0	254	1536	20.50	1	3
13.	WB	Bev T+R Q	120	70	2.0	881	1510	20.50	1	3
15.	WB	Bev LT Q	120	110	2.0	249	1536	20.50	1	3
22.	NB	Cin THR Q	120	80	2.0	1273	1584	20.50	1	3
24.	NB	Cin RT Q	120	72	2.0	422	1117	20.50	1	3
26.	NB	Cin LT Q	120	73	2.0	89	224	20.50	1	3
30.	SB	Cin T+R Q	120	80	2.0	1023	1449	20.50	1	3
32.	SB	Cin LT Q	120	73	2.0	94	168	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	492.0	301.0	5.0
2.	SE 164 S	488.0	448.0	5.0
3.	SE 82 S	486.0	530.0	5.0
4.	SE CNR	491.0	605.0	5.0
5.	SE 82 E	564.0	612.0	5.0
6.	SE 164 E	646.0	612.0	5.0
7.	SE MID E	775.0	615.0	5.0
8.	NE MID E	767.0	715.0	5.0
9.	NE 164 E	637.0	714.0	5.0
10.	NE 82 E	555.0	714.0	5.0
11.	NE CNR	474.0	717.0	5.0
12.	NE 82 N	473.0	796.0	5.0
13.	NE 164 N	472.0	877.0	5.0
14.	NE MID N	474.0	999.0	5.0
15.	NW MID N	372.0	996.0	5.0
16.	NW 164 N	367.0	884.0	5.0
17.	NW 82 N	367.0	803.0	5.0
18.	NW CNR	365.0	726.0	5.0
19.	NW 82 W	287.0	721.0	5.0
20.	NW 164 W	206.0	720.0	5.0
21.	NW MID W	62.0	720.0	5.0
22.	SW MID W	56.0	606.0	5.0
23.	SW 164 W	209.0	606.0	5.0
24.	SW 82 W	289.0	606.0	5.0
25.	SW CNR	361.0	601.0	5.0
26.	SW 82 S	376.0	526.0	5.0
27.	SW 164 S	380.0	445.0	5.0
28.	SW MID S	385.0	307.0	5.0

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.4	.2	.2	.4	.5	.5	.5	.0	.0	.0	.2	.2	.2	.1	.2	.3	.3	.3	.0	.0
5.	.2	.2	.2	.4	.5	.5	.5	.0	.0	.0	.1	.1	.1	.1	.2	.3	.3	.4	.0	.0
10.	.0	.1	.2	.4	.5	.4	.5	.0	.0	.0	.1	.1	.1	.1	.3	.3	.3	.4	.0	.0
15.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.1	.1	.1	.0	.3	.2	.4	.4	.1	.0
20.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.4	.5	.1	.0
25.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.5	.6	.1	.0
30.	.0	.2	.2	.4	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.6	.6	.2	.0
35.	.1	.2	.2	.5	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.6	.5	.2	.0
40.	.1	.2	.2	.5	.5	.4	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.5	.5	.2	.0
45.	.0	.2	.2	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.3	.2	.5	.5	.2	.0
50.	.0	.2	.2	.5	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.2	.5	.4	.2	.1
55.	.0	.2	.2	.5	.4	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.2	.5	.4	.2	.1
60.	.0	.2	.2	.5	.4	.5	.5	.0	.0	.0	.0	.0	.0	.0	.2	.3	.5	.4	.2	.1
65.	.0	.2	.2	.4	.6	.5	.6	.0	.0	.0	.0	.0	.0	.0	.2	.3	.5	.4	.2	.1
70.	.0	.1	.2	.4	.6	.6	.6	.0	.0	.0	.0	.0	.0	.0	.2	.3	.5	.4	.2	.1
75.	.0	.0	.2	.4	.6	.6	.6	.1	.0	.0	.0	.0	.0	.0	.2	.3	.5	.3	.2	.1
80.	.0	.0	.2	.4	.6	.5	.4	.1	.2	.1	.1	.0	.0	.0	.2	.4	.5	.3	.2	.1
85.	.0	.0	.1	.3	.4	.4	.4	.2	.3	.5	.4	.0	.0	.0	.2	.4	.5	.4	.3	.1
90.	.0	.0	.0	.3	.3	.3	.3	.3	.3	.5	.4	.0	.0	.0	.2	.4	.5	.5	.3	.3
95.	.0	.0	.0	.2	.2	.2	.2	.4	.5	.6	.5	.0	.0	.0	.2	.4	.6	.5	.4	.3
100.	.0	.0	.0	.1	.1	.1	.1	.5	.5	.6	.5	.2	.0	.0	.2	.5	.7	.6	.3	.4
105.	.0	.0	.0	.0	.1	.1	.1	.5	.5	.7	.6	.2	.0	.0	.2	.5	.7	.6	.3	.4
110.	.0	.0	.0	.0	.0	.0	.0	.5	.5	.6	.6	.2	.1	.0	.2	.6	.7	.5	.3	.3
115.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.6	.2	.2	.0	.2	.7	.7	.5	.2	.3
120.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.6	.2	.2	.0	.2	.7	.7	.5	.3	.4
125.	.0	.0	.0	.0	.0	.0	.0	.5	.6	.6	.5	.3	.2	.0	.3	.7	.7	.4	.3	.5
130.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.5	.3	.2	.1	.4	.7	.7	.4	.3	.5
135.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.5	.3	.2	.1	.4	.6	.7	.3	.4	.5
140.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.4	.3	.1	.1	.4	.6	.6	.4	.5	.6
145.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.4	.3	.1	.1	.3	.5	.5	.5	.6	.6
150.	.0	.0	.0	.0	.0	.0	.0	.4	.5	.6	.4	.3	.1	.1	.4	.5	.4	.5	.6	.6
155.	.0	.0	.0	.0	.0	.0	.0	.4	.6	.6	.3	.3	.1	.0	.4	.5	.5	.5	.7	.6
160.	.1	.0	.0	.0	.0	.0	.0	.4	.6	.6	.3	.2	.1	.0	.4	.6	.4	.6	.7	.6
165.	.2	.1	.1	.0	.0	.0	.0	.4	.6	.6	.3	.2	.0	.0	.4	.5	.4	.5	.7	.6
170.	.2	.2	.1	.1	.0	.0	.0	.4	.6	.6	.4	.2	.2	.1	.4	.5	.4	.4	.7	.5
175.	.3	.3	.3	.1	.0	.0	.0	.4	.6	.6	.4	.3	.2	.2	.4	.4	.3	.4	.6	.5
180.	.4	.6	.7	.6	.1	.0	.0	.4	.6	.7	.6	.5	.3	.2	.3	.4	.3	.4	.5	.5
185.	.7	.7	.7	.6	.1	.1	.0	.4	.7	.7	.6	.5	.4	.4	.2	.2	.2	.5	.5	.5
190.	.7	.7	.7	.6	.2	.1	.0	.4	.7	.7	.6	.5	.4	.3	.2	.0	.1	.3	.5	.5
195.	.7	.7	.6	.6	.1	.1	.0	.4	.7	.8	.6	.4	.4	.4	.0	.1	.1	.4	.5	.5
200.	.7	.7	.6	.6	.2	.1	.0	.4	.7	.8	.6	.3	.4	.4	.0	.1	.1	.4	.5	.5
205.	.6	.6	.6	.6	.2	.1	.0	.4	.7	.9	.5	.2	.4	.5	.1	.1	.1	.4	.5	.5

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.6	.6	.6	.6	.2	.1	.0	.4	.7	.9	.5	.2	.4	.5	.1	.1	.2	.4	.5	.5
215.	.6	.6	.6	.5	.3	.1	.0	.4	.7	.9	.5	.3	.5	.5	.1	.1	.2	.5	.5	.5
220.	.6	.6	.6	.5	.3	.1	.0	.4	.7	.7	.4	.4	.6	.6	.1	.1	.2	.5	.5	.5
225.	.6	.6	.6	.4	.2	.1	.0	.4	.6	.5	.5	.5	.6	.5	.1	.1	.2	.5	.5	.4
230.	.6	.6	.6	.4	.2	.1	.0	.4	.6	.5	.5	.6	.6	.4	.1	.1	.2	.5	.5	.5
235.	.6	.5	.5	.3	.2	.1	.0	.4	.6	.5	.6	.6	.6	.4	.0	.1	.2	.5	.5	.5
240.	.6	.5	.5	.3	.2	.1	.0	.4	.6	.5	.6	.6	.6	.3	.0	.1	.2	.5	.5	.5
245.	.5	.5	.5	.3	.2	.0	.0	.4	.6	.3	.7	.7	.6	.3	.0	.1	.2	.5	.4	.5
250.	.5	.5	.5	.3	.2	.0	.0	.5	.5	.5	.7	.7	.6	.3	.0	.1	.2	.4	.4	.5
255.	.5	.5	.5	.3	.1	.0	.1	.5	.7	.6	.7	.7	.5	.3	.0	.0	.2	.4	.4	.5
260.	.5	.5	.5	.3	.1	.1	.1	.6	.6	.6	.7	.6	.5	.3	.0	.0	.1	.4	.4	.4
265.	.5	.5	.5	.5	.3	.2	.1	.6	.5	.6	.6	.6	.5	.3	.0	.0	.0	.3	.3	.3
270.	.6	.5	.5	.5	.3	.3	.4	.4	.4	.4	.6	.5	.4	.3	.0	.0	.0	.3	.3	.2
275.	.6	.5	.7	.5	.4	.4	.4	.0	.3	.3	.6	.5	.4	.3	.0	.0	.0	.1	.1	.1
280.	.6	.5	.7	.6	.5	.5	.4	.0	.1	.2	.5	.5	.4	.3	.0	.0	.0	.0	.0	.0
285.	.5	.5	.7	.6	.4	.4	.5	.0	.1	.2	.4	.5	.4	.2	.0	.0	.0	.0	.0	.0
290.	.5	.7	.7	.6	.3	.3	.5	.0	.1	.2	.4	.5	.4	.2	.0	.0	.0	.0	.0	.0
295.	.5	.7	.8	.6	.2	.3	.5	.0	.1	.2	.4	.5	.3	.2	.0	.0	.0	.0	.0	.0
300.	.5	.7	.8	.5	.4	.5	.5	.0	.1	.2	.4	.5	.3	.2	.0	.0	.0	.0	.0	.0
305.	.5	.8	.8	.3	.4	.5	.4	.0	.1	.2	.5	.5	.3	.2	.0	.0	.0	.0	.0	.0
310.	.6	.7	.7	.4	.5	.5	.4	.0	.1	.2	.5	.6	.4	.2	.0	.0	.0	.0	.0	.0
315.	.7	.7	.6	.4	.5	.7	.4	.0	.1	.2	.5	.5	.4	.3	.0	.0	.0	.0	.0	.0
320.	.6	.7	.5	.6	.6	.6	.5	.0	.1	.2	.6	.5	.4	.3	.0	.0	.0	.0	.0	.0
325.	.6	.6	.5	.5	.6	.6	.5	.0	.1	.1	.6	.5	.4	.3	.0	.0	.0	.0	.0	.0
330.	.6	.6	.4	.5	.7	.6	.5	.0	.1	.1	.6	.5	.4	.3	.0	.0	.0	.0	.0	.0
335.	.6	.6	.7	.5	.6	.6	.5	.0	.1	.1	.5	.5	.3	.3	.0	.0	.0	.0	.0	.0
340.	.6	.4	.7	.6	.6	.5	.5	.0	.0	.1	.6	.5	.3	.3	.0	.0	.0	.0	.0	.0
345.	.6	.5	.5	.5	.6	.5	.5	.0	.0	.1	.6	.4	.3	.3	.0	.0	.0	.0	.0	.0
350.	.4	.5	.5	.5	.6	.5	.5	.0	.0	.1	.3	.2	.3	.3	.0	.0	.0	.0	.0	.0
355.	.5	.5	.2	.3	.5	.5	.5	.0	.0	.1	.2	.2	.2	.3	.1	.0	.1	.2	.0	.0
360.	.4	.2	.2	.4	.5	.5	.5	.0	.0	.0	.2	.2	.2	.1	.2	.3	.3	.3	.0	.0
MAX	.7	.8	.8	.6	.7	.7	.6	.6	.7	.9	.7	.7	.6	.6	.4	.7	.7	.6	.7	.6
DEGR.	185	305	295	180	330	315	65	260	185	205	245	245	220	220	130	115	100	25	155	140

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.4	.4	.4	.5	.4	.2	.2
5.	.0	.4	.5	.4	.4	.4	.2	.3
10.	.0	.4	.5	.5	.4	.4	.3	.4
15.	.0	.4	.5	.7	.4	.3	.3	.4
20.	.0	.4	.5	.6	.4	.2	.5	.4
25.	.0	.4	.5	.6	.5	.2	.4	.4
30.	.0	.4	.5	.5	.5	.3	.4	.4
35.	.0	.4	.5	.5	.3	.3	.5	.4
40.	.0	.5	.7	.5	.3	.3	.6	.5
45.	.0	.6	.7	.5	.4	.4	.5	.4
50.	.0	.6	.7	.4	.4	.5	.5	.3
55.	.0	.6	.6	.4	.5	.5	.5	.3
60.	.0	.7	.4	.2	.4	.5	.5	.3
65.	.0	.7	.3	.4	.4	.5	.5	.3
70.	.0	.7	.3	.4	.4	.5	.5	.3
75.	.0	.5	.5	.3	.5	.5	.3	.3
80.	.0	.3	.5	.3	.5	.5	.3	.3
85.	.1	.5	.4	.4	.5	.4	.3	.3
90.	.2	.4	.3	.3	.4	.3	.3	.2
95.	.4	.2	.2	.3	.4	.3	.3	.3
100.	.3	.0	.0	.2	.4	.3	.3	.3
105.	.4	.0	.0	.1	.3	.3	.3	.3
110.	.5	.0	.0	.2	.3	.3	.3	.3
115.	.5	.0	.0	.2	.3	.3	.3	.3
120.	.5	.0	.0	.2	.3	.3	.3	.3
125.	.5	.0	.0	.2	.3	.3	.3	.3
130.	.5	.0	.1	.2	.3	.3	.3	.3
135.	.5	.0	.1	.2	.3	.3	.4	.4
140.	.5	.0	.1	.2	.3	.4	.4	.4
145.	.5	.0	.1	.2	.3	.4	.4	.4
150.	.5	.0	.1	.2	.3	.4	.5	.4
155.	.5	.0	.1	.2	.3	.4	.4	.4
160.	.5	.0	.1	.2	.4	.5	.4	.4
165.	.5	.0	.1	.2	.3	.4	.4	.4
170.	.5	.0	.0	.1	.3	.4	.4	.4
175.	.5	.0	.0	.1	.2	.4	.4	.4
180.	.5	.0	.0	.0	.2	.2	.4	.4
185.	.5	.0	.0	.0	.1	.2	.2	.2
190.	.5	.0	.0	.0	.0	.1	.1	.1
195.	.5	.0	.0	.0	.0	.0	.1	.1
200.	.5	.0	.0	.0	.0	.0	.0	.0
205.	.5	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.5	.0	.0	.0	.0	.0	.0	.0
215.	.5	.0	.0	.0	.0	.0	.0	.0
220.	.5	.0	.0	.0	.0	.0	.0	.0
225.	.5	.0	.0	.0	.0	.0	.0	.0
230.	.5	.0	.0	.0	.0	.0	.0	.0
235.	.5	.0	.0	.0	.0	.0	.0	.0
240.	.5	.0	.0	.0	.0	.0	.0	.0
245.	.5	.0	.0	.0	.0	.0	.0	.0
250.	.4	.0	.0	.0	.0	.0	.0	.0
255.	.5	.0	.0	.0	.0	.0	.0	.0
260.	.4	.1	.1	.1	.1	.0	.0	.0
265.	.3	.1	.2	.2	.2	.0	.0	.0
270.	.2	.2	.3	.3	.3	.0	.0	.0
275.	.0	.3	.4	.4	.4	.1	.0	.0
280.	.0	.3	.6	.5	.5	.2	.0	.0
285.	.0	.6	.6	.5	.5	.2	.0	.0
290.	.0	.6	.6	.5	.5	.2	.2	.0
295.	.0	.6	.6	.5	.5	.2	.2	.0
300.	.0	.6	.6	.5	.5	.2	.2	.0
305.	.0	.5	.5	.5	.6	.3	.2	.0
310.	.0	.5	.5	.6	.5	.3	.2	.0
315.	.0	.5	.5	.6	.5	.3	.2	.1
320.	.0	.5	.5	.6	.4	.3	.1	.1
325.	.0	.4	.4	.5	.4	.3	.1	.1
330.	.0	.4	.4	.4	.3	.3	.1	.0
335.	.0	.4	.4	.4	.3	.3	.1	.0
340.	.0	.4	.4	.4	.3	.2	.1	.0
345.	.0	.4	.5	.5	.3	.2	.1	.1
350.	.0	.4	.5	.5	.3	.2	.1	.1
355.	.0	.4	.4	.5	.4	.3	.1	.1
360.	.0	.4	.4	.4	.5	.4	.2	.2
MAX	.5	.7	.7	.7	.6	.5	.6	.5
DEGR.	110	60	40	15	305	50	40	40

THE HIGHEST CONCENTRATION IS .90 PPM AT 205 DEGREES FROM REC10.
THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 305 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .80 PPM AT 295 DEGREES FROM REC3 .

Site 5 – La Brea & Olympic
Input Files

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Site 5 Olymp & La Brea (S5EXAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Existing AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1183 3.3  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1183 3.3  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        65       2.0 1183   20.5 1108 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1220 3.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1542 3.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1542 3.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 1542   20.5 1103 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1679 3.3  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    1463 3.3  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    1463 3.3  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    1463 3.3  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1346 3.3  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1346 3.3  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1346   20.5 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     117 3.3  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     117 3.3  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        86       2.0  117   20.5 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    1452 3.3  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    1452 3.3  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    1452 3.3  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    1655 3.3  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    1536 3.3  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    1536 3.3  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        69       2.0 1536   20.5 1403 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     119 3.3  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     119 3.3  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        58       2.0  119   20.5  208 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    1492 3.3  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5EXPM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Existing PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1745 3.3  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1745 3.3  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        65       2.0 1745   20.5 1154 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1744 3.3  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1171 3.3  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1171 3.3  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 1171   20.5 1094 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1167 3.3  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    1547 3.3  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    1547 3.3  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    1547 3.3  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1494 3.3  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1494 3.3  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1494   20.5 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      53 3.3  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      53 3.3  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        90       2.0   53   20.5 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    1699 3.3  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    1699 3.3  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    1699 3.3  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    1845 3.3  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    1705 3.3  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    1705 3.3  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        65       2.0 1705   20.5 1411 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     140 3.3  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     140 3.3  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        53       2.0  140   20.5  180 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    1698 3.3  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5NBAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 No Build AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1574 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1574 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        66       2.0 1574   04.1 1112 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1611 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    2014 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    2014 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 2014   04.1 1105 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2122 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2059 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1961 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1961 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        69       2.0 1961   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      98 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      98 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0   98   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2119 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2322 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2165 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2165 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2165   04.1 1408 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     157 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     157 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  157   04.1  190 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2117 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5NBPM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 No Build PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2302 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2302 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        66       2.0 2302   04.1 1115 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2212 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1456 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1456 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        56       2.0 1456   04.1 1100 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1502 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2217 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2217 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2217 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2174 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2174 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2174   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      43 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      43 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   43   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2520 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2520 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2520 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2660 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2472 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2472 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        61       2.0 2472   04.1 1412 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     188 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     188 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  188   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2401 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M1AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 MOS 1 AM                          33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1576 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1576 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        66       2.0 1576   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1595 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1928 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1928 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 1928   04.1 1106 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2087 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2062 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2062 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2062 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1961 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1961 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1961   04.1 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     101 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     101 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0  101   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2113 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2113 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2113 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2347 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2200 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2200 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2200   04.1 1404 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     147 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     147 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  147   04.1  191 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2118 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M1PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 MOS 1 PM                          33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2330 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2330 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        65       2.0 2330   04.1 1113 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2181 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1459 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1459 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        56       2.0 1459   04.1 1098 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1529 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2190 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2190 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2190 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2143 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2143 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        64       2.0 2143   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      47 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      47 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   47   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2562 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2562 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2562 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2702 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2515 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2515 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2515   04.1 1411 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     187 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     187 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  187   04.1  161 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2409 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M2AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 MOS 2 AM                          33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1580 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1580 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        64       2.0 1580   04.1 1110 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1583 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1900 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1900 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        52       2.0 1900   04.1 1103 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2025 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2071 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2071 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2071 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1950 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1950 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1950   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     121 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     121 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        89       2.0  121   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2119 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2342 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2204 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2204 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        67       2.0 2204   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     138 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     138 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        58       2.0  138   04.1  196 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2166 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M2PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 MOS 2 PM                          33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2286 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2286 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        68       2.0 2286   04.1 1117 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2151 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1487 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1487 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        57       2.0 1487   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1533 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2206 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2206 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2206 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2161 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2161 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        64       2.0 2161   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      45 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      45 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   45   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2567 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2567 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2567 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2684 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2495 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2495 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        59       2.0 2495   04.1 1412 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     189 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     189 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        50       2.0  189   04.1  158 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2412 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B1AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 1 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1590 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1590 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        66       2.0 1590   04.1 1112 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1612 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1948 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1948 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        55       2.0 1948   04.1 1106 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2060 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2040 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2040 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2040 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1944 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1944 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1944   04.1 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      96 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      96 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0   96   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2107 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2107 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2107 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2343 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2185 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2185 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2185   04.1 1408 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     158 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     158 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  158   04.1  189 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2142 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B1PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 1 PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2260 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2260 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        65       2.0 2260   04.1 1115 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2168 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1438 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1438 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        56       2.0 1438   04.1 1099 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1541 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2204 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2204 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2204 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2163 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2163 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2163   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      41 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      41 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   41   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2518 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2518 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2518 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2672 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2483 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2483 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2483   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     189 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     189 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  189   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2347 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B2AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 2 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1548 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1548 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        66       2.0 1548   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1564 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1925 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1925 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 1925   04.1 1105 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2025 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2059 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1959 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1959 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1959   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     100 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     100 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0  100   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2119 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2326 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2184 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2184 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        67       2.0 2184   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     142 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     142 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        55       2.0  142   04.1  191 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2150 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B2PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 2 PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2284 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2284 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        67       2.0 2284   04.1 1117 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2172 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1465 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1465 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        56       2.0 1465   04.1 1100 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1487 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2140 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2140 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2140 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2098 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2098 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2098   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      42 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      42 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   42   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2479 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2479 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2479 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2654 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2470 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2470 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        61       2.0 2470   04.1 1414 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     184 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     184 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  184   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2405 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B3AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 3 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1555 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1555 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      101        67       2.0 1555   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1559 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1904 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1904 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      101        54       2.0 1904   04.1 1104 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2050 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2016 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2016 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2016 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1911 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1911 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       101        69       2.0 1911   04.1 1424 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     105 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     105 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       101        88       2.0  105   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2084 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2084 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2084 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2342 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2195 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2195 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       101        68       2.0 2195   04.1 1406 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     147 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     147 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       101        57       2.0  147   04.1  197 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2124 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B3PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 3 PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2253 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2253 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        68       2.0 2253   04.1 1121 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2174 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1458 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1458 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        56       2.0 1458   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1491 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2233 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2233 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2233 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2192 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2192 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2192   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      41 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      41 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   41   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2555 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2555 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2555 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2623 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2428 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2428 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2428   04.1 1411 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     195 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     195 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        50       2.0  195   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2347 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B4AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 4 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1578 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1578 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        62       2.0 1578   04.1 1106 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1606 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1912 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1912 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        50       2.0 1912   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2025 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2060 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2060 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2060 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1957 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1957 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1957   04.1 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     103 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     103 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        90       2.0  103   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2099 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2099 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2099 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2294 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2148 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2148 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        68       2.0 2148   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     146 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     146 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        60       2.0  146   04.1  202 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2114 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B4PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 4 PM                       33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2244 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2244 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        67       2.0 2244   04.1 1116 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2159 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1464 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1464 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        56       2.0 1464   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1507 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2251 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2251 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2251 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2208 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2208 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2208   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      43 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      43 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   43   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2548 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2548 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2548 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2648 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2466 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2466 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        61       2.0 2466   04.1 1413 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     182 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     182 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  182   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2393 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B5AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 5 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1549 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1549 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        66       2.0 1549   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1559 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1904 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1904 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 1904   04.1 1106 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2022 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2042 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2042 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2042 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1944 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1944 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        69       2.0 1944   04.1 1424 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      98 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      98 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0   98   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2105 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2105 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2105 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2303 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2153 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2153 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2153   04.1 1408 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     150 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     150 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  150   04.1  190 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2112 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

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Site 5 Olymp & La Brea (S5B5PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Build 5 PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2222 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2222 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        67       2.0 2222   04.1 1117 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2166 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1455 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1455 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        56       2.0 1455   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1515 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2226 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2226 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2226 0.8  0.  56   30.
  1
```

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NB        Brea T+R  AG   795.   760.   706.   856.    2196 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2196 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2196   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      30 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      30 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        93       2.0   30   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2530 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2530 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2530 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2640 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2446 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2446 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2446   04.1 1410 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     194 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     194 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  194   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2332 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

Site 5 – La Brea & Olympic
Output Files

JOB: Site 5 Olymp & La Brea (S5EXAM.DAT) RUN: Site 5 Existing AM
DATE: 03/19/2010 TIME: 10:04:28.84

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	1183.	3.3	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	1183.	3.3	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	415.4	1035.7	*	129.	272.	AG	143.	100.0	.0	48.0	.86	6.5
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	1220.	3.9	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1542.	3.9	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1542.	3.9	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	824.0	1060.9	*	129.	91.	AG	119.	100.0	.0	48.0	.83	6.6
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	1679.	3.3	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	1463.	3.3	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	1463.	3.3	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	1463.	3.3	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	1346.	3.3	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	1346.	3.3	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	955.7	264.3	*	768.	157.	AG	112.	100.0	.0	36.0	1.13	39.0
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	117.	3.3	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	117.	3.3	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	655.6	911.6	*	67.	156.	AG	47.	100.0	.0	12.0	.79	3.4
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	1452.	3.3	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	1452.	3.3	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	1452.	3.3	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	1655.	3.3	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	1536.	3.3	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	1536.	3.3	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	824.2	2743.7	*	1640.	8.	AG	114.	100.0	.0	36.0	1.35	83.3
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	119.	3.3	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	119.	3.3	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	687.0	1609.7	*	497.	8.	AG	32.	100.0	.0	12.0	1.51	25.3
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	1492.	3.3	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	1492.	3.3	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	1492.	3.3	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	1492.	3.3	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	1492.	3.3	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	1492.	3.3	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5EXAM.DAT) RUN: Site 5 Existing AM
DATE: 03/19/2010 TIME: 10:04:28.84

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	100	65	2.0	1183	1108	20.50	1	3
7.	WB Oly AP Q	*	100	54	2.0	1542	1103	20.50	1	3
14.	NB Brea T+R Q	*	100	68	2.0	1346	1423	20.50	1	3
17.	NB Brea LT Q	*	100	86	2.0	117	1490	20.50	1	3
24.	SB Brea T+R Q	*	100	69	2.0	1536	1403	20.50	1	3
27.	SB Brea LT Q	*	100	58	2.0	119	208	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

JOB: Site 5 Olymp & La Brea (S5EXAM.DAT) RUN: Site 5 Existing AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.3	.4	.5	.6	.4	.3	.0	.1	.3	.5	.6	.5	.4	1.0	.4	.2	.2	.0	.0
5.	.0	.2	.4	.5	.6	.3	.3	.0	.0	.2	.4	.5	.4	.5	1.0	.7	.3	.2	.1	.0
10.	.0	.1	.4	.5	.4	.2	.2	.0	.0	.0	.3	.4	.4	.4	1.1	.8	.7	.4	.1	.1
15.	.0	.0	.3	.4	.4	.2	.2	.0	.0	.0	.2	.4	.4	.3	1.0	.9	.7	.6	.1	.1
20.	.0	.0	.3	.4	.4	.3	.2	.0	.0	.0	.1	.2	.3	.3	1.0	1.0	.9	.7	.2	.1
25.	.0	.0	.3	.4	.3	.2	.2	.0	.0	.0	.0	.1	.1	.2	.9	1.1	.9	.7	.3	.1
30.	.0	.0	.3	.4	.3	.2	.2	.0	.0	.0	.0	.1	.1	.1	.8	1.0	1.0	.7	.3	.1
35.	.0	.0	.3	.4	.4	.3	.3	.0	.0	.0	.0	.0	.1	.1	.7	1.1	.9	.5	.4	.1
40.	.0	.0	.1	.4	.4	.3	.3	.0	.0	.0	.0	.0	.0	.1	.7	1.0	.8	.7	.3	.1
45.	.0	.0	.1	.5	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	1.0	.7	.6	.2	.1
50.	.0	.1	.1	.5	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.5	1.0	.7	.6	.1	.1
55.	.0	.2	.2	.4	.4	.3	.3	.0	.0	.0	.0	.0	.0	.0	.5	.9	.7	.4	.1	.1
60.	.0	.2	.2	.4	.4	.3	.3	.0	.0	.0	.0	.0	.0	.0	.5	.8	.5	.4	.2	.1
65.	.0	.0	.2	.4	.4	.3	.3	.1	.0	.0	.0	.0	.0	.0	.5	.7	.5	.4	.2	.1
70.	.0	.0	.2	.5	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.5	.7	.5	.4	.2	.2
75.	.0	.0	.2	.4	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.5	.7	.5	.2	.3	.2
80.	.0	.0	.1	.3	.3	.3	.3	.2	.2	.2	.1	.0	.0	.0	.4	.7	.5	.2	.2	.2
85.	.0	.0	.0	.3	.3	.3	.3	.2	.2	.2	.3	.0	.0	.0	.4	.7	.6	.4	.2	.1
90.	.0	.0	.0	.3	.3	.3	.3	.3	.3	.4	.3	.0	.0	.0	.4	.7	.6	.6	.4	.2
95.	.0	.0	.0	.1	.3	.2	.2	.4	.4	.5	.4	.0	.0	.0	.4	.7	.6	.8	.5	.3
100.	.0	.0	.0	.1	.1	.1	.1	.4	.4	.5	.6	.1	.0	.0	.4	.7	.7	.7	.5	.4
105.	.0	.0	.0	.1	.1	.1	.1	.4	.4	.6	.6	.1	.0	.0	.4	.7	.7	.7	.5	.6
110.	.0	.0	.0	.0	.1	.1	.1	.4	.4	.6	.7	.1	.0	.0	.4	.7	.9	.6	.5	.5
115.	.1	.0	.0	.0	.0	.0	.0	.4	.3	.6	.6	.2	.1	.0	.4	.6	.8	.6	.6	.5
120.	.1	.0	.0	.0	.0	.0	.0	.4	.3	.6	.6	.1	.1	.0	.4	.7	.8	.6	.5	.6
125.	.1	.1	.0	.0	.0	.0	.0	.4	.3	.6	.6	.2	.1	.0	.5	.7	.9	.6	.5	.6
130.	.2	.2	.0	.0	.0	.0	.0	.3	.3	.6	.6	.3	.0	.0	.5	.7	.8	.6	.5	.6
135.	.2	.2	.3	.0	.0	.0	.0	.3	.4	.6	.6	.3	.0	.0	.5	.8	.9	.6	.6	.6
140.	.2	.2	.3	.0	.0	.0	.0	.3	.3	.6	.6	.3	.0	.0	.5	.9	.9	.5	.6	.6
145.	.2	.4	.5	.1	.0	.0	.0	.3	.3	.6	.5	.3	.0	.0	.5	1.1	.8	.6	.6	.6
150.	.2	.4	.4	.1	.0	.0	.0	.3	.3	.6	.6	.2	.0	.0	.5	1.2	.7	.6	.6	.4
155.	.3	.4	.6	.2	.0	.0	.0	.3	.3	.6	.6	.3	.1	.0	.5	1.0	.7	.6	.6	.4
160.	.3	.5	.7	.4	.1	.0	.0	.3	.3	.7	.6	.3	.3	.0	.6	.9	.9	.6	.6	.4
165.	.4	.5	.8	.4	.1	.0	.0	.3	.3	.7	.6	.3	.3	.0	.8	.9	.6	.5	.6	.4
170.	.4	.5	.8	.4	.1	.1	.0	.3	.4	.7	.6	.3	.3	.1	.8	.8	.6	.5	.6	.3
175.	.4	.5	.7	.5	.1	.1	.0	.3	.4	.7	.7	.3	.3	.1	1.0	.8	.6	.5	.6	.3
180.	.4	.5	.8	.5	.1	.1	.0	.3	.4	.7	.6	.4	.3	.1	1.1	.7	.4	.4	.6	.3
185.	.5	.5	.8	.4	.1	.1	.0	.3	.4	.7	.5	.4	.1	.2	1.0	.6	.4	.4	.5	.3
190.	.5	.5	.7	.4	.1	.1	.1	.4	.4	.7	.5	.4	.1	.1	1.1	.6	.3	.5	.5	.3
195.	.4	.5	.7	.4	.1	.1	.1	.4	.5	.7	.5	.3	.1	.1	1.0	.6	.3	.5	.5	.3
200.	.4	.5	.7	.5	.1	.1	.1	.4	.5	.7	.5	.2	.2	.2	1.0	.5	.2	.5	.5	.2
205.	.4	.5	.7	.5	.1	.1	.1	.4	.5	.7	.4	.2	.2	.3	.8	.6	.2	.5	.5	.2

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WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.4	.4	.6	.5	.1	.1	.1	.4	.6	.7	.4	.2	.3	.3	.8	.3	.2	.5	.5	.3
215.	.4	.3	.6	.5	.1	.1	.1	.4	.6	.7	.2	.3	.3	.3	.7	.3	.2	.5	.4	.3
220.	.4	.4	.5	.5	.1	.1	.1	.4	.6	.7	.3	.4	.5	.3	.6	.2	.2	.5	.4	.3
225.	.4	.4	.5	.4	.1	.1	.1	.4	.7	.6	.3	.5	.6	.3	.6	.1	.2	.5	.4	.3
230.	.3	.4	.5	.4	.2	.1	.1	.4	.7	.6	.6	.6	.5	.3	.5	.1	.2	.5	.4	.3
235.	.3	.4	.5	.4	.2	.1	.1	.4	.6	.7	.6	.6	.6	.4	.5	.1	.1	.5	.3	.3
240.	.3	.4	.4	.4	.2	.1	.1	.4	.6	.7	.6	.6	.4	.4	.4	.1	.1	.5	.2	.3
245.	.3	.4	.5	.4	.2	.1	.1	.4	.6	.7	.6	.5	.5	.4	.4	.1	.1	.4	.4	.4
250.	.4	.4	.5	.3	.1	.1	.1	.5	.6	.7	.6	.5	.5	.4	.4	.1	.1	.4	.4	.4
255.	.4	.4	.5	.4	.1	.2	.2	.5	.7	.7	.7	.5	.4	.4	.4	.0	.1	.4	.4	.4
260.	.4	.4	.5	.4	.2	.2	.1	.5	.6	.7	.7	.5	.4	.4	.4	.0	.1	.4	.4	.4
265.	.4	.4	.5	.5	.2	.1	.1	.6	.5	.6	.5	.5	.4	.3	.4	.0	.1	.2	.4	.4
270.	.4	.4	.5	.4	.3	.2	.2	.5	.5	.5	.3	.4	.4	.3	.4	.0	.0	.2	.3	.3
275.	.4	.4	.5	.4	.3	.3	.5	.3	.4	.3	.4	.4	.4	.3	.4	.0	.0	.2	.2	.2
280.	.4	.4	.6	.6	.4	.5	.5	.2	.3	.3	.4	.5	.4	.4	.4	.0	.0	.1	.2	.2
285.	.4	.3	.8	.6	.5	.5	.4	.1	.3	.3	.4	.5	.4	.4	.4	.0	.0	.1	.1	.1
290.	.3	.4	.9	.6	.5	.5	.4	.2	.2	.2	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1
295.	.3	.6	.9	.6	.6	.4	.4	.1	.1	.1	.3	.4	.4	.4	.4	.0	.0	.0	.1	.1
300.	.3	.7	.9	.6	.6	.5	.4	.1	.1	.1	.4	.4	.4	.4	.4	.0	.0	.0	.0	.0
305.	.3	.6	.9	.4	.4	.6	.5	.1	.1	.1	.5	.4	.4	.3	.4	.0	.0	.0	.0	.0
310.	.3	.4	.9	.4	.5	.6	.5	.1	.1	.1	.5	.4	.4	.3	.4	.0	.0	.0	.0	.0
315.	.2	.4	.7	.5	.6	.6	.4	.1	.1	.1	.5	.4	.4	.3	.4	.0	.0	.0	.0	.0
320.	.2	.4	.5	.5	.6	.5	.4	.1	.1	.1	.4	.5	.4	.4	.5	.0	.0	.0	.0	.0
325.	.1	.4	.6	.4	.6	.5	.4	.1	.1	.1	.4	.5	.5	.5	.5	.0	.0	.0	.0	.0
330.	.1	.3	.5	.4	.5	.5	.4	.1	.1	.1	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0
335.	.1	.2	.5	.4	.5	.4	.3	.1	.1	.1	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
340.	.1	.1	.5	.4	.5	.4	.3	.1	.1	.2	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
345.	.1	.2	.6	.5	.5	.3	.3	.1	.1	.2	.3	.6	.5	.5	.7	.1	.0	.0	.0	.0
350.	.1	.2	.6	.6	.5	.3	.3	.1	.1	.3	.4	.5	.5	.5	.8	.2	.1	.0	.0	.0
355.	.1	.3	.4	.5	.6	.4	.3	.0	.1	.3	.5	.5	.5	.5	.9	.3	.1	.1	.0	.0
360.	.0	.3	.4	.5	.6	.4	.3	.0	.1	.3	.5	.6	.5	.4	1.0	.4	.2	.2	.0	.0
MAX DEGR.	.5 185	.7 300	.9 290	.6 280	.6 0	.6 305	.5 275	.6 265	.7 225	.7 160	.7 110	.6 0	.6 225	.5 5	1.1 10	1.2 150	1.0 30	.8 95	.6 115	.6 105

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.7	.5	.4	.3	.5
5.	.0	.2	.2	.7	.6	.4	.4	.6
10.	.0	.2	.4	.7	.7	.5	.4	.6
15.	.0	.2	.4	.8	.7	.4	.5	.5
20.	.0	.3	.4	.8	.7	.3	.3	.6
25.	.1	.3	.5	.8	.5	.4	.4	.6
30.	.1	.3	.5	.8	.4	.5	.5	.6
35.	.1	.3	.5	.7	.5	.5	.5	.6
40.	.1	.3	.6	.7	.4	.5	.4	.5
45.	.1	.3	.6	.7	.4	.6	.5	.4
50.	.1	.3	.6	.7	.4	.7	.6	.5
55.	.1	.3	.6	.6	.6	.7	.6	.4
60.	.1	.3	.6	.6	.6	.7	.6	.4
65.	.1	.2	.6	.7	.6	.6	.5	.3
70.	.2	.3	.6	.7	.6	.7	.3	.3
75.	.2	.3	.5	.7	.6	.7	.3	.4
80.	.1	.4	.5	.7	.7	.5	.3	.6
85.	.2	.4	.4	.5	.7	.5	.4	.6
90.	.2	.2	.4	.3	.4	.4	.4	.5
95.	.3	.2	.3	.3	.4	.4	.5	.6
100.	.4	.1	.3	.3	.4	.4	.5	.6
105.	.4	.0	.1	.1	.3	.4	.5	.6
110.	.5	.1	.1	.2	.3	.5	.5	.6
115.	.4	.1	.1	.2	.3	.4	.6	.6
120.	.4	.1	.1	.2	.4	.4	.5	.5
125.	.4	.1	.1	.2	.4	.4	.5	.5
130.	.4	.0	.1	.1	.4	.4	.5	.5
135.	.4	.0	.1	.1	.3	.4	.4	.4
140.	.3	.0	.1	.1	.3	.4	.4	.4
145.	.3	.0	.1	.1	.3	.4	.3	.4
150.	.3	.0	.0	.1	.3	.3	.2	.2
155.	.3	.0	.0	.0	.2	.2	.1	.2
160.	.3	.0	.0	.0	.2	.2	.1	.1
165.	.3	.0	.0	.0	.1	.0	.0	.1
170.	.3	.0	.0	.0	.0	.0	.0	.1
175.	.3	.0	.0	.0	.0	.0	.0	.0
180.	.3	.0	.0	.0	.0	.0	.0	.0
185.	.3	.0	.0	.0	.0	.0	.0	.0
190.	.3	.0	.0	.0	.0	.0	.0	.0
195.	.3	.0	.0	.0	.0	.0	.0	.0
200.	.3	.0	.0	.0	.0	.0	.0	.0
205.	.3	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.3	.0	.0	.0	.0	.0	.0	.0
215.	.3	.0	.0	.0	.0	.0	.0	.0
220.	.3	.0	.0	.0	.0	.0	.0	.0
225.	.3	.0	.0	.0	.0	.0	.0	.0
230.	.3	.0	.0	.0	.0	.0	.0	.0
235.	.3	.0	.0	.0	.0	.0	.0	.0
240.	.3	.0	.0	.0	.0	.0	.0	.0
245.	.4	.0	.0	.0	.0	.0	.0	.0
250.	.4	.0	.0	.0	.0	.0	.0	.0
255.	.4	.1	.0	.0	.0	.0	.0	.0
260.	.4	.1	.1	.0	.1	.0	.0	.0
265.	.4	.1	.1	.2	.2	.0	.0	.0
270.	.3	.1	.2	.4	.3	.0	.0	.0
275.	.2	.3	.2	.4	.5	.0	.0	.0
280.	.2	.3	.3	.4	.6	.0	.0	.0
285.	.1	.3	.3	.5	.5	.1	.0	.0
290.	.1	.3	.3	.5	.5	.1	.0	.0
295.	.1	.3	.3	.5	.6	.2	.0	.0
300.	.0	.3	.3	.5	.6	.2	.1	.0
305.	.0	.3	.3	.5	.6	.2	.1	.0
310.	.0	.3	.3	.6	.6	.3	.2	.1
315.	.0	.2	.3	.6	.5	.3	.1	.1
320.	.0	.2	.2	.6	.5	.3	.1	.1
325.	.0	.2	.2	.6	.5	.3	.1	.1
330.	.0	.2	.2	.6	.4	.3	.2	.2
335.	.0	.2	.2	.6	.4	.3	.2	.2
340.	.0	.2	.2	.6	.4	.4	.2	.4
345.	.0	.2	.2	.6	.3	.6	.2	.5
350.	.0	.2	.2	.6	.4	.5	.3	.5
355.	.0	.2	.2	.6	.4	.4	.3	.4
360.	.0	.2	.2	.7	.5	.4	.3	.5
MAX DEGR.	.5 (110)	.4 (80)	.6 (40)	.8 (15)	.7 (10)	.7 (50)	.6 (50)	.6 (5)

THE HIGHEST CONCENTRATION IS 1.20 PPM AT 150 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS 1.10 PPM AT 10 DEGREES FROM REC15.
THE 3RD HIGHEST CONCENTRATION IS 1.00 PPM AT 30 DEGREES FROM REC17.

JOB: Site 5 Olymp & La Brea (S5EXPM.DAT) RUN: Site 5 Existing PM
DATE: 03/19/2010 TIME: 10:21:35.12

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1745.	3.3	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1745.	3.3	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-500.7	1061.7	1045.	272.	AG	143.	100.0	.0	48.0	1.22	53.1
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1744.	3.3	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1171.	3.3	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1171.	3.3	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	781.2	1061.9	86.	91.	AG	119.	100.0	.0	48.0	.64	4.4
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	1167.	3.3	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	1547.	3.3	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	1547.	3.3	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	1547.	3.3	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1494.	3.3	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1494.	3.3	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	1159.0	-217.5	1291.	157.	AG	112.	100.0	.0	36.0	1.25	65.6
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	53.	3.3	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	53.	3.3	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	639.5	947.4	28.	156.	AG	49.	100.0	.0	12.0	.60	1.4
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	1699.	3.3	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	1699.	3.3	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	1699.	3.3	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	1845.	3.3	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	1705.	3.3	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	1705.	3.3	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	821.8	2727.1	1624.	8.	AG	107.	100.0	.0	36.0	1.30	82.5
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	140.	3.3	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	140.	3.3	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	722.5	1848.9	739.	8.	AG	29.	100.0	.0	12.0	1.82	37.5
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	1698.	3.3	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	1698.	3.3	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	1698.	3.3	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	1698.	3.3	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	1698.	3.3	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	1698.	3.3	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5EXPM.DAT) RUN: Site 5 Existing PM
DATE: 03/19/2010 TIME: 10:21:35.12

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	65	2.0	1745	1154	20.50	1	3
7.	WB Oly AP Q	100	54	2.0	1171	1094	20.50	1	3
14.	NB Brea T+R Q	100	68	2.0	1494	1422	20.50	1	3
17.	NB Brea LT Q	100	90	2.0	53	1490	20.50	1	3
24.	SB Brea T+R Q	100	65	2.0	1705	1411	20.50	1	3
27.	SB Brea LT Q	100	53	2.0	140	180	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

JOB: Site 5 Olymp & La Brea (S5EXPM.DAT) RUN: Site 5 Existing PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.2	.3	.6	.6	.3	.3	.0	.1	.3	.5	.6	.6	.5	1.0	.5	.2	.2	.0	.0
5.	* .0	.2	.3	.6	.5	.3	.3	.0	.0	.2	.4	.6	.5	.5	1.0	.7	.4	.3	.1	.0
10.	* .0	.1	.3	.6	.4	.3	.3	.0	.0	.1	.3	.4	.5	.5	1.0	.8	.7	.5	.1	.0
15.	* .0	.1	.2	.5	.3	.2	.3	.0	.0	.0	.3	.4	.4	.4	.9	.8	.8	.6	.1	.1
20.	* .0	.1	.2	.5	.3	.2	.3	.0	.0	.0	.1	.3	.3	.3	1.0	1.2	.8	.7	.1	.1
25.	* .0	.1	.1	.5	.3	.2	.3	.0	.0	.0	.1	.1	.2	.2	.9	1.2	.9	.8	.3	.1
30.	* .0	.1	.1	.5	.3	.3	.3	.0	.0	.0	.0	.1	.1	.1	.8	1.2	.8	.7	.4	.1
35.	* .0	.1	.1	.5	.3	.3	.3	.0	.0	.0	.0	.0	.1	.1	.7	1.0	.8	.6	.3	.1
40.	* .0	.1	.1	.5	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.7	1.0	.7	.7	.2	.1
45.	* .0	.1	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	1.0	.7	.7	.2	.1
50.	* .0	.1	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	1.0	.7	.6	.2	.1
55.	* .0	.1	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	.7	.6	.5	.2	.1
60.	* .0	.1	.1	.4	.2	.3	.3	.0	.0	.0	.0	.0	.0	.0	.5	.7	.7	.5	.2	.1
65.	* .0	.1	.1	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.5	.2	.1
70.	* .0	.1	.1	.2	.4	.4	.4	.1	.0	.0	.0	.0	.0	.0	.5	.7	.6	.4	.2	.1
75.	* .0	.0	.1	.2	.4	.4	.4	.1	.0	.0	.0	.0	.0	.0	.4	.7	.6	.3	.2	.2
80.	* .0	.0	.1	.3	.4	.4	.4	.1	.1	.1	.0	.0	.0	.0	.4	.7	.6	.3	.3	.2
85.	* .0	.0	.1	.2	.4	.4	.4	.1	.1	.2	.1	.0	.0	.0	.4	.7	.6	.3	.2	.1
90.	* .0	.0	.0	.2	.3	.3	.2	.3	.3	.3	.3	.0	.0	.0	.4	.7	.6	.5	.2	.2
95.	* .0	.0	.0	.1	.2	.2	.2	.3	.3	.3	.4	.0	.0	.0	.4	.7	.6	.7	.2	.3
100.	* .0	.0	.0	.1	.2	.2	.2	.3	.3	.3	.4	.0	.0	.0	.4	.7	.6	.7	.2	.5
105.	* .0	.0	.0	.1	.1	.1	.1	.3	.3	.3	.4	.1	.0	.0	.4	.7	.7	.7	.4	.5
110.	* .1	.0	.0	.0	.1	.1	.1	.3	.3	.3	.4	.1	.0	.0	.4	.7	.7	.7	.5	.5
115.	* .1	.0	.0	.0	.0	.0	.0	.3	.3	.3	.4	.1	.0	.0	.4	.8	.7	.6	.6	.5
120.	* .1	.0	.0	.0	.0	.0	.0	.3	.3	.3	.4	.1	.0	.0	.4	.8	.8	.5	.7	.6
125.	* .1	.1	.0	.0	.0	.0	.0	.3	.3	.3	.5	.1	.0	.0	.5	.8	.8	.4	.5	.6
130.	* .2	.2	.0	.0	.0	.0	.0	.3	.2	.3	.5	.1	.0	.0	.5	.8	1.0	.6	.4	.7
135.	* .2	.2	.3	.0	.0	.0	.0	.2	.2	.3	.5	.1	.0	.0	.5	.8	.8	.6	.5	.6
140.	* .2	.2	.3	.1	.0	.0	.0	.2	.2	.3	.4	.2	.0	.0	.5	.7	.8	.6	.5	.6
145.	* .2	.4	.5	.1	.0	.0	.0	.2	.2	.4	.4	.2	.0	.0	.5	.8	.8	.7	.5	.6
150.	* .2	.4	.6	.2	.0	.0	.0	.2	.2	.4	.5	.2	.0	.0	.5	1.0	.7	.6	.5	.6
155.	* .4	.5	.7	.2	.1	.0	.0	.2	.2	.5	.5	.3	.0	.0	.5	.9	.9	.6	.5	.5
160.	* .4	.5	.7	.4	.1	.0	.0	.2	.2	.5	.6	.3	.1	.0	.7	1.0	.8	.5	.6	.5
165.	* .4	.6	.8	.4	.1	.1	.0	.2	.3	.6	.5	.3	.2	.1	.7	1.0	.7	.5	.5	.5
170.	* .5	.6	.8	.5	.1	.1	.0	.2	.3	.6	.5	.3	.2	.1	.8	.9	.6	.4	.5	.5
175.	* .5	.6	.9	.5	.2	.1	.1	.3	.3	.6	.6	.3	.2	.1	1.0	.8	.5	.4	.5	.5
180.	* .5	.6	.8	.5	.2	.1	.1	.3	.3	.6	.5	.4	.1	.2	1.1	.7	.5	.3	.5	.5
185.	* .5	.6	.8	.5	.2	.1	.1	.3	.3	.6	.4	.3	.1	.2	1.0	.6	.6	.3	.5	.5
190.	* .5	.6	.7	.4	.2	.1	.1	.3	.3	.6	.4	.3	.1	.2	1.1	.6	.4	.4	.5	.5
195.	* .5	.6	.7	.4	.1	.1	.1	.3	.3	.6	.5	.2	.1	.1	1.1	.6	.4	.4	.5	.5
200.	* .5	.5	.7	.5	.1	.1	.1	.3	.3	.6	.6	.2	.2	.2	1.0	.5	.3	.4	.5	.6
205.	* .5	.5	.7	.5	.1	.1	.1	.3	.3	.6	.5	.2	.2	.3	1.0	.4	.3	.4	.5	.5

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JOB: Site 5 Olymp & La Brea (S5EXPM.DAT) RUN: Site 5 Existing PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .4	.4	.6	.5	.1	.1	.1	.3	.3	.6	.4	.2	.3	.3	.8	.3	.3	.4	.5	.5
215.	* .4	.5	.6	.5	.1	.1	.1	.3	.3	.6	.5	.5	.5	.4	.8	.2	.3	.4	.5	.5
220.	* .4	.5	.5	.5	.1	.1	.1	.3	.3	.6	.5	.5	.5	.5	.8	.2	.4	.4	.5	.5
225.	* .4	.5	.5	.4	.2	.1	.1	.3	.4	.5	.5	.6	.5	.5	.6	.1	.4	.5	.5	.5
230.	* .4	.5	.6	.4	.2	.1	.1	.3	.4	.6	.6	.7	.5	.6	.6	.1	.3	.5	.5	.5
235.	* .4	.5	.6	.4	.2	.1	.1	.3	.3	.6	.7	.7	.5	.5	.5	.1	.3	.5	.7	.6
240.	* .4	.5	.6	.4	.2	.1	.1	.2	.4	.7	.7	.7	.4	.5	.5	.1	.3	.5	.7	.6
245.	* .4	.4	.6	.4	.3	.1	.1	.2	.5	.8	.7	.7	.5	.5	.5	.1	.4	.6	.7	.6
250.	* .4	.4	.6	.3	.3	.1	.2	.3	.6	.6	.7	.7	.5	.5	.5	.1	.4	.7	.6	.6
255.	* .4	.4	.6	.5	.3	.2	.2	.4	.6	.8	.7	.8	.5	.5	.4	.1	.4	.7	.6	.6
260.	* .4	.5	.6	.5	.3	.3	.2	.5	.4	.8	.8	.6	.5	.4	.4	.1	.2	.6	.6	.6
265.	* .4	.5	.6	.7	.3	.2	.3	.5	.5	.7	.8	.6	.5	.4	.4	.1	.1	.5	.6	.6
270.	* .4	.5	.7	.6	.4	.3	.3	.3	.4	.6	.5	.6	.4	.4	.4	.0	.1	.4	.5	.5
275.	* .4	.6	.7	.8	.7	.3	.3	.3	.4	.5	.5	.5	.4	.4	.4	.0	.0	.2	.3	.3
280.	* .5	.6	.9	.8	.7	.4	.4	.2	.3	.4	.5	.5	.4	.4	.4	.0	.0	.2	.2	.2
285.	* .5	.6	.9	.7	.6	.4	.5	.0	.2	.1	.3	.5	.4	.4	.4	.0	.0	.1	.1	.1
290.	* .4	.6	.9	.7	.6	.6	.4	.0	.1	.1	.3	.5	.4	.4	.4	.0	.0	.0	.1	.1
295.	* .4	.7	1.0	.6	.6	.4	.4	.1	.1	.2	.4	.5	.4	.4	.4	.0	.0	.0	.0	.0
300.	* .4	.7	.9	.6	.5	.4	.3	.1	.1	.2	.4	.5	.4	.4	.4	.0	.0	.0	.0	.0
305.	* .4	.7	.9	.7	.5	.5	.2	.1	.1	.2	.4	.5	.4	.4	.4	.0	.0	.0	.0	.0
310.	* .4	.6	.9	.7	.5	.5	.3	.1	.1	.2	.4	.4	.5	.4	.4	.0	.0	.0	.0	.0
315.	* .3	.5	.8	.5	.6	.5	.4	.1	.1	.2	.5	.4	.5	.4	.4	.0	.0	.0	.0	.0
320.	* .2	.4	.6	.5	.6	.5	.4	.1	.1	.1	.5	.5	.5	.4	.4	.0	.0	.0	.0	.0
325.	* .1	.4	.6	.5	.6	.4	.4	.1	.1	.1	.4	.5	.5	.4	.5	.0	.0	.0	.0	.0
330.	* .0	.3	.6	.6	.6	.4	.4	.1	.1	.1	.4	.5	.5	.4	.5	.0	.0	.0	.0	.0
335.	* .1	.2	.6	.5	.6	.4	.4	.1	.2	.2	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
340.	* .1	.1	.5	.5	.6	.4	.4	.1	.2	.2	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
345.	* .1	.2	.5	.5	.6	.4	.4	.1	.2	.3	.3	.6	.5	.5	.6	.1	.0	.0	.0	.0
350.	* .1	.2	.5	.7	.6	.4	.3	.1	.2	.3	.4	.6	.5	.5	.7	.2	.1	.0	.0	.0
355.	* .1	.2	.4	.6	.6	.4	.3	.0	.1	.3	.5	.6	.5	.6	.9	.3	.1	.1	.0	.0
360.	* .0	.2	.3	.6	.6	.3	.3	.0	.1	.3	.5	.6	.6	.5	1.0	.5	.2	.2	.0	.0
MAX	* .5	.7	1.0	.8	.7	.6	.5	.5	.6	.8	.8	.8	.6	.6	1.1	1.2	1.0	.8	.7	.7
DEGR.	* 170	295	295	275	275	290	285	260	250	245	260	255	0	230	180	20	130	25	120	130

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JOB: Site 5 Olymp & La Brea (S5EXPM.DAT) RUN: Site 5 Existing PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.7	.7	.8	.6	.5	.3	.7
5.	.0	.7	.7	.8	.7	.6	.5	.6
10.	.0	.7	.8	.8	.7	.6	.6	.5
15.	.0	.7	.8	.9	.9	.6	.5	.6
20.	.0	.7	.8	.9	.8	.4	.4	.6
25.	.1	.8	.8	1.0	.7	.4	.5	.6
30.	.1	.8	.8	.9	.8	.4	.5	.6
35.	.1	.8	.8	.9	.6	.5	.5	.6
40.	.1	.8	.8	.8	.5	.6	.6	.6
45.	.1	.9	.8	.8	.5	.6	.6	.4
50.	.1	.9	.8	.8	.4	.6	.6	.5
55.	.1	.9	.9	.8	.6	.5	.6	.5
60.	.1	.9	.8	.6	.6	.5	.6	.5
65.	.1	.8	.7	.6	.6	.5	.5	.5
70.	.1	.9	.7	.8	.6	.6	.5	.4
75.	.2	.9	.7	.7	.7	.6	.4	.5
80.	.1	.9	.6	.6	.7	.6	.4	.6
85.	.1	.7	.6	.5	.5	.6	.5	.6
90.	.2	.7	.5	.3	.6	.5	.5	.5
95.	.4	.5	.3	.3	.6	.5	.5	.6
100.	.5	.3	.4	.3	.4	.5	.5	.6
105.	.5	.2	.3	.3	.4	.5	.5	.6
110.	.5	.2	.1	.2	.3	.5	.5	.7
115.	.7	.1	.1	.2	.3	.5	.6	.6
120.	.8	.1	.1	.2	.4	.5	.5	.5
125.	.7	.1	.1	.2	.4	.5	.5	.5
130.	.7	.1	.1	.1	.5	.5	.5	.5
135.	.6	.1	.1	.1	.5	.5	.5	.4
140.	.6	.0	.1	.1	.4	.5	.4	.4
145.	.5	.0	.1	.1	.3	.4	.3	.4
150.	.5	.0	.1	.1	.3	.4	.3	.3
155.	.5	.0	.0	.1	.2	.3	.2	.2
160.	.5	.0	.0	.0	.2	.2	.1	.2
165.	.5	.0	.0	.0	.2	.2	.1	.1
170.	.5	.0	.0	.0	.0	.0	.0	.1
175.	.5	.0	.0	.0	.0	.0	.0	.0
180.	.5	.0	.0	.0	.0	.0	.0	.0
185.	.5	.0	.0	.0	.0	.0	.0	.0
190.	.5	.0	.0	.0	.0	.0	.0	.0
195.	.5	.0	.0	.0	.0	.0	.0	.0
200.	.5	.0	.0	.0	.0	.0	.0	.0
205.	.5	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.5	.0	.0	.0	.0	.0	.0	.0
215.	.5	.0	.0	.0	.0	.0	.0	.0
220.	.5	.0	.0	.0	.0	.0	.0	.0
225.	.5	.0	.0	.0	.0	.0	.0	.0
230.	.5	.0	.0	.0	.0	.0	.0	.0
235.	.6	.0	.0	.0	.0	.0	.0	.0
240.	.6	.0	.0	.0	.0	.0	.0	.0
245.	.6	.0	.0	.0	.0	.0	.0	.0
250.	.6	.2	.1	.1	.0	.0	.0	.0
255.	.6	.2	.1	.1	.1	.0	.0	.0
260.	.6	.3	.3	.4	.3	.0	.0	.0
265.	.5	.5	.4	.5	.5	.0	.0	.0
270.	.5	.6	.7	.6	.6	.1	.0	.0
275.	.2	.8	.9	.8	.9	.1	.1	.0
280.	.2	1.0	.9	1.0	.9	.3	.1	.0
285.	.1	1.0	1.0	1.0	.9	.3	.1	.1
290.	.1	1.0	1.0	1.0	.8	.3	.1	.1
295.	.0	1.0	1.0	1.0	.8	.2	.1	.1
300.	.0	.9	.8	.8	.8	.3	.2	.1
305.	.0	.8	.8	.8	.7	.3	.1	.1
310.	.0	.8	.8	.8	.7	.3	.1	.2
315.	.0	.8	.8	.8	.6	.3	.1	.2
320.	.0	.8	.7	.7	.6	.3	.2	.2
325.	.0	.7	.6	.7	.6	.2	.3	.2
330.	.0	.7	.6	.7	.5	.2	.3	.5
335.	.0	.7	.7	.7	.5	.3	.3	.4
340.	.0	.7	.7	.7	.5	.3	.3	.4
345.	.0	.7	.7	.7	.4	.5	.3	.5
350.	.0	.7	.7	.7	.5	.4	.3	.6
355.	.0	.7	.7	.7	.6	.4	.3	.5
360.	.0	.7	.7	.8	.6	.5	.3	.7
MAX DEGR.	.8 120	1.0 280	1.0 285	1.0 25	.9 15	.6 5	.6 10	.7 110

THE HIGHEST CONCENTRATION IS 1.20 PPM AT 20 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS 1.10 PPM AT 180 DEGREES FROM REC15.
THE 3RD HIGHEST CONCENTRATION IS 1.00 PPM AT 25 DEGREES FROM REC24.

JOB: Site 5 Olymp & La Brea (S5NBAM.DAT) RUN: Site 5 No Build AM
DATE: 03/19/2010 TIME: 10:48:39.32

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1574.	.8	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1574.	.8	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-293.1	1055.8	837.	272.	AG	29.	100.0	.0	48.0	1.18	42.5
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1611.	.9	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	2014.	.9	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	2014.	.9	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	1341.2	1048.5	646.	91.	AG	24.	100.0	.0	48.0	1.08	32.8
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	2122.	.8	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2059.	.8	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2059.	.8	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2059.	.8	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1961.	.8	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1961.	.8	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	1845.4	-1844.0	3056.	157.	AG	23.	100.0	.0	36.0	1.70	155.3
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	98.	.8	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	98.	.8	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	653.7	915.8	63.	156.	AG	10.	100.0	.0	12.0	.82	3.2
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2119.	.8	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2119.	.8	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2119.	.8	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2322.	.8	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2165.	.8	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2165.	.8	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	1071.7	4459.6	3374.	8.	AG	22.	100.0	.0	36.0	1.71	171.4
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	157.	.8	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	157.	.8	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	746.3	2008.9	901.	8.	AG	6.	100.0	.0	12.0	1.99	45.8
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2117.	.8	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2117.	.8	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2117.	.8	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2117.	.8	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2117.	.8	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2117.	.8	.0	56.0		

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JOB: Site 5 Olymp & La Brea (S5NBAM.DAT) RUN: Site 5 No Build AM
DATE: 03/19/2010 TIME: 10:48:39.32

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	66	2.0	1574	1112	4.10	1	3
7.	WB Oly AP Q	100	54	2.0	2014	1105	4.10	1	3
14.	NB Brea T+R Q	100	69	2.0	1961	1423	4.10	1	3
17.	NB Brea LT Q	100	88	2.0	98	1490	4.10	1	3
24.	SB Brea T+R Q	100	66	2.0	2165	1408	4.10	1	3
27.	SB Brea LT Q	100	54	2.0	157	190	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

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JOB: Site 5 Olymp & La Brea (S5NBAM.DAT) RUN: Site 5 No Build AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.1	.1	.2
135.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.1	.1	.2
140.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.1	.2	.1	.1	.2
145.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.1	.1	.2
150.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
155.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.1	.1	.2	.0	.2	.2
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.2	.0	.2	.2
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.1	.0	.2	.2
170.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
175.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
180.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.1	.2	.2
185.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.1	.2	.2
190.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
195.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.0	.0	.2	.2
200.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.1	.1	.1	.0	.0	.2	.2
205.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.1	.1	.0	.0	.0	.2	.2

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JOB: Site 5 Olymp & La Brea (S5NBAM.DAT) RUN: Site 5 No Build AM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
215.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.1	.2	.2
220.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
225.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
250.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
255.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
260.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1
285.	.1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.0	.0	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX DEGR.	.1 130	.2 175	.2 235	.1 55	.2 60	.2 60	.1 45	.2 90	.2 90	.2 100	.2 100	.1 0	.1 0	.1 0	.3 10	.2 30	.2 75	.2 35	.2 155	.2 130

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JOB: Site 5 Olymp & La Brea (S5NBAM.DAT) RUN: Site 5 No Build AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.0	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.0	.0	.1	.1
20.	.0	.1	.1	.1	.0	.1	.0	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.0	.1	.0	.1
35.	.0	.1	.1	.1	.1	.1	.0	.1
40.	.0	.1	.1	.1	.0	.0	.0	.1
45.	.0	.1	.1	.1	.0	.0	.0	.1
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.1
60.	.0	.1	.1	.1	.0	.1	.0	.1
65.	.0	.1	.1	.1	.0	.1	.0	.0
70.	.0	.1	.1	.1	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.2
80.	.0	.1	.1	.0	.0	.1	.0	.2
85.	.1	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.2
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.0	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.2	.0	.0	.0	.0	.0	.0	.0
165.	.2	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.2	.0	.0	.0	.0	.0	.0	.0
190.	.2	.0	.0	.0	.0	.0	.0	.0
195.	.2	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

1

JOB: Site 5 Olymp & La Brea (S5NBAM.DAT) RUN: Site 5 No Build AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.1	.1	.1	.1	.1	.0	.0	.0
270.	.1	.1	.1	.1	.1	.0	.0	.0
275.	.1	.2	.1	.1	.1	.0	.0	.0
280.	.1	.2	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX	.2	.2	.1	.1	.1	.1	.1	.2
DEGR.	115	275	0	0	10	20	0	75

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 175 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 235 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5NBPM.DAT) RUN: Site 5 No Build PM
DATE: 03/19/2010 TIME: 10:59:15.30

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	2302.	.8	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	2302.	.8	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	-2188.0	1109.6	*	2733.	272.	AG	29.	100.0	.0	48.0	1.72	138.8
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	2212.	.8	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1456.	.8	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1456.	.8	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	821.3	1061.0	*	126.	91.	AG	25.	100.0	.0	48.0	.83	6.4
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	1502.	.8	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	2217.	.8	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	2217.	.8	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	2217.	.8	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	2174.	.8	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	2174.	.8	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	2078.0	-2395.2	*	3655.	157.	AG	22.	100.0	.0	36.0	1.82	185.7
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	43.	.8	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	43.	.8	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	639.6	947.2	*	28.	156.	AG	10.	100.0	.0	12.0	.73	1.4
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	2520.	.8	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	2520.	.8	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	2520.	.8	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	2660.	.8	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	2472.	.8	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	2472.	.8	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	1118.7	4785.7	*	3704.	8.	AG	20.	100.0	.0	36.0	1.67	188.1
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	188.	.8	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	188.	.8	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	794.5	2333.7	*	1229.	8.	AG	6.	100.0	.0	12.0	2.38	62.4
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	2401.	.8	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	2401.	.8	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	2401.	.8	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	2401.	.8	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	2401.	.8	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	2401.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5NBPM.DAT) RUN: Site 5 No Build PM
DATE: 03/19/2010 TIME: 10:59:15.30

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	100	66	2.0	2302	1115	4.10	1	3
7.	WB Oly AP Q	*	100	56	2.0	1456	1100	4.10	1	3
14.	NB Brea T+R Q	*	100	68	2.0	2174	1423	4.10	1	3
17.	NB Brea LT Q	*	100	92	2.0	43	1490	4.10	1	3
24.	SB Brea T+R Q	*	100	61	2.0	2472	1412	4.10	1	3
27.	SB Brea LT Q	*	100	51	2.0	188	176	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

JOB: Site 5 Olymp & La Brea (S5NBPM.DAT) RUN: Site 5 No Build PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.1	.0	.0
30.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.2	.1	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.0	.1
160.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.1	.0	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
190.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
195.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.1
200.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1
205.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1

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JOB: Site 5 Olymp & La Brea (S5NBPM.DAT) RUN: Site 5 No Build PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
225.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1	.1
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.2	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX DEGR.	.1 130	.2 165	.2 225	.2 190	.1 0	.1 0	.1 0	.1 90	.1 230	.1 120	.2 255	.1 0	.1 0	.1 0	.2 0	.3 25	.2 50	.2 30	.2 240	.2 240

1

JOB: Site 5 Olymp & La Brea (S5NBPM.DAT) RUN: Site 5 No Build PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.0	.1	.2
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.1	.1	.1	.1
20.	.0	.2	.2	.2	.2	.1	.1	.1
25.	.0	.2	.2	.2	.1	.1	.1	.1
30.	.0	.2	.2	.2	.2	.1	.0	.1
35.	.0	.2	.2	.2	.2	.1	.0	.1
40.	.0	.2	.2	.2	.1	.1	.0	.1
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.2
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.1	.2
85.	.0	.2	.2	.1	.1	.1	.1	.2
90.	.0	.1	.1	.0	.1	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.1	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.1	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.1	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.2	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.0	.0	.0
290.	.0	.2	.2	.2	.2	.0	.0	.0
295.	.0	.2	.1	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.2	.0	.0	.1
335.	.0	.2	.1	.2	.1	.0	.0	.1
340.	.0	.2	.2	.2	.1	.0	.0	.1
345.	.0	.2	.2	.2	.1	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 115	.2 0	.2 0	.2 0	.2 20	.1 10	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 165 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 225 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5M1AM.DAT) RUN: Site 5 MOS 1 AM
DATE: 03/19/2010 TIME: 11:22:51.01

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1576.	.8	.0	56.0		
2.	EB	Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1576.	.8	.0	68.0		
3.	EB	Oly AP Q	544.0	1032.0	-303.6	1056.1	848.	272.	AG	29.	100.0	.0	48.0	1.18	43.1
4.	EB	Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1595.	.9	.0	56.0		
5.	WB	Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1928.	.9	.0	56.0		
6.	WB	Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1928.	.9	.0	68.0		
7.	WB	Oly AP Q	695.0	1064.0	1123.6	1053.7	429.	91.	AG	24.	100.0	.0	48.0	1.04	21.8
8.	WB	Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	2087.	.8	.0	56.0		
9.	NB	Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2062.	.8	.0	56.0		
10.	NB	Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2062.	.8	.0	56.0		
11.	NB	Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2062.	.8	.0	56.0		
12.	NB	Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1961.	.8	.0	56.0		
13.	NB	Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1961.	.8	.0	56.0		
14.	NB	Brea T+R Q	657.0	972.0	1789.3	-1711.1	2912.	157.	AG	22.	100.0	.0	36.0	1.64	147.9
15.	NB	Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	101.	.8	.0	32.0		
16.	NB	Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	101.	.8	.0	32.0		
17.	NB	Brea LT Q	628.0	973.0	655.6	911.5	67.	156.	AG	10.	100.0	.0	12.0	.85	3.4
18.	NB	Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2113.	.8	.0	56.0		
19.	NB	Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2113.	.8	.0	56.0		
20.	NB	Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2113.	.8	.0	56.0		
21.	SB	Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2347.	.8	.0	56.0		
22.	SB	Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2200.	.8	.0	56.0		
23.	SB	Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2200.	.8	.0	56.0		
24.	SB	Brea T+R Q	590.0	1120.0	1091.0	4593.6	3510.	8.	AG	22.	100.0	.0	36.0	1.74	178.3
25.	SB	Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	147.	.8	.0	32.0		
26.	SB	Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	147.	.8	.0	32.0		
27.	SB	Brea LT Q	614.0	1118.0	729.1	1892.9	783.	8.	AG	6.	100.0	.0	12.0	1.84	39.8
28.	SB	Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2118.	.8	.0	56.0		
29.	SB	Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2118.	.8	.0	56.0		
30.	SB	Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2118.	.8	.0	56.0		
31.	SB	Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2118.	.8	.0	56.0		
32.	SB	Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2118.	.8	.0	56.0		
33.	SB	Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2118.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5M1AM.DAT) RUN: Site 5 MOS 1 AM
DATE: 03/19/2010 TIME: 11:22:51.01

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB	Oly AP Q	100	66	2.0	1576	1111	4.10	1	3
7.	WB	Oly AP Q	100	54	2.0	1928	1106	4.10	1	3
14.	NB	Brea T+R Q	100	68	2.0	1961	1422	4.10	1	3
17.	NB	Brea LT Q	100	88	2.0	101	1490	4.10	1	3
24.	SB	Brea T+R Q	100	66	2.0	2200	1404	4.10	1	3
27.	SB	Brea LT Q	100	54	2.0	147	191	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

JOB: Site 5 Olymp & La Brea (S5M1AM.DAT) RUN: Site 5 MOS 1 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
135.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.1	.1	.2
140.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.1	.2	.1	.1	.2
145.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
150.	.1	.0	.1	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
155.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.2	.0	.2	.2
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.2	.0	.2	.2
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.2
170.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
175.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
180.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.1	.2	.2
185.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
190.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
195.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.0	.0	.2	.2
200.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.0	.0	.0	.2	.2
205.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.0	.0	.0	.2	.2

1

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
215.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.1	.2	.2
220.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
225.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
250.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
255.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
260.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.1	.0	.0	.0	.0	.1	.2	.0	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1
285.	.1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.0	.0	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX DEGR.	.1	.2	.2	.1	.1	.1	.1	.2	.2	.2	.2	.1	.1	.1	.3	.2	.2	.2	.2	.2
	130	175	235	55	45	45	45	95	95	100	100	0	0	0	10	30	70	35	155	130

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.0	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.0	.0	.1	.1
20.	.0	.1	.1	.1	.0	.1	.0	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.0	.1	.0	.1
35.	.0	.1	.1	.1	.1	.1	.0	.1
40.	.0	.1	.1	.1	.0	.0	.0	.1
45.	.0	.1	.1	.1	.0	.0	.0	.0
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.0
60.	.0	.1	.1	.1	.0	.1	.0	.0
65.	.0	.1	.1	.1	.0	.1	.0	.0
70.	.0	.1	.1	.1	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.1
80.	.0	.1	.1	.0	.0	.1	.0	.2
85.	.1	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.1
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.0	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.2	.0	.0	.0	.0	.0	.0	.0
165.	.2	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.2	.0	.0	.0	.0	.0	.0	.0
190.	.2	.0	.0	.0	.0	.0	.0	.0
195.	.2	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.1	.1	.1	.1	.1	.0	.0	.0
270.	.1	.1	.1	.1	.1	.0	.0	.0
275.	.1	.2	.1	.1	.1	.0	.0	.0
280.	.0	.2	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX	.2	.2	.1	.1	.1	.1	.1	.2
DEGR.	115	275	0	0	10	20	0	80

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 175 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 235 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5M1PM.DAT) RUN: Site 5 MOS 1 PM
DATE: 03/19/2010 TIME: 11:57:35.38

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	2330.	.8	.0	56.0		
2.	EB	Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	2330.	.8	.0	68.0		
3.	EB	Oly AP Q	544.0	1032.0	-2147.3	1108.5	2692.	272.	AG	29.	100.0	.0	48.0	1.69	136.8
4.	EB	Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	2181.	.8	.0	56.0		
5.	WB	Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1459.	.8	.0	56.0		
6.	WB	Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1459.	.8	.0	68.0		
7.	WB	Oly AP Q	695.0	1064.0	821.7	1061.0	127.	91.	AG	25.	100.0	.0	48.0	.83	6.4
8.	WB	Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	1529.	.8	.0	56.0		
9.	NB	Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2190.	.8	.0	56.0		
10.	NB	Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2190.	.8	.0	56.0		
11.	NB	Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2190.	.8	.0	56.0		
12.	NB	Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	2143.	.8	.0	56.0		
13.	NB	Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	2143.	.8	.0	56.0		
14.	NB	Brea T+R Q	657.0	972.0	1808.8	-1757.2	2962.	157.	AG	21.	100.0	.0	36.0	1.57	150.5
15.	NB	Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	47.	.8	.0	32.0		
16.	NB	Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	47.	.8	.0	32.0		
17.	NB	Brea LT Q	628.0	973.0	642.1	941.6	34.	156.	AG	10.	100.0	.0	12.0	.80	1.7
18.	NB	Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2562.	.8	.0	56.0		
19.	NB	Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2562.	.8	.0	56.0		
20.	NB	Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2562.	.8	.0	56.0		
21.	SB	Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2702.	.8	.0	56.0		
22.	SB	Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2515.	.8	.0	56.0		
23.	SB	Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2515.	.8	.0	56.0		
24.	SB	Brea T+R Q	590.0	1120.0	1120.2	4796.2	3714.	8.	AG	20.	100.0	.0	36.0	1.65	188.7
25.	SB	Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	187.	.8	.0	32.0		
26.	SB	Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	187.	.8	.0	32.0		
27.	SB	Brea LT Q	614.0	1118.0	803.8	2396.1	1292.	8.	AG	6.	100.0	.0	12.0	2.60	65.6
28.	SB	Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2409.	.8	.0	56.0		
29.	SB	Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2409.	.8	.0	56.0		
30.	SB	Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2409.	.8	.0	56.0		
31.	SB	Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2409.	.8	.0	56.0		
32.	SB	Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2409.	.8	.0	56.0		
33.	SB	Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2409.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5M1PM.DAT) RUN: Site 5 MOS 1 PM
DATE: 03/19/2010 TIME: 11:57:35.38

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB	Oly AP Q	100	65	2.0	2330	1113	4.10	1	3
7.	WB	Oly AP Q	100	56	2.0	1459	1098	4.10	1	3
14.	NB	Brea T+R Q	100	64	2.0	2143	1423	4.10	1	3
17.	NB	Brea LT Q	100	92	2.0	47	1490	4.10	1	3
24.	SB	Brea T+R Q	100	60	2.0	2515	1411	4.10	1	3
27.	SB	Brea LT Q	100	51	2.0	187	161	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

JOB: Site 5 Olymp & La Brea (S5M1PM.DAT) RUN: Site 5 MOS 1 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
5.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.2	.0	.0
30.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.3	.1	.2	.0	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.1
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0	.1
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0	.1
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
160.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.1	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.1	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
190.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
195.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.0	.0	.0	.1	.1
200.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.0	.0	.0	.1	.1
205.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.0	.0	.0	.1	.1

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JOB: Site 5 Olymp & La Brea (S5M1PM.DAT) RUN: Site 5 MOS 1 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
225.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1	.2
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
MAX	.1	.2	.2	.2	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.2	.3	.2	.2	.2	.2
DEGR.	130	165	225	195	0	0	0	90	230	120	255	0	0	0	5	25	50	25	240	235

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JOB: Site 5 Olymp & La Brea (S5M1PM.DAT) RUN: Site 5 MOS 1 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.1	.1	.2
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.1	.1	.1	.1
20.	.0	.2	.2	.2	.2	.1	.1	.1
25.	.0	.2	.2	.2	.2	.1	.1	.1
30.	.0	.2	.2	.2	.2	.1	.0	.0
35.	.0	.2	.2	.2	.2	.1	.0	.0
40.	.0	.2	.2	.2	.2	.1	.0	.0
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.1
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.1	.1
85.	.0	.2	.2	.1	.1	.1	.1	.1
90.	.0	.1	.1	.0	.0	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.1
100.	.1	.0	.0	.0	.0	.1	.1	.1
105.	.1	.0	.0	.0	.0	.1	.1	.1
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.1	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.1	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 5 Olymp & La Brea (S5M1PM.DAT) RUN: Site 5 MOS 1 PM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.2	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.2	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.0	.0	.0
290.	.0	.2	.2	.2	.2	.0	.0	.0
295.	.0	.2	.2	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.1	.0	.0	.1
335.	.0	.2	.2	.2	.1	.0	.0	.1
340.	.0	.2	.2	.2	.1	.0	.0	.1
345.	.0	.2	.2	.2	.1	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 115	.2 0	.2 0	.2 0	.2 20	.1 5	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 165 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 225 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5M2AM.DAT) RUN: Site 5 MOS 2 AM
DATE: 03/19/2010 TIME: 12:16:43.70

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1580.	.8	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1580.	.8	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-90.0	1050.0	634.	272.	AG	28.	100.0	.0	48.0	1.11	32.2
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1583.	.9	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1900.	.9	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1900.	.9	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	917.8	1058.7	223.	91.	AG	23.	100.0	.0	48.0	.98	11.3
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	2025.	.8	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2071.	.8	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2071.	.8	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2071.	.8	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1950.	.8	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1950.	.8	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	1777.1	-1682.2	2881.	157.	AG	36.0	100.0	.0	36.0	1.63	146.3
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	121.	.8	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	121.	.8	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	744.5	713.7	284.	156.	AG	10.	100.0	.0	12.0	1.16	14.4
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2119.	.8	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2119.	.8	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2119.	.8	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2342.	.8	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2204.	.8	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2204.	.8	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	1111.7	4737.3	3655.	8.	AG	22.	100.0	.0	36.0	1.80	185.7
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	138.	.8	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	138.	.8	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	724.5	1862.2	752.	8.	AG	6.	100.0	.0	12.0	1.86	38.2
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2166.	.8	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2166.	.8	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2166.	.8	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2166.	.8	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2166.	.8	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2166.	.8	.0	56.0		

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JOB: Site 5 Olymp & La Brea (S5M2AM.DAT) RUN: Site 5 MOS 2 AM
DATE: 03/19/2010 TIME: 12:16:43.70

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	64	2.0	1580	1110	4.10	1	3
7.	WB Oly AP Q	100	52	2.0	1900	1103	4.10	1	3
14.	NB Brea T+R Q	100	68	2.0	1950	1423	4.10	1	3
17.	NB Brea LT Q	100	89	2.0	121	1490	4.10	1	3
24.	SB Brea T+R Q	100	67	2.0	2204	1409	4.10	1	3
27.	SB Brea LT Q	100	58	2.0	138	196	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

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JOB: Site 5 Olymp & La Brea (S5M2AM.DAT) RUN: Site 5 MOS 2 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
135.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
140.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.1	.2	.0	.1	.2
145.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
150.	.1	.0	.1	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.1	.1	.2	.0	.1	.2
155.	.1	.0	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.2	.0	.0	.2
160.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.1	.1	.2	.0	.0	.1
165.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
170.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.1	.2
175.	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
180.	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
185.	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
190.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
195.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1
200.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.1	.1
205.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
215.	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
220.	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.1	.1	.0	.0	.1	.2	.2
225.	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2	.1	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	.0	.0	.2	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	.0	.0	.2	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	.1	.0	.2	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
250.	.1	.0	.2	.0	.0	.0	.0	.1	.2	.1	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
255.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
260.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
265.	.1	.0	.1	.0	.0	.0	.0	.0	.2	.0	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX DEGR.	.1 130	.2 175	.2 235	.1 55	.1 45	.1 45	.1 45	.2 255	.2 160	.2 100	.2 105	.1 0	.1 0	.1 0	.3 10	.2 30	.2 70	.2 35	.2 175	.2 130

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.1	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.1	.1	.1	.1
20.	.0	.1	.1	.1	.0	.1	.1	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.1	.1	.0	.1
35.	.0	.1	.1	.1	.1	.1	.0	.1
40.	.0	.1	.1	.1	.1	.1	.0	.1
45.	.0	.1	.1	.1	.1	.0	.0	.0
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.0
60.	.0	.1	.1	.1	.0	.1	.0	.0
65.	.0	.1	.1	.1	.0	.1	.0	.1
70.	.0	.1	.1	.1	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.1
80.	.0	.1	.1	.0	.0	.1	.0	.2
85.	.0	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.1
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.2	.0	.0	.0	.0	.0	.0	.0
190.	.2	.0	.0	.0	.0	.0	.0	.0
195.	.2	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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JOB: Site 5 Olymp & La Brea (S5M2AM.DAT) RUN: Site 5 MOS 2 AM

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.1	.0	.0	.0	.0	.0	.0	.0
260.	.1	.0	.0	.0	.0	.0	.0	.0
265.	.1	.0	.0	.0	.0	.0	.0	.0
270.	.1	.1	.1	.1	.1	.0	.0	.0
275.	.1	.2	.1	.1	.1	.0	.0	.0
280.	.0	.2	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.0	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX	.2	.2	.1	.1	.1	.1	.1	.2
DEGR.	115	275	0	0	5	15	0	80

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 175 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 235 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5M2PM.DAT) RUN: Site 5 MOS 2 PM
DATE: 03/19/2010 TIME: 12:25:06.55

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	2286.	.8	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	2286.	.8	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-2374.1	1114.9	2919.	272.	AG	30.	100.0	.0	48.0	1.83	148.3
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	2151.	.8	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1487.	.8	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1487.	.8	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	835.2	1060.6	140.	91.	AG	25.	100.0	.0	48.0	.86	7.1
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	1533.	.8	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2206.	.8	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2206.	.8	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2206.	.8	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	2161.	.8	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	2161.	.8	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	1833.1	-1814.8	3025.	157.	AG	21.	100.0	.0	36.0	1.58	153.7
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	45.	.8	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	45.	.8	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	640.8	944.6	31.	156.	AG	10.	100.0	.0	12.0	.76	1.6
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2567.	.8	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2567.	.8	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2567.	.8	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2684.	.8	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2495.	.8	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2495.	.8	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	1087.7	4571.0	3487.	8.	AG	19.	100.0	.0	36.0	1.59	177.1
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	189.	.8	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	189.	.8	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	806.8	2416.3	1313.	8.	AG	5.	100.0	.0	12.0	2.63	66.7
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2412.	.8	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2412.	.8	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2412.	.8	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2412.	.8	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2412.	.8	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2412.	.8	.0	56.0		

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JOB: Site 5 Olymp & La Brea (S5M2PM.DAT) RUN: Site 5 MOS 2 PM
DATE: 03/19/2010 TIME: 12:25:06.55

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	68	2.0	2286	1117	4.10	1	3
7.	WB Oly AP Q	100	57	2.0	1487	1101	4.10	1	3
14.	NB Brea T+R Q	100	64	2.0	2161	1423	4.10	1	3
17.	NB Brea LT Q	100	92	2.0	45	1490	4.10	1	3
24.	SB Brea T+R Q	100	59	2.0	2495	1412	4.10	1	3
27.	SB Brea LT Q	100	50	2.0	189	158	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

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JOB: Site 5 Olymp & La Brea (S5M2PM.DAT) RUN: Site 5 MOS 2 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.2	.0	.0
30.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.2
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.1
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0	.1
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0	.1
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.1	.0	.1	.1
160.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.1	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
190.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
195.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.0	.0	.0	.1	.1
200.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.0	.0	.0	.1	.1
205.	.1	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.0	.0	.0	.1	.1

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JOB: Site 5 Olymp & La Brea (S5M2PM.DAT) RUN: Site 5 MOS 2 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
225.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1	.2
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.1	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
MAX	.1	.2	.2	.2	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.2	.3	.2	.2	.2	.2
DEGR.	130	165	225	190	0	0	0	90	210	110	255	0	0	0	10	25	50	25	240	125

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JOB: Site 5 Olymp & La Brea (S5M2PM.DAT) RUN: Site 5 MOS 2 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.1	.1	.2
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.1	.1	.1	.1
20.	.0	.2	.2	.2	.1	.1	.1	.1
25.	.0	.2	.2	.2	.1	.1	.1	.1
30.	.0	.2	.2	.2	.1	.1	.0	.0
35.	.0	.2	.2	.2	.1	.1	.0	.0
40.	.0	.2	.2	.2	.1	.1	.0	.0
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.1
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.1	.1
85.	.0	.2	.2	.0	.1	.1	.1	.1
90.	.0	.1	.1	.0	.0	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.1
100.	.1	.0	.0	.0	.0	.1	.1	.1
105.	.1	.0	.0	.0	.0	.1	.1	.1
110.	.2	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.1	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.1	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.1	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.2	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.1	.0	.0
290.	.0	.2	.2	.2	.2	.1	.0	.0
295.	.0	.2	.1	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.2	.0	.0	.1
335.	.0	.2	.1	.2	.1	.0	.0	.1
340.	.0	.2	.2	.2	.1	.0	.0	.1
345.	.0	.2	.2	.2	.1	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 110	.2 0	.2 0	.2 0	.2 275	.1 5	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 165 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 225 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B1AM.DAT) RUN: Site 5 Build 1 AM
DATE: 03/19/2010 TIME: 12:37:37.10

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1590.	.8	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1590.	.8	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-335.0	1057.0	879.	272.	AG	29.	100.0	.0	48.0	1.19	44.7
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1612.	.9	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1948.	.9	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1948.	.9	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	1287.6	1049.8	593.	91.	AG	24.	100.0	.0	48.0	1.08	30.1
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	2060.	.8	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2040.	.8	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2040.	.8	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2040.	.8	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1944.	.8	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1944.	.8	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	1769.0	-1662.9	2860.	157.	AG	22.	100.0	.0	36.0	1.63	145.3
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	96.	.8	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	96.	.8	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	652.5	918.4	60.	156.	AG	10.	100.0	.0	12.0	.81	3.0
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2107.	.8	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2107.	.8	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2107.	.8	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2343.	.8	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2185.	.8	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2185.	.8	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	1082.1	4532.0	3447.	8.	AG	22.	100.0	.0	36.0	1.73	175.1
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	158.	.8	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	158.	.8	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	747.9	2019.5	911.	8.	AG	6.	100.0	.0	12.0	2.00	46.3
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2142.	.8	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2142.	.8	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2142.	.8	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2142.	.8	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2142.	.8	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2142.	.8	.0	56.0		

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JOB: Site 5 Olymp & La Brea (S5B1AM.DAT) RUN: Site 5 Build 1 AM
DATE: 03/19/2010 TIME: 12:37:37.10

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	66	2.0	1590	1112	4.10	1	3
7.	WB Oly AP Q	100	55	2.0	1948	1106	4.10	1	3
14.	NB Brea T+R Q	100	68	2.0	1944	1422	4.10	1	3
17.	NB Brea LT Q	100	88	2.0	96	1490	4.10	1	3
24.	SB Brea T+R Q	100	66	2.0	2185	1408	4.10	1	3
27.	SB Brea LT Q	100	54	2.0	158	189	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

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MODEL RESULTS

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angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	* .0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	* .0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	* .0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	* .0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	* .0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
75.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	* .0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	* .0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	* .0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	* .0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	* .0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	* .0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
135.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
140.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.1	.2	.0	.1	.2
145.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
150.	* .1	.0	.1	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
155.	* .1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.2	.0	.2	.2
160.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.2	.0	.1	.2
165.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.1	.0	.1	.2
170.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
175.	* .1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
180.	* .1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
185.	* .1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
190.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
195.	* .0	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.0	.0	.2	.2
200.	* .0	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2
205.	* .0	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2

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JOB: Site 5 Olymp & La Brea (S5B1AM.DAT) RUN: Site 5 Build 1 AM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
215.	* .1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.1	.2	.2
220.	* .1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
225.	* .1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	* .0	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	* .0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	* .0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	* .0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
250.	* .1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
255.	* .1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
260.	* .1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
265.	* .1	.0	.1	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	* .1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	* .1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	* .1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1
285.	* .1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
305.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	* .0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	* .0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	* .0	.0	.2	.0	.0	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	* .0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
360.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX	* .1	.2	.2	.1	.2	.2	.1	.2	.2	.2	.2	.1	.1	.1	.3	.2	.2	.2	.2	.2
DEGR.	* 130	175	235	55	60	55	45	90	95	100	100	0	0	0	10	30	70	35	155	130

1

JOB: Site 5 Olymp & La Brea (S5B1AM.DAT) RUN: Site 5 Build 1 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.0	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.0	.1	.1	.1
20.	.0	.1	.1	.1	.0	.1	.0	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.1	.1	.0	.1
35.	.0	.1	.1	.1	.1	.1	.0	.1
40.	.0	.1	.1	.1	.1	.0	.0	.1
45.	.0	.1	.1	.1	.0	.0	.0	.0
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.0
60.	.0	.1	.1	.1	.0	.1	.0	.0
65.	.0	.1	.1	.1	.0	.1	.0	.0
70.	.0	.1	.1	.1	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.1
80.	.0	.1	.1	.0	.0	.1	.0	.2
85.	.1	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.1
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.2	.0	.0	.0	.0	.0	.0	.0
165.	.2	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.2	.0	.0	.0	.0	.0	.0	.0
190.	.2	.0	.0	.0	.0	.0	.0	.0
195.	.2	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.1	.1	.1	.1	.1	.0	.0	.0
270.	.1	.1	.1	.1	.1	.0	.0	.0
275.	.1	.2	.1	.1	.1	.0	.0	.0
280.	.0	.2	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX DEGR.	.2 115	.2 275	.1 0	.1 0	.1 10	.1 15	.1 0	.2 80

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 175 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 235 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B1PM.DAT) RUN: Site 5 Build 1 PM
DATE: 03/19/2010 TIME: 12:47:08.38

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION		LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB	Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	2260.	.8	.0	56.0		
2.	EB	Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	2260.	.8	.0	68.0		
3.	EB	Oly AP Q	544.0	1032.0	-1969.6	1103.4	2515.	272.	AG	29.	100.0	.0	48.0	1.64	127.7
4.	EB	Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	2168.	.8	.0	56.0		
5.	WB	Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1438.	.8	.0	56.0		
6.	WB	Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1438.	.8	.0	68.0		
7.	WB	Oly AP Q	695.0	1064.0	817.7	1061.1	123.	91.	AG	25.	100.0	.0	48.0	.82	6.2
8.	WB	Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	1541.	.8	.0	56.0		
9.	NB	Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2204.	.8	.0	56.0		
10.	NB	Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2204.	.8	.0	56.0		
11.	NB	Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2204.	.8	.0	56.0		
12.	NB	Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	2163.	.8	.0	56.0		
13.	NB	Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	2163.	.8	.0	56.0		
14.	NB	Brea T+R Q	657.0	972.0	2065.8	-2366.3	3623.	157.	AG	22.	100.0	.0	36.0	1.81	184.1
15.	NB	Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	41.	.8	.0	32.0		
16.	NB	Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	41.	.8	.0	32.0		
17.	NB	Brea LT Q	628.0	973.0	638.5	949.5	26.	156.	AG	10.	100.0	.0	12.0	.69	1.3
18.	NB	Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2518.	.8	.0	56.0		
19.	NB	Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2518.	.8	.0	56.0		
20.	NB	Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2518.	.8	.0	56.0		
21.	SB	Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2672.	.8	.0	56.0		
22.	SB	Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2483.	.8	.0	56.0		
23.	SB	Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2483.	.8	.0	56.0		
24.	SB	Brea T+R Q	590.0	1120.0	1103.9	4683.1	3600.	8.	AG	20.	100.0	.0	36.0	1.63	182.9
25.	SB	Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	189.	.8	.0	32.0		
26.	SB	Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	189.	.8	.0	32.0		
27.	SB	Brea LT Q	614.0	1118.0	796.1	2344.2	1240.	8.	AG	6.	100.0	.0	12.0	2.39	63.0
28.	SB	Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2347.	.8	.0	56.0		
29.	SB	Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2347.	.8	.0	56.0		
30.	SB	Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2347.	.8	.0	56.0		
31.	SB	Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2347.	.8	.0	56.0		
32.	SB	Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2347.	.8	.0	56.0		
33.	SB	Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2347.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5B1PM.DAT) RUN: Site 5 Build 1 PM
DATE: 03/19/2010 TIME: 12:47:08.38

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION		CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB	Oly AP Q	100	65	2.0	2260	1115	4.10	1	3
7.	WB	Oly AP Q	100	56	2.0	1438	1099	4.10	1	3
14.	NB	Brea T+R Q	100	68	2.0	2163	1423	4.10	1	3
17.	NB	Brea LT Q	100	92	2.0	41	1490	4.10	1	3
24.	SB	Brea T+R Q	100	60	2.0	2483	1409	4.10	1	3
27.	SB	Brea LT Q	100	51	2.0	189	176	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

JOB: Site 5 Olymp & La Brea (S5B1PM.DAT) RUN: Site 5 Build 1 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.2	.0	.0
30.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.1
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0	.1
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
160.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.1	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
190.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
195.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.0	.0	.0	.1	.1
200.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.0	.0	.0	.1	.1
205.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.0	.0	.0	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
225.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1	.2
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.2	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
MAX	.1	.2	.2	.2	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.2	.3	.2	.2	.2	.2
DEGR.	130	165	225	190	0	0	0	90	235	120	255	0	0	0	5	25	50	25	240	235

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.0	.1	.2
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.1	.1	.1	.1
20.	.0	.2	.2	.1	.0	.1	.1	.1
25.	.0	.2	.2	.2	.1	.1	.1	.1
30.	.0	.2	.2	.2	.1	.1	.0	.1
35.	.0	.2	.2	.2	.1	.1	.0	.1
40.	.0	.2	.2	.2	.1	.1	.0	.1
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.1
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.0	.2
85.	.0	.2	.2	.0	.1	.1	.1	.2
90.	.0	.1	.1	.0	.0	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.0	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.1	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.1	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.0	.0	.0
290.	.0	.2	.2	.2	.2	.0	.0	.0
295.	.0	.2	.1	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.1	.0	.0	.1
335.	.0	.2	.1	.2	.1	.0	.0	.1
340.	.0	.2	.2	.2	.0	.0	.0	.1
345.	.0	.2	.2	.2	.0	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 115	.2 0	.2 0	.2 0	.2 280	.1 10	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 165 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 225 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B2AM.DAT) RUN: Site 5 Build 2 AM
DATE: 03/19/2010 TIME: 12:56:42.57

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	1548.	.8	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	1548.	.8	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	-230.3	1054.0	*	775.	272.	AG	29.	100.0	.0	48.0	1.16	39.4
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	1564.	.9	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1925.	.9	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1925.	.9	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	1113.2	1054.0	*	418.	91.	AG	24.	100.0	.0	48.0	1.04	21.3
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	2025.	.8	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	2059.	.8	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	2059.	.8	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	2059.	.8	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	1959.	.8	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	1959.	.8	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	1789.3	-1711.1	*	2912.	157.	AG	22.	100.0	.0	36.0	1.64	147.9
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	100.	.8	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	100.	.8	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	654.9	913.0	*	66.	156.	AG	10.	100.0	.0	12.0	.84	3.3
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	2119.	.8	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	2119.	.8	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	2119.	.8	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	2326.	.8	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	2184.	.8	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	2184.	.8	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	1102.8	4675.2	*	3592.	8.	AG	22.	100.0	.0	36.0	1.78	182.5
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	142.	.8	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	142.	.8	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	724.4	1861.3	*	751.	8.	AG	6.	100.0	.0	12.0	1.82	38.2
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	2150.	.8	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	2150.	.8	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	2150.	.8	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	2150.	.8	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	2150.	.8	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	2150.	.8	.0	56.0		

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JOB: Site 5 Olymp & La Brea (S5B2AM.DAT) RUN: Site 5 Build 2 AM
DATE: 03/19/2010 TIME: 12:56:42.57

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	100	66	2.0	1548	1111	4.10	1	3
7.	WB Oly AP Q	*	100	54	2.0	1925	1105	4.10	1	3
14.	NB Brea T+R Q	*	100	68	2.0	1959	1423	4.10	1	3
17.	NB Brea LT Q	*	100	88	2.0	100	1490	4.10	1	3
24.	SB Brea T+R Q	*	100	67	2.0	2184	1409	4.10	1	3
27.	SB Brea LT Q	*	100	55	2.0	142	191	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

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JOB: Site 5 Olymp & La Brea (S5B2AM.DAT) RUN: Site 5 Build 2 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	.0	.0	.0	.0	.0	.1	.0	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
135.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
140.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.1	.2	.0	.1	.2
145.	.1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
150.	.1	.0	.1	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
155.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.2	.0	.1	.2
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.2	.0	.1	.1
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
170.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.1	.2
175.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
180.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
185.	.1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.2	.2
190.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
195.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1
200.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1
205.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
215.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
220.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
225.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
250.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
255.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
260.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.1	.0	.0	.0	.0	.1	.2	.0	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0
MAX DEGR.	.1 130	.2 175	.2 235	.1 60	.1 50	.1 45	.1 45	.2 100	.2 95	.2 100	.2 100	.1 0	.1 0	.1 0	.3 10	.2 30	.2 70	.2 35	.2 175	.2 130

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.1	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.1	.1	.1	.1
20.	.0	.1	.1	.1	.0	.1	.0	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.1	.1	.0	.1
35.	.0	.1	.1	.1	.1	.1	.0	.1
40.	.0	.1	.1	.1	.1	.1	.0	.1
45.	.0	.1	.1	.1	.0	.0	.0	.0
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.0
60.	.0	.1	.1	.1	.0	.1	.0	.0
65.	.0	.1	.1	.1	.0	.1	.0	.0
70.	.0	.1	.1	.1	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.1
80.	.0	.1	.1	.0	.0	.1	.0	.2
85.	.0	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.1
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.2	.0	.0	.0	.0	.0	.0	.0
190.	.2	.0	.0	.0	.0	.0	.0	.0
195.	.2	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.1	.0	.0	.0	.0	.0	.0	.0
265.	.1	.0	.0	.1	.0	.0	.0	.0
270.	.1	.1	.1	.1	.1	.0	.0	.0
275.	.1	.2	.1	.1	.1	.0	.0	.0
280.	.0	.2	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX	.2	.2	.1	.1	.1	.1	.1	.2
DEGR.	115	275	0	0	5	15	0	80

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 175 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 235 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B2PM.DAT) RUN: Site 5 Build 2 PM
DATE: 03/19/2010 TIME: 13:03:17.54

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	2284.	.8	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	2284.	.8	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	-2260.0	1111.7	*	2805.	272.	AG	29.	100.0	.0	48.0	1.77	142.5
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	2172.	.8	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1465.	.8	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1465.	.8	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	822.9	1060.9	*	128.	91.	AG	25.	100.0	.0	48.0	.83	6.5
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	1487.	.8	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	2140.	.8	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	2140.	.8	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	2140.	.8	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	2098.	.8	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	2098.	.8	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	1976.4	-2154.3	*	3393.	157.	AG	22.	100.0	.0	36.0	1.76	172.4
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	42.	.8	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	42.	.8	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	639.0	948.4	*	27.	156.	AG	10.	100.0	.0	12.0	.71	1.4
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	2479.	.8	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	2479.	.8	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	2479.	.8	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	2654.	.8	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	2470.	.8	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	2470.	.8	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	1117.2	4775.4	*	3693.	8.	AG	20.	100.0	.0	36.0	1.67	187.6
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	184.	.8	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	184.	.8	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	788.3	2291.4	*	1186.	8.	AG	6.	100.0	.0	12.0	2.33	60.3
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	2405.	.8	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	2405.	.8	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	2405.	.8	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	2405.	.8	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	2405.	.8	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	2405.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5B2PM.DAT) RUN: Site 5 Build 2 PM
DATE: 03/19/2010 TIME: 13:03:17.54

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	100	67	2.0	2284	1117	4.10	1	3
7.	WB Oly AP Q	*	100	56	2.0	1465	1100	4.10	1	3
14.	NB Brea T+R Q	*	100	68	2.0	2098	1423	4.10	1	3
17.	NB Brea LT Q	*	100	92	2.0	42	1490	4.10	1	3
24.	SB Brea T+R Q	*	100	61	2.0	2470	1414	4.10	1	3
27.	SB Brea LT Q	*	100	51	2.0	184	176	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

JOB: Site 5 Olymp & La Brea (S5B2PM.DAT) RUN: Site 5 Build 2 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.2	.1	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.2	.1	.0
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.2	.1	.0
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.2	.0	.1
160.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.1	.0	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.1
190.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.1
195.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.1	.1	.0	.0	.1
200.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.1
205.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.1

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JOB: Site 5 Olymp & La Brea (S5B2PM.DAT) RUN: Site 5 Build 2 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
225.	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.2	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0
MAX DEGR.	.1 130	.2 165	.2 230	.1 0	.1 0	.1 0	.1 0	.1 90	.1 225	.1 115	.2 255	.1 0	.1 0	.1 0	.2 0	.3 25	.2 50	.2 30	.2 240	.2 240

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JOB: Site 5 Olymp & La Brea (S5B2PM.DAT) RUN: Site 5 Build 2 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.0	.1	.2
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.1	.1	.1	.1
20.	.0	.2	.2	.2	.1	.1	.1	.1
25.	.0	.2	.2	.2	.1	.1	.1	.1
30.	.0	.2	.2	.2	.1	.1	.0	.1
35.	.0	.2	.2	.2	.1	.1	.0	.1
40.	.0	.2	.2	.2	.1	.1	.0	.1
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.2
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.1	.2
85.	.0	.2	.2	.0	.1	.1	.1	.2
90.	.0	.1	.1	.0	.0	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.2	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.1	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.1	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.1	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.2	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.0	.0	.0
290.	.0	.2	.2	.2	.2	.0	.0	.0
295.	.0	.2	.1	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.2	.0	.0	.1
335.	.0	.2	.1	.2	.1	.0	.0	.1
340.	.0	.2	.2	.2	.1	.0	.0	.1
345.	.0	.2	.2	.2	.1	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 110	.2 0	.2 0	.2 0	.2 275	.1 10	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 165 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 230 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B3AM.DAT) RUN: Site 5 Build 3 AM
DATE: 03/19/2010 TIME: 13:12:26.96

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	1555.	.8	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	1555.	.8	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	-272.9	1055.2	*	817.	272.	AG	29.	100.0	.0	48.0	1.18	41.5
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	1559.	.9	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1904.	.9	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1904.	.9	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	1001.7	1056.7	*	307.	91.	AG	24.	100.0	.0	48.0	1.01	15.6
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	2050.	.8	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	2016.	.8	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	2016.	.8	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	2016.	.8	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	1911.	.8	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	1911.	.8	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	1741.2	-1597.1	*	2788.	157.	AG	23.	100.0	.0	36.0	1.62	141.7
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	105.	.8	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	105.	.8	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	653.9	915.4	*	63.	156.	AG	10.	100.0	.0	12.0	.80	3.2
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	2084.	.8	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	2084.	.8	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	2084.	.8	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	2342.	.8	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	2195.	.8	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	2195.	.8	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	1115.0	4760.0	*	3678.	8.	AG	22.	100.0	.0	36.0	1.81	186.8
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	147.	.8	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	147.	.8	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	732.5	1915.8	*	807.	8.	AG	6.	100.0	.0	12.0	1.88	41.0
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	2124.	.8	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	2124.	.8	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	2124.	.8	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	2124.	.8	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	2124.	.8	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	2124.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5B3AM.DAT) RUN: Site 5 Build 3 AM
DATE: 03/19/2010 TIME: 13:12:26.96

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	101	67	2.0	1555	1111	4.10	1	3
7.	WB Oly AP Q	*	101	54	2.0	1904	1104	4.10	1	3
14.	NB Brea T+R Q	*	101	69	2.0	1911	1424	4.10	1	3
17.	NB Brea LT Q	*	101	88	2.0	105	1490	4.10	1	3
24.	SB Brea T+R Q	*	101	68	2.0	2195	1406	4.10	1	3
27.	SB Brea LT Q	*	101	57	2.0	147	197	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

JOB: Site 5 Olymp & La Brea (S5B3AM.DAT) RUN: Site 5 Build 3 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	.0	.0	.0	.0	.0	.1	.0	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
135.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
140.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.1	.2	.0	.1	.2
145.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
150.	.1	.0	.1	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.1	.1	.2	.0	.1	.2
155.	.1	.0	.1	.1	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0	.1	.1	.2	.0	.2	.2
160.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.2	.0	.1	.1
165.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.2
170.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
175.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
180.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
185.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
190.	.1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
195.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2
200.	.0	.1	.1	.1	.0	.0	.0	.2	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.1	.2
205.	.0	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.2

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
215.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
220.	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.1	.1	.0	.0	.0	.2	.2
225.	.1	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	.0	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	.0	.0	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	.0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
250.	.1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
255.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
260.	.1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
265.	.1	.0	.1	.0	.0	.0	.0	.1	.2	.0	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	.1	.0	.1	.0	.0	.0	.0	.1	.1	.0	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	.1	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	.1	.0	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1
285.	.1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX DEGR.	.1 130	.1 160	.2 240	.1 60	.1 50	.1 45	.1 45	.2 155	.2 100	.2 100	.2 105	.1 0	.1 0	.1 0	.3 10	.2 30	.2 70	.2 35	.2 155	.2 130

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.1	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.1	.0	.1	.1
20.	.0	.1	.1	.1	.0	.1	.0	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.0	.1	.0	.1
35.	.0	.1	.1	.1	.1	.1	.0	.1
40.	.0	.1	.1	.1	.0	.0	.0	.1
45.	.0	.1	.1	.1	.0	.0	.0	.1
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.1
60.	.0	.1	.1	.1	.0	.1	.0	.0
65.	.0	.1	.1	.1	.0	.1	.0	.0
70.	.0	.1	.1	.1	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.1
80.	.0	.1	.1	.0	.0	.1	.0	.2
85.	.1	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.2
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.0	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.2	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.2	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.2	.0	.0	.0	.0	.0	.0	.0
190.	.2	.0	.0	.0	.0	.0	.0	.0
195.	.2	.0	.0	.0	.0	.0	.0	.0
200.	.2	.0	.0	.0	.0	.0	.0	.0
205.	.2	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.1	.1	.1	.1	.1	.0	.0	.0
270.	.1	.1	.1	.1	.1	.0	.0	.0
275.	.1	.2	.1	.1	.1	.0	.0	.0
280.	.0	.2	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX DEGR.	.2 110	.2 275	.1 0	.1 0	.1 5	.1 20	.1 0	.2 80

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 240 DEGREES FROM REC3 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 155 DEGREES FROM REC8 .

JOB: Site 5 Olymp & La Brea (S5B3PM.DAT) RUN: Site 5 Build 3 PM
DATE: 03/19/2010 TIME: 13:32:02.42

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	2253.	.8	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	2253.	.8	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	-2280.1	1112.2	*	2825.	272.	AG	30.	100.0	.0	48.0	1.80	143.5
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	2174.	.8	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1458.	.8	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1458.	.8	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	821.3	1061.0	*	126.	91.	AG	25.	100.0	.0	48.0	.83	6.4
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	1491.	.8	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	2233.	.8	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	2233.	.8	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	2233.	.8	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	2192.	.8	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	2192.	.8	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	2102.4	-2453.0	*	3718.	157.	AG	22.	100.0	.0	36.0	1.83	188.8
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	41.	.8	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	41.	.8	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	638.5	949.5	*	26.	156.	AG	10.	100.0	.0	12.0	.69	1.3
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	2555.	.8	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	2555.	.8	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	2555.	.8	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	2623.	.8	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	2428.	.8	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	2428.	.8	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	1077.2	4498.1	*	3413.	8.	AG	20.	100.0	.0	36.0	1.60	173.4
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	195.	.8	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	195.	.8	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	803.8	2396.1	*	1292.	8.	AG	5.	100.0	.0	12.0	2.44	65.6
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	2347.	.8	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	2347.	.8	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	2347.	.8	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	2347.	.8	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	2347.	.8	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	2347.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5B3PM.DAT) RUN: Site 5 Build 3 PM
DATE: 03/19/2010 TIME: 13:32:02.42

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	100	68	2.0	2253	1121	4.10	1	3
7.	WB Oly AP Q	*	100	56	2.0	1458	1101	4.10	1	3
14.	NB Brea T+R Q	*	100	68	2.0	2192	1423	4.10	1	3
17.	NB Brea LT Q	*	100	92	2.0	41	1490	4.10	1	3
24.	SB Brea T+R Q	*	100	60	2.0	2428	1411	4.10	1	3
27.	SB Brea LT Q	*	100	50	2.0	195	176	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

JOB: Site 5 Olymp & La Brea (S5B3PM.DAT) RUN: Site 5 Build 3 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.2	.1	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.2	.0	.1
160.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.1	.0	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
190.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
195.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.1
200.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1
205.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1

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JOB: Site 5 Olymp & La Brea (S5B3PM.DAT) RUN: Site 5 Build 3 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
225.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1	.1
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.1	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.2	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
360.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
MAX	.1	.2	.2	.2	.1	.1	.1	.1	.1	.1	.2	.1	.1	.1	.2	.3	.2	.2	.2	.2
DEGR.	130	160	225	190	0	0	0	90	230	120	255	0	0	0	10	25	55	30	240	240

1

JOB: Site 5 Olymp & La Brea (S5B3PM.DAT) RUN: Site 5 Build 3 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.0	.1	.2
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.1	.1	.1	.1
20.	.0	.2	.2	.1	.0	.1	.1	.1
25.	.0	.2	.2	.2	.1	.1	.1	.1
30.	.0	.2	.2	.2	.1	.1	.0	.1
35.	.0	.2	.2	.2	.1	.1	.0	.1
40.	.0	.2	.2	.2	.1	.1	.0	.1
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.1
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.0	.2
85.	.0	.2	.2	.0	.1	.1	.1	.2
90.	.0	.1	.1	.0	.0	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.2	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.0	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.1	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.1	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.0	.0	.0
290.	.0	.2	.2	.2	.2	.1	.0	.0
295.	.0	.2	.1	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.2	.0	.0	.1
335.	.0	.2	.1	.2	.1	.0	.0	.1
340.	.0	.2	.2	.1	.0	.0	.0	.1
345.	.0	.2	.2	.1	.0	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 110	.2 0	.2 0	.2 0	.2 280	.1 10	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 160 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 225 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B4AM.DAT) RUN: Site 5 Build 4 AM
DATE: 03/19/2010 TIME: 14:33:37.21

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	1578.	.8	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	1578.	.8	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	134.3	1043.6	*	410.	272.	AG	27.	100.0	.0	48.0	1.05	20.8
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	1606.	.9	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1912.	.9	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1912.	.9	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	887.6	1059.4	*	193.	91.	AG	22.	100.0	.0	48.0	.94	9.8
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	2025.	.8	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	2060.	.8	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	2060.	.8	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	2060.	.8	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	1957.	.8	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	1957.	.8	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	1785.2	-1701.4	*	2902.	157.	AG	22.	100.0	.0	36.0	1.64	147.4
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	103.	.8	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	103.	.8	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	727.1	752.3	*	242.	156.	AG	10.	100.0	.0	12.0	1.16	12.3
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	2099.	.8	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	2099.	.8	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	2099.	.8	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	2294.	.8	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	2148.	.8	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	2148.	.8	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	1105.5	4694.4	*	3611.	8.	AG	22.	100.0	.0	36.0	1.82	183.5
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	146.	.8	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	146.	.8	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	740.4	1969.3	*	861.	8.	AG	7.	100.0	.0	12.0	2.03	43.7
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	2114.	.8	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	2114.	.8	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	2114.	.8	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	2114.	.8	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	2114.	.8	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	2114.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5B4AM.DAT) RUN: Site 5 Build 4 AM
DATE: 03/19/2010 TIME: 14:33:37.21

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	100	62	2.0	1578	1106	4.10	1	3
7.	WB Oly AP Q	*	100	50	2.0	1912	1101	4.10	1	3
14.	NB Brea T+R Q	*	100	68	2.0	1957	1422	4.10	1	3
17.	NB Brea LT Q	*	100	90	2.0	103	1490	4.10	1	3
24.	SB Brea T+R Q	*	100	68	2.0	2148	1409	4.10	1	3
27.	SB Brea LT Q	*	100	60	2.0	146	202	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

JOB: Site 5 Olymp & La Brea (S5B4AM.DAT) RUN: Site 5 Build 4 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	.1	.0	.0	.0	.0	.0	.0	.1	.0	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
135.	.1	.0	.0	.0	.0	.0	.0	.1	.0	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
140.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
145.	.1	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.1
150.	.1	.0	.1	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.1	.1	.2	.0	.1	.1
155.	.1	.0	.1	.1	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.1	.1	.2	.0	.0	.2
160.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.1	.1	.2	.0	.0	.1
165.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.1
170.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.0	.2
175.	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.1	.1
180.	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.1	.1
185.	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.2	.1	.0	.0	.1	.1
190.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.1	.2
195.	.0	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1
200.	.0	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1
205.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1

1

JOB: Site 5 Olymp & La Brea (S5B4AM.DAT) RUN: Site 5 Build 4 AM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.1	.2
215.	.1	.0	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
220.	.1	.1	.1	.1	.0	.0	.0	.1	.2	.2	.1	.0	.0	.1	.1	.0	.0	.1	.2	.2
225.	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	.1	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	.0	.0	.2	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	.0	.0	.2	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	.1	.0	.2	.0	.0	.0	.0	.1	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.1
250.	.1	.0	.2	.0	.0	.0	.0	.1	.2	.1	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
255.	.1	.0	.2	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
260.	.1	.0	.1	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
265.	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0
360.	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0
MAX DEGR.	.1 130	.2 175	.2 235	.1 55	.1 45	.1 45	.1 45	.1 85	.2 160	.2 105	.2 105	.1 0	.1 0	.1 0	.3 10	.2 30	.2 80	.2 35	.2 215	.2 135

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JOB: Site 5 Olymp & La Brea (S5B4AM.DAT) RUN: Site 5 Build 4 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.1	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.1	.0	.1	.1
20.	.0	.1	.1	.1	.0	.1	.0	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.0	.1	.0	.1
35.	.0	.1	.1	.1	.0	.1	.0	.1
40.	.0	.1	.1	.1	.0	.0	.0	.1
45.	.0	.1	.1	.1	.0	.0	.0	.0
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.0
60.	.0	.1	.1	.1	.0	.1	.0	.0
65.	.0	.1	.1	.1	.0	.1	.0	.0
70.	.0	.1	.1	.0	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.1
80.	.0	.1	.1	.0	.0	.1	.0	.2
85.	.0	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.1
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.0	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.0	.0	.0	.0	.0	.0	.0	.0
205.	.0	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0
240.	.1	.0	.0	.0	.0	.0	.0	.0
245.	.1	.0	.0	.0	.0	.0	.0	.0
250.	.1	.0	.0	.0	.0	.0	.0	.0
255.	.1	.0	.0	.0	.0	.0	.0	.0
260.	.1	.0	.0	.0	.0	.0	.0	.0
265.	.1	.0	.0	.0	.0	.0	.0	.0
270.	.1	.0	.0	.1	.1	.0	.0	.0
275.	.1	.1	.1	.1	.1	.0	.0	.0
280.	.0	.1	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.0	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX DEGR.	.2 115	.2 285	.1 0	.1 0	.1 5	.1 20	.1 0	.2 80

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 175 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 235 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B4PM.DAT) RUN: Site 5 Build 4 PM
DATE: 03/19/2010 TIME: 14:02:36.33

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	2244.	.8	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	2244.	.8	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-2155.3	1108.7	2700.	272.	AG	29.	100.0	.0	48.0	1.74	137.2
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	2159.	.8	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1464.	.8	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1464.	.8	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	822.9	1060.9	128.	91.	AG	25.	100.0	.0	48.0	.83	6.5
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	1507.	.8	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2251.	.8	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2251.	.8	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2251.	.8	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	2208.	.8	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	2208.	.8	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	2126.8	-2510.8	3780.	157.	AG	22.	100.0	.0	36.0	1.85	192.0
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	43.	.8	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	43.	.8	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	639.6	947.2	28.	156.	AG	10.	100.0	.0	12.0	.73	1.4
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2548.	.8	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2548.	.8	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2548.	.8	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2648.	.8	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2466.	.8	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2466.	.8	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	1115.7	4765.1	3683.	8.	AG	20.	100.0	.0	36.0	1.66	187.1
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	182.	.8	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	182.	.8	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	785.1	2270.3	1165.	8.	AG	6.	100.0	.0	12.0	2.30	59.2
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2393.	.8	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2393.	.8	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2393.	.8	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2393.	.8	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2393.	.8	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2393.	.8	.0	56.0		

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JOB: Site 5 Olymp & La Brea (S5B4PM.DAT) RUN: Site 5 Build 4 PM
DATE: 03/19/2010 TIME: 14:02:36.33

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	67	2.0	2244	1116	4.10	1	3
7.	WB Oly AP Q	100	56	2.0	1464	1101	4.10	1	3
14.	NB Brea T+R Q	100	68	2.0	2208	1423	4.10	1	3
17.	NB Brea LT Q	100	92	2.0	43	1490	4.10	1	3
24.	SB Brea T+R Q	100	61	2.0	2466	1413	4.10	1	3
27.	SB Brea LT Q	100	51	2.0	182	176	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

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JOB: Site 5 Olymp & La Brea (S5B4PM.DAT) RUN: Site 5 Build 4 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.1	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.2	.1	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.0	.1
160.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.1	.0	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
190.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
195.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.1	.0	.0	.1
200.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1
205.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1

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JOB: Site 5 Olymp & La Brea (S5B4PM.DAT) RUN: Site 5 Build 4 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
225.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1	.1
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.2	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.2	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX DEGR.	.1 130	.2 160	.2 225	.2 190	.1 0	.1 0	.1 0	.1 90	.1 225	.1 115	.2 255	.1 0	.1 0	.1 0	.2 0	.3 25	.2 50	.2 30	.2 240	.2 240

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JOB: Site 5 Olymp & La Brea (S5B4PM.DAT) RUN: Site 5 Build 4 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.0	.1	.2
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.0	.1	.1	.1
20.	.0	.2	.2	.1	.1	.1	.1	.1
25.	.0	.2	.2	.2	.1	.1	.1	.1
30.	.0	.2	.2	.2	.1	.1	.0	.1
35.	.0	.2	.2	.2	.1	.1	.0	.1
40.	.0	.2	.2	.2	.1	.1	.0	.1
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.2
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.1	.2
85.	.0	.2	.2	.0	.1	.1	.1	.2
90.	.0	.1	.1	.0	.0	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.2	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.1	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.1	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.1	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.1	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.0	.0	.0
290.	.0	.2	.2	.2	.2	.0	.0	.0
295.	.0	.2	.1	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.2	.0	.0	.1
335.	.0	.2	.1	.2	.1	.0	.0	.1
340.	.0	.2	.1	.1	.0	.0	.0	.1
345.	.0	.2	.2	.1	.0	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 110	.2 0	.2 0	.2 0	.2 280	.1 10	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 160 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 225 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B5AM.DAT) RUN: Site 5 Build 5 AM
DATE: 03/19/2010 TIME: 14:28:45.17

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1549.	.8	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1549.	.8	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-230.3	1054.0	775.	272.	AG	29.	100.0	.0	48.0	1.16	39.4
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1559.	.9	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1904.	.9	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1904.	.9	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	1061.4	1055.2	367.	91.	AG	24.	100.0	.0	48.0	1.03	18.6
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	2022.	.8	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	2042.	.8	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	2042.	.8	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	2042.	.8	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1944.	.8	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1944.	.8	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	1825.0	-1795.7	3004.	157.	AG	23.	100.0	.0	36.0	1.69	152.6
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	98.	.8	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	98.	.8	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	653.7	915.8	63.	156.	AG	10.	100.0	.0	12.0	.82	3.2
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	2105.	.8	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	2105.	.8	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	2105.	.8	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	2303.	.8	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	2153.	.8	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	2153.	.8	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	1065.7	4418.3	3332.	8.	AG	22.	100.0	.0	36.0	1.70	169.3
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	150.	.8	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	150.	.8	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	735.3	1934.9	826.	8.	AG	6.	100.0	.0	12.0	1.90	42.0
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	2112.	.8	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	2112.	.8	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	2112.	.8	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	2112.	.8	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	2112.	.8	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	2112.	.8	.0	56.0		

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JOB: Site 5 Olymp & La Brea (S5B5AM.DAT) RUN: Site 5 Build 5 AM
DATE: 03/19/2010 TIME: 14:28:45.17

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	66	2.0	1549	1111	4.10	1	3
7.	WB Oly AP Q	100	54	2.0	1904	1106	4.10	1	3
14.	NB Brea T+R Q	100	69	2.0	1944	1424	4.10	1	3
17.	NB Brea LT Q	100	88	2.0	98	1490	4.10	1	3
24.	SB Brea T+R Q	100	66	2.0	2153	1408	4.10	1	3
27.	SB Brea LT Q	100	54	2.0	150	190	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

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JOB: Site 5 Olymp & La Brea (S5B5AM.DAT) RUN: Site 5 Build 5 AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
5.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
10.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.0	.0
15.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.0
25.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.0
30.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0
35.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
40.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
45.	* .0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
50.	* .0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0	.0
55.	* .0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0	.0
60.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
65.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
70.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
75.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0
80.	* .0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
85.	* .0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0
90.	* .0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0	.1
95.	* .0	.0	.0	.0	.0	.1	.0	.1	.2	.1	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
100.	* .0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0	.0	.0	.1	.2	.2	.0	.1	.1
105.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
110.	* .0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
115.	* .0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
120.	* .0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
125.	* .0	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.1
130.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
135.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.2	.2	.0	.1	.2
140.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.2	.0	.0	.0	.1	.1	.2	.0	.1	.2
145.	* .1	.0	.0	.0	.0	.0	.0	.2	.1	.2	.1	.0	.0	.0	.1	.1	.2	.0	.1	.2
150.	* .1	.0	.1	.0	.0	.0	.0	.2	.1	.2	.0	.0	.0	.0	.1	.1	.2	.0	.1	.2
155.	* .1	.0	.1	.1	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0	.1	.1	.2	.0	.1	.2
160.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.2	.0	.1	.1
165.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1
170.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.1	.2
175.	* .1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
180.	* .1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
185.	* .1	.2	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
190.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.0	.0	.0	.2	.1	.0	.0	.2	.2
195.	* .0	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1
200.	* .0	.1	.1	.1	.0	.0	.0	.2	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1
205.	* .0	.1	.1	.1	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
215.	* .1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
220.	* .1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.1	.0	.0	.1	.1	.0	.0	.0	.2	.2
225.	* .1	.1	.1	.1	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
230.	* .0	.1	.1	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
235.	* .0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
240.	* .0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
245.	* .0	.0	.2	.0	.0	.0	.0	.2	.2	.2	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
250.	* .1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.0	.1	.0	.1	.1	.0	.0	.2	.2	.2
255.	* .1	.0	.2	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.1	.1	.0	.0	.2	.2	.2
260.	* .1	.0	.1	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.2	.2	.2
265.	* .1	.0	.1	.0	.0	.0	.0	.1	.2	.0	.1	.0	.0	.1	.1	.0	.0	.1	.1	.1
270.	* .1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.0	.1	.0	.1	.1	.0	.0	.1	.1	.1
275.	* .1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.1	.1
280.	* .1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	* .1	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
300.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
305.	* .0	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
310.	* .0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
315.	* .0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
320.	* .0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
325.	* .0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
330.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
335.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
340.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
345.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
355.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
360.	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.2	.1	.0	.0	.0	.0
MAX DEGR.	* .1 130	.2 175	.2 235	.1 60	.1 50	.1 45	.1 45	.2 105	.2 95	.2 100	.2 105	.1 0	.1 0	.1 0	.3 10	.2 30	.2 80	.2 35	.2 175	.2 130

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.1	.1	.1	.0	.0	.1	.1
5.	.0	.1	.1	.1	.0	.0	.1	.1
10.	.0	.1	.1	.1	.1	.0	.1	.1
15.	.0	.1	.1	.1	.0	.0	.1	.1
20.	.0	.1	.1	.1	.0	.1	.0	.1
25.	.0	.1	.1	.1	.0	.1	.0	.1
30.	.0	.1	.1	.1	.0	.1	.0	.1
35.	.0	.1	.1	.1	.0	.1	.0	.1
40.	.0	.1	.1	.1	.0	.0	.0	.1
45.	.0	.1	.1	.1	.0	.0	.0	.1
50.	.0	.1	.1	.1	.0	.0	.0	.1
55.	.0	.1	.1	.1	.0	.0	.0	.1
60.	.0	.1	.1	.1	.0	.1	.0	.1
65.	.0	.1	.1	.1	.0	.1	.0	.0
70.	.0	.1	.1	.1	.0	.1	.0	.1
75.	.0	.1	.1	.0	.0	.1	.0	.2
80.	.0	.1	.1	.0	.0	.0	.0	.2
85.	.0	.1	.1	.0	.0	.0	.0	.2
90.	.1	.1	.0	.0	.0	.0	.1	.2
95.	.1	.1	.0	.0	.0	.0	.1	.2
100.	.1	.0	.0	.0	.0	.0	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.1	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.0	.1	.2
130.	.2	.0	.0	.0	.0	.0	.1	.2
135.	.2	.0	.0	.0	.0	.0	.0	.1
140.	.2	.0	.0	.0	.0	.0	.0	.1
145.	.2	.0	.0	.0	.0	.0	.0	.1
150.	.2	.0	.0	.0	.0	.0	.0	.1
155.	.2	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.2	.0	.0	.0	.0	.0	.0	.0
175.	.2	.0	.0	.0	.0	.0	.0	.0
180.	.2	.0	.0	.0	.0	.0	.0	.0
185.	.2	.0	.0	.0	.0	.0	.0	.0
190.	.2	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.2	.0	.0	.0	.0	.0	.0	.0
215.	.2	.0	.0	.0	.0	.0	.0	.0
220.	.2	.0	.0	.0	.0	.0	.0	.0
225.	.2	.0	.0	.0	.0	.0	.0	.0
230.	.2	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.1	.0	.0	.0	.0	.0	.0	.0
265.	.1	.0	.0	.1	.0	.0	.0	.0
270.	.1	.1	.1	.1	.1	.0	.0	.0
275.	.1	.2	.1	.1	.1	.0	.0	.0
280.	.0	.2	.1	.1	.1	.0	.0	.0
285.	.0	.2	.1	.1	.1	.0	.0	.0
290.	.0	.2	.1	.1	.1	.0	.0	.0
295.	.0	.2	.1	.1	.1	.0	.0	.0
300.	.0	.2	.1	.1	.1	.0	.0	.0
305.	.0	.2	.1	.1	.1	.0	.0	.0
310.	.0	.1	.1	.1	.1	.0	.0	.0
315.	.0	.1	.1	.1	.1	.0	.0	.0
320.	.0	.1	.1	.1	.1	.0	.0	.0
325.	.0	.1	.1	.1	.1	.0	.0	.0
330.	.0	.1	.1	.1	.1	.0	.0	.0
335.	.0	.1	.1	.1	.0	.0	.0	.1
340.	.0	.1	.1	.1	.0	.0	.0	.1
345.	.0	.1	.1	.1	.0	.0	.0	.1
350.	.0	.1	.1	.1	.0	.0	.1	.1
355.	.0	.1	.1	.1	.0	.0	.1	.1
360.	.0	.1	.1	.1	.0	.0	.1	.1
MAX	.2	.2	.1	.1	.1	.1	.1	.2
DEGR.	115	275	0	0	10	20	0	75

THE HIGHEST CONCENTRATION IS .30 PPM AT 10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 175 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 235 DEGREES FROM REC3 .

JOB: Site 5 Olymp & La Brea (S5B5PM.DAT) RUN: Site 5 Build 5 PM
DATE: 03/19/2010 TIME: 14:29:03.35

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	*	354.0	1033.0	-378.0	1053.0	*	732.	272.	AG	2222.	.8	.0	56.0		
2.	EB Oly AP	*	353.0	1037.0	623.0	1030.0	*	270.	91.	AG	2222.	.8	.0	68.0		
3.	EB Oly AP Q	*	544.0	1032.0	-2092.4	1106.9	*	2637.	272.	AG	29.	100.0	.0	48.0	1.72	134.0
4.	EB Oly DP	*	624.0	1024.0	1617.0	1000.0	*	993.	91.	AG	2166.	.8	.0	56.0		
5.	WB Oly AP	*	891.0	1065.0	1622.0	1047.0	*	731.	91.	AG	1455.	.8	.0	56.0		
6.	WB Oly AP	*	890.0	1060.0	630.0	1066.0	*	260.	271.	AG	1455.	.8	.0	68.0		
7.	WB Oly AP Q	*	695.0	1064.0	820.5	1061.0	*	125.	91.	AG	25.	100.0	.0	48.0	.82	6.4
8.	WB Oly DP	*	628.0	1073.0	-378.0	1100.0	*	1006.	272.	AG	1515.	.8	.0	56.0		
9.	NB Brea AP	*	1230.0	261.0	1042.0	547.0	*	342.	327.	AG	2226.	.8	.0	56.0		
10.	NB Brea AP	*	1042.0	547.0	981.0	616.0	*	92.	319.	AG	2226.	.8	.0	56.0		
11.	NB Brea AP	*	981.0	616.0	795.0	761.0	*	236.	308.	AG	2226.	.8	.0	56.0		
12.	NB Brea T+R	*	795.0	760.0	706.0	856.0	*	131.	317.	AG	2196.	.8	.0	56.0		
13.	NB Brea T+R	*	706.0	856.0	653.0	980.0	*	135.	337.	AG	2196.	.8	.0	56.0		
14.	NB Brea T+R Q	*	657.0	972.0	2110.6	-2472.3	*	3738.	157.	AG	22.	100.0	.0	36.0	1.84	189.9
15.	NB Brea LT	*	777.0	742.0	686.0	845.0	*	137.	319.	AG	30.	.8	.0	32.0		
16.	NB Brea LT	*	686.0	845.0	625.0	981.0	*	149.	336.	AG	30.	.8	.0	32.0		
17.	NB Brea LT Q	*	628.0	973.0	636.1	955.1	*	20.	156.	AG	10.	100.0	.0	12.0	.68	1.0
18.	NB Brea DP	*	653.0	978.0	638.0	1130.0	*	153.	354.	AG	2530.	.8	.0	56.0		
19.	NB Brea DP	*	638.0	1130.0	658.0	1238.0	*	110.	10.	AG	2530.	.8	.0	56.0		
20.	NB Brea DP	*	658.0	1238.0	933.0	2002.0	*	812.	20.	AG	2530.	.8	.0	56.0		
21.	SB Brea AP	*	644.0	1336.0	884.0	2016.0	*	721.	19.	AG	2640.	.8	.0	56.0		
22.	SB Brea T+R	*	644.0	1337.0	606.0	1228.0	*	115.	199.	AG	2446.	.8	.0	56.0		
23.	SB Brea T+R	*	606.0	1228.0	588.0	1103.0	*	126.	188.	AG	2446.	.8	.0	56.0		
24.	SB Brea T+R Q	*	590.0	1120.0	1086.1	4559.7	*	3475.	8.	AG	20.	100.0	.0	36.0	1.61	176.5
25.	SB Brea LT	*	665.0	1326.0	629.0	1221.0	*	111.	199.	AG	194.	.8	.0	32.0		
26.	SB Brea LT	*	629.0	1221.0	612.0	1105.0	*	117.	188.	AG	194.	.8	.0	32.0		
27.	SB Brea LT Q	*	614.0	1118.0	804.0	2397.0	*	1293.	8.	AG	6.	100.0	.0	12.0	2.46	65.7
28.	SB Brea DP	*	588.0	1102.0	600.0	989.0	*	114.	174.	AG	2332.	.8	.0	56.0		
29.	SB Brea DP	*	600.0	989.0	650.0	854.0	*	144.	160.	AG	2332.	.8	.0	56.0		
30.	SB Brea DP	*	650.0	854.0	723.0	758.0	*	121.	143.	AG	2332.	.8	.0	56.0		
31.	SB Brea DP	*	723.0	758.0	938.0	583.0	*	277.	129.	AG	2332.	.8	.0	56.0		
32.	SB Brea DP	*	938.0	583.0	1029.0	479.0	*	138.	139.	AG	2332.	.8	.0	56.0		
33.	SB Brea DP	*	1029.0	479.0	1184.0	227.0	*	296.	148.	AG	2332.	.8	.0	56.0		

JOB: Site 5 Olymp & La Brea (S5B5PM.DAT) RUN: Site 5 Build 5 PM
DATE: 03/19/2010 TIME: 14:29:03.35

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	*	100	67	2.0	2222	1117	4.10	1	3
7.	WB Oly AP Q	*	100	56	2.0	1455	1101	4.10	1	3
14.	NB Brea T+R Q	*	100	68	2.0	2196	1423	4.10	1	3
17.	NB Brea LT Q	*	100	93	2.0	30	1490	4.10	1	3
24.	SB Brea T+R Q	*	100	60	2.0	2446	1410	4.10	1	3
27.	SB Brea LT Q	*	100	51	2.0	194	176	4.10	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	SE MID S	*	873.0	736.0	5.0	*
2.	SE 164 S	*	771.0	827.0	5.0	*
3.	SE 82 S	*	719.0	893.0	5.0	*
4.	SE CNR	*	695.0	985.0	5.0	*
5.	SE 82 E	*	784.0	990.0	5.0	*
6.	SE 164 E	*	866.0	989.0	5.0	*
7.	SE MID E	*	986.0	986.0	5.0	*
8.	NE MID E	*	977.0	1089.0	5.0	*
9.	NE 164 E	*	844.0	1094.0	5.0	*
10.	NE 82 E	*	762.0	1096.0	5.0	*
11.	NE CNR	*	680.0	1105.0	5.0	*
12.	NE 82 N	*	683.0	1199.0	5.0	*
13.	NE 164 N	*	707.0	1278.0	5.0	*
14.	NE MID N	*	748.0	1407.0	5.0	*
15.	NW MID N	*	646.0	1421.0	5.0	*
16.	NW 164 N	*	592.0	1268.0	5.0	*
17.	NW 82 N	*	569.0	1188.0	5.0	*
18.	NW CNR	*	550.0	1110.0	5.0	*
19.	NW 82 W	*	462.0	1106.0	5.0	*
20.	NW 164 W	*	380.0	1107.0	5.0	*
21.	NW MID W	*	226.0	1111.0	5.0	*
22.	SW MID W	*	220.0	1007.0	5.0	*
23.	SW 164 W	*	395.0	1000.0	5.0	*
24.	SW 82 W	*	478.0	998.0	5.0	*
25.	SW CNR	*	560.0	994.0	5.0	*
26.	SW 82 S	*	594.0	911.0	5.0	*
27.	SW 164 S	*	626.0	834.0	5.0	*
28.	SW MID S	*	709.0	731.0	5.0	*

JOB: Site 5 Olymp & La Brea (S5B5PM.DAT) RUN: Site 5 Build 5 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
5.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0	.0	.0
10.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
15.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0
20.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0
25.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.2	.3	.1	.1	.0	.0
30.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.0
35.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
40.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
45.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.2	.0
50.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.0
55.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
60.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
65.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
70.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
75.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
80.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
85.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
90.	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
95.	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
100.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
105.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
110.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
115.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
120.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
125.	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
130.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
135.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.0	.0
140.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.2	.2	.1	.0
145.	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.1	.0
150.	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0
155.	.1	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.2	.0	.1
160.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
165.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
170.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.1	.0	.1
175.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
180.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
185.	.1	.2	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
190.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.1
195.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.2	.0	.0	.0	.1
200.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1
205.	.1	.2	.1	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.1

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JOB: Site 5 Olymp & La Brea (S5B5PM.DAT) RUN: Site 5 Build 5 PM

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
215.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.0	.1	.1
220.	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
225.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
230.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.1	.1	.1
235.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1	.2
240.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
245.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
250.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.0	.2	.2	.2
255.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
260.	.1	.1	.2	.0	.0	.0	.0	.0	.1	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
265.	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2
270.	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.1	.2	.2
275.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
280.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
285.	.1	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
290.	.1	.2	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
295.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
300.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
305.	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
310.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
315.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
320.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
325.	.0	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
330.	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
335.	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
340.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
345.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
350.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0
355.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
360.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
MAX DEGR.	.1 130	.2 160	.2 225	.2 190	.1 0	.1 0	.1 0	.1 90	.1 230	.1 120	.2 255	.1 0	.1 0	.1 0	.2 10	.3 25	.2 55	.2 30	.2 240	.2 235

1

JOB: Site 5 Olymp & La Brea (S5B5PM.DAT) RUN: Site 5 Build 5 PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.2	.2	.1	.0	.1	.2
5.	.0	.2	.2	.2	.1	.0	.1	.1
10.	.0	.2	.2	.2	.1	.1	.1	.1
15.	.0	.2	.2	.2	.0	.1	.1	.1
20.	.0	.2	.2	.1	.0	.1	.1	.1
25.	.0	.2	.2	.1	.1	.1	.1	.1
30.	.0	.2	.2	.2	.1	.1	.0	.1
35.	.0	.2	.2	.2	.1	.1	.0	.1
40.	.0	.2	.2	.2	.1	.1	.0	.1
45.	.0	.2	.2	.2	.1	.1	.0	.0
50.	.0	.2	.2	.2	.1	.1	.0	.1
55.	.0	.2	.2	.2	.1	.1	.0	.1
60.	.0	.2	.2	.2	.0	.1	.0	.1
65.	.0	.2	.2	.2	.0	.1	.0	.1
70.	.0	.2	.2	.2	.0	.1	.0	.1
75.	.0	.2	.2	.1	.0	.1	.0	.1
80.	.0	.2	.2	.1	.1	.1	.0	.2
85.	.0	.2	.2	.0	.1	.1	.1	.2
90.	.0	.1	.1	.0	.0	.1	.1	.1
95.	.1	.1	.0	.0	.0	.1	.1	.2
100.	.1	.0	.0	.0	.0	.1	.1	.2
105.	.1	.0	.0	.0	.0	.1	.1	.2
110.	.2	.0	.0	.0	.0	.1	.1	.2
115.	.2	.0	.0	.0	.0	.1	.1	.2
120.	.2	.0	.0	.0	.0	.1	.1	.2
125.	.2	.0	.0	.0	.0	.1	.1	.2
130.	.1	.0	.0	.0	.1	.1	.1	.2
135.	.1	.0	.0	.0	.1	.0	.1	.1
140.	.1	.0	.0	.0	.1	.0	.0	.1
145.	.1	.0	.0	.0	.0	.0	.0	.1
150.	.1	.0	.0	.0	.0	.0	.0	.1
155.	.1	.0	.0	.0	.0	.0	.0	.1
160.	.1	.0	.0	.0	.0	.0	.0	.0
165.	.1	.0	.0	.0	.0	.0	.0	.0
170.	.1	.0	.0	.0	.0	.0	.0	.0
175.	.1	.0	.0	.0	.0	.0	.0	.0
180.	.1	.0	.0	.0	.0	.0	.0	.0
185.	.1	.0	.0	.0	.0	.0	.0	.0
190.	.1	.0	.0	.0	.0	.0	.0	.0
195.	.1	.0	.0	.0	.0	.0	.0	.0
200.	.1	.0	.0	.0	.0	.0	.0	.0
205.	.1	.0	.0	.0	.0	.0	.0	.0

1

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.1	.0	.0	.0	.0	.0	.0	.0
215.	.1	.0	.0	.0	.0	.0	.0	.0
220.	.1	.0	.0	.0	.0	.0	.0	.0
225.	.1	.0	.0	.0	.0	.0	.0	.0
230.	.1	.0	.0	.0	.0	.0	.0	.0
235.	.2	.0	.0	.0	.0	.0	.0	.0
240.	.2	.0	.0	.0	.0	.0	.0	.0
245.	.2	.0	.0	.0	.0	.0	.0	.0
250.	.2	.0	.0	.0	.0	.0	.0	.0
255.	.2	.0	.0	.0	.0	.0	.0	.0
260.	.2	.0	.0	.0	.0	.0	.0	.0
265.	.2	.2	.1	.1	.1	.0	.0	.0
270.	.2	.2	.1	.1	.1	.0	.0	.0
275.	.0	.2	.2	.1	.1	.0	.0	.0
280.	.0	.2	.2	.1	.2	.0	.0	.0
285.	.0	.2	.2	.2	.2	.0	.0	.0
290.	.0	.2	.2	.2	.2	.0	.0	.0
295.	.0	.2	.1	.2	.2	.0	.0	.0
300.	.0	.2	.1	.2	.2	.0	.0	.0
305.	.0	.2	.1	.2	.2	.0	.0	.0
310.	.0	.2	.1	.2	.2	.0	.0	.0
315.	.0	.2	.1	.2	.2	.0	.0	.0
320.	.0	.2	.1	.2	.2	.0	.0	.0
325.	.0	.2	.1	.2	.2	.0	.0	.0
330.	.0	.2	.1	.2	.2	.0	.0	.1
335.	.0	.2	.1	.2	.1	.0	.0	.1
340.	.0	.2	.1	.1	.0	.0	.0	.1
345.	.0	.2	.2	.1	.0	.0	.1	.1
350.	.0	.2	.2	.2	.1	.0	.1	.1
355.	.0	.2	.2	.2	.1	.0	.1	.1
360.	.0	.2	.2	.2	.1	.0	.1	.2
MAX DEGR.	.2 110	.2 0	.2 0	.2 0	.2 280	.1 10	.1 0	.2 0

THE HIGHEST CONCENTRATION IS .30 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS .20 PPM AT 160 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS .20 PPM AT 225 DEGREES FROM REC3 .

Site 5

Existing with Project

Input & Output Files

```
Site 5 Olymp & La Br (S5EXWPAM.DAT)     60.0321.0.0000.000280.30480000
1    1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Existing WITH PROJ AM            33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1172 3.3  0.  56
30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1172 3.3  0.  68
30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        66       2.0 1172   20.5 1110 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1211 3.9  0.  56
30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1538 3.9  0.  56
30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1538 3.9  0.  68
30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 1538   20.5 1105 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1671 3.3  0.  56
30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    1468 3.3  0.  56
30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    1468 3.3  0.  56
```

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30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    1468 3.3  0.  56
30.
  1
NB        Brea T+R  AG   795.   760.   706.   856.    1355 3.3  0.  56
30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1355 3.3  0.  56
30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.       0.  36   3
       100        68       2.0 1355   20.5 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     113 3.3  0.  32
30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     113 3.3  0.  32
30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.       0.  12   1
       100        87       2.0  113   20.5 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    1452 3.3  0.  56
30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    1452 3.3  0.  56
30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    1452 3.3  0.  56
30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    1745 3.3  0.  56
30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    1626 3.3  0.  56
30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    1626 3.3  0.  56
30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.       0.  36   3
       100        68       2.0 1626   20.5 1403 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     119 3.3  0.  32
30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     119 3.3  0.  32
30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.       0.  12   1
       100        57       2.0  119   20.5  199 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    1598 3.3  0.  56
30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    1598 3.3  0.  56
30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    1598 3.3  0.  56
```

```
30.
  1
SB         Brea DP   AG   723.   758.   938.   583.    1598 3.3  0.  56
30.
  1
SB         Brea DP   AG   938.   583.  1029.   479.    1598 3.3  0.  56
30.
  1
SB         Brea DP   AG  1029.   479.  1184.   227.    1598 3.3  0.  56
30.
1.0   04 1000.   0Y  5  0 72
```

JOB: Site 5 Olymp & La Br (S5EXWPAM.DAT) RUN: Site 5 Existing WITH PROJ AM
DATE: 07/13/2011 TIME: 13:59:43.42

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1172.	3.3	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1172.	3.3	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	409.1	1035.8	135.	272.	AG	145.	100.0	.0	48.0	.88	6.9
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1211.	3.9	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1538.	3.9	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1538.	3.9	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	822.8	1060.9	128.	91.	AG	119.	100.0	.0	48.0	.83	6.5
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	1671.	3.3	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	1468.	3.3	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	1468.	3.3	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	1468.	3.3	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1355.	3.3	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1355.	3.3	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	967.9	235.4	800.	157.	AG	112.	100.0	.0	36.0	1.13	40.6
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	113.	3.3	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	113.	3.3	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	657.6	907.0	72.	156.	AG	48.	100.0	.0	12.0	.84	3.7
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	1452.	3.3	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	1452.	3.3	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	1452.	3.3	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	1745.	3.3	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	1626.	3.3	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	1626.	3.3	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	848.6	2912.8	1811.	8.	AG	112.	100.0	.0	36.0	1.38	92.0
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	119.	3.3	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	119.	3.3	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	689.9	1629.4	517.	8.	AG	31.	100.0	.0	12.0	1.55	26.3
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	1598.	3.3	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	1598.	3.3	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	1598.	3.3	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	1598.	3.3	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	1598.	3.3	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	1598.	3.3	.0	56.0		

1

JOB: Site 5 Olymp & La Br (S5EXWPAM.DAT) RUN: Site 5 Existing WITH PROJ AM
DATE: 07/13/2011 TIME: 13:59:43.42

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	66	2.0	1172	1110	20.50	1	3
7.	WB Oly AP Q	100	54	2.0	1538	1105	20.50	1	3
14.	NB Brea T+R Q	100	68	2.0	1355	1423	20.50	1	3
17.	NB Brea LT Q	100	87	2.0	113	1490	20.50	1	3
24.	SB Brea T+R Q	100	68	2.0	1626	1403	20.50	1	3
27.	SB Brea LT Q	100	57	2.0	119	199	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

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JOB: Site 5 Olymp & La Br (S5EXWPAM.DAT) RUN: Site 5 Existing WITH PROJ AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.3	.4	.5	.6	.4	.3	.0	.1	.3	.5	.6	.5	.4	1.0	.4	.2	.2	.0	.0
5.	.0	.2	.4	.5	.6	.3	.3	.0	.0	.2	.4	.5	.4	.5	1.0	.7	.3	.2	.1	.0
10.	.0	.1	.4	.5	.4	.2	.2	.0	.0	.0	.3	.4	.4	.4	1.1	.8	.7	.4	.1	.1
15.	.0	.0	.3	.4	.4	.2	.2	.0	.0	.0	.3	.4	.4	.3	1.0	.9	.7	.6	.1	.1
20.	.0	.0	.3	.4	.4	.3	.2	.0	.0	.0	.1	.2	.3	.3	1.0	1.0	.9	.7	.2	.1
25.	.0	.0	.3	.4	.3	.2	.2	.0	.0	.0	.0	.1	.1	.2	.9	1.2	.9	.7	.3	.1
30.	.0	.0	.3	.4	.3	.2	.2	.0	.0	.0	.0	.1	.1	.1	.8	1.1	.9	.7	.3	.1
35.	.0	.0	.3	.4	.4	.3	.3	.0	.0	.0	.0	.0	.1	.1	.7	1.1	.9	.6	.4	.1
40.	.0	.0	.1	.4	.4	.3	.3	.0	.0	.0	.0	.0	.0	.1	.7	1.0	.7	.7	.3	.1
45.	.0	.0	.1	.5	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	1.0	.7	.6	.2	.1
50.	.0	.1	.1	.5	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	1.0	.7	.6	.1	.1
55.	.0	.2	.2	.4	.4	.3	.3	.0	.0	.0	.0	.0	.0	.0	.5	.8	.7	.5	.1	.1
60.	.0	.2	.2	.4	.4	.3	.3	.0	.0	.0	.0	.0	.0	.0	.5	.7	.5	.5	.2	.1
65.	.0	.0	.2	.4	.4	.3	.3	.1	.0	.0	.0	.0	.0	.0	.5	.7	.6	.4	.2	.1
70.	.0	.0	.2	.5	.3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.5	.7	.6	.4	.2	.2
75.	.0	.0	.2	.4	.3	.3	.3	.1	.1	.1	.0	.0	.0	.0	.5	.7	.6	.2	.3	.2
80.	.0	.0	.1	.3	.3	.3	.3	.2	.1	.2	.1	.0	.0	.0	.4	.7	.6	.2	.3	.2
85.	.0	.0	.0	.3	.3	.3	.3	.2	.2	.2	.3	.0	.0	.0	.4	.7	.6	.4	.2	.1
90.	.0	.0	.0	.3	.3	.3	.3	.3	.3	.4	.3	.0	.0	.0	.4	.7	.6	.6	.4	.2
95.	.0	.0	.0	.1	.2	.2	.2	.4	.4	.5	.4	.0	.0	.0	.4	.7	.6	.8	.5	.3
100.	.0	.0	.0	.1	.1	.1	.1	.4	.4	.5	.6	.1	.0	.0	.4	.7	.7	.7	.5	.4
105.	.0	.0	.0	.1	.1	.1	.1	.4	.4	.6	.6	.1	.0	.0	.4	.7	.7	.7	.6	.6
110.	.0	.0	.0	.0	.1	.1	.1	.4	.4	.6	.7	.1	.0	.0	.4	.7	.9	.6	.5	.5
115.	.1	.0	.0	.0	.0	.0	.0	.4	.3	.6	.6	.2	.1	.0	.4	.6	.9	.6	.6	.5
120.	.1	.0	.0	.0	.0	.0	.0	.4	.3	.6	.6	.1	.1	.0	.4	.7	.9	.6	.6	.6
125.	.1	.1	.0	.0	.0	.0	.0	.4	.3	.6	.6	.2	.1	.0	.5	.7	.9	.6	.5	.6
130.	.2	.2	.0	.0	.0	.0	.0	.3	.3	.6	.6	.3	.0	.0	.5	.7	.8	.6	.5	.6
135.	.2	.2	.3	.0	.0	.0	.0	.3	.4	.6	.6	.3	.0	.0	.5	.8	.9	.6	.6	.6
140.	.2	.2	.3	.0	.0	.0	.0	.3	.3	.6	.6	.3	.0	.0	.5	.9	.9	.5	.6	.6
145.	.2	.4	.5	.1	.0	.0	.0	.3	.3	.6	.5	.2	.0	.0	.5	1.2	.8	.6	.6	.6
150.	.2	.4	.4	.1	.0	.0	.0	.3	.3	.6	.6	.2	.0	.0	.5	1.2	.7	.6	.6	.6
155.	.3	.5	.6	.2	.0	.0	.0	.3	.3	.6	.6	.3	.1	.0	.5	.9	.8	.7	.7	.4
160.	.4	.5	.7	.4	.1	.0	.0	.3	.3	.7	.6	.3	.3	.0	.6	.9	.9	.6	.6	.4
165.	.4	.5	.8	.4	.1	.0	.0	.3	.3	.7	.6	.3	.3	.0	.8	.9	.7	.5	.6	.4
170.	.4	.5	.8	.4	.1	.1	.0	.3	.4	.7	.6	.3	.3	.1	.8	.8	.6	.6	.6	.4
175.	.4	.5	.8	.5	.1	.1	.0	.3	.4	.7	.7	.3	.3	.1	1.0	.8	.6	.5	.6	.3
180.	.4	.5	.8	.5	.1	.1	.0	.3	.4	.7	.6	.4	.3	.1	1.1	.7	.4	.4	.6	.3
185.	.5	.5	.8	.4	.1	.1	.1	.4	.4	.7	.5	.4	.1	.2	1.0	.6	.4	.4	.6	.3
190.	.5	.5	.7	.4	.1	.1	.1	.4	.4	.7	.5	.4	.1	.1	1.1	.6	.3	.5	.5	.3
195.	.4	.5	.7	.4	.1	.1	.1	.4	.5	.7	.6	.3	.1	.1	1.1	.6	.3	.5	.5	.3
200.	.4	.5	.7	.5	.1	.1	.1	.4	.5	.7	.6	.2	.2	.2	1.0	.5	.2	.5	.5	.2
205.	.4	.5	.7	.5	.1	.1	.1	.4	.5	.7	.4	.2	.2	.3	.8	.5	.2	.5	.5	.2

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WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	.4	.4	.6	.5	.1	.1	.1	.4	.6	.7	.4	.2	.3	.3	.8	.3	.2	.5	.5	.3
215.	.4	.3	.6	.5	.1	.1	.1	.4	.6	.7	.3	.3	.4	.3	.7	.3	.2	.5	.5	.3
220.	.4	.4	.5	.5	.1	.1	.1	.4	.6	.7	.3	.4	.5	.3	.6	.3	.2	.5	.4	.3
225.	.4	.4	.5	.4	.1	.1	.1	.4	.6	.6	.3	.5	.6	.4	.5	.1	.2	.5	.4	.3
230.	.3	.4	.5	.4	.2	.1	.1	.4	.7	.6	.6	.6	.6	.4	.5	.1	.2	.5	.4	.3
235.	.3	.4	.5	.4	.2	.1	.1	.4	.6	.7	.6	.6	.6	.4	.4	.1	.1	.5	.4	.3
240.	.3	.4	.4	.4	.2	.1	.1	.4	.6	.7	.6	.6	.4	.4	.4	.1	.1	.5	.2	.3
245.	.3	.4	.5	.4	.2	.1	.1	.4	.6	.8	.6	.5	.5	.4	.4	.1	.1	.4	.4	.4
250.	.4	.4	.6	.3	.1	.1	.1	.5	.6	.7	.6	.5	.5	.4	.4	.1	.1	.4	.4	.4
255.	.4	.4	.5	.4	.1	.2	.2	.5	.7	.7	.7	.5	.4	.4	.4	.0	.1	.4	.4	.4
260.	.4	.4	.5	.4	.2	.2	.1	.5	.7	.7	.7	.5	.3	.4	.4	.0	.1	.4	.4	.4
265.	.4	.4	.5	.5	.2	.1	.1	.5	.5	.6	.5	.5	.4	.3	.4	.0	.1	.2	.4	.4
270.	.4	.4	.5	.4	.3	.2	.2	.5	.5	.6	.4	.4	.4	.3	.4	.0	.0	.2	.3	.3
275.	.4	.4	.5	.4	.3	.3	.4	.3	.4	.3	.4	.4	.4	.3	.4	.0	.0	.2	.2	.2
280.	.4	.4	.7	.6	.4	.5	.5	.2	.3	.3	.4	.5	.4	.4	.4	.0	.0	.1	.2	.2
285.	.4	.4	.8	.6	.5	.5	.4	.1	.3	.3	.4	.5	.4	.4	.4	.0	.0	.1	.1	.1
290.	.3	.5	.9	.6	.5	.5	.4	.2	.2	.2	.3	.3	.4	.4	.4	.0	.0	.0	.1	.1
295.	.3	.6	.9	.6	.6	.4	.4	.1	.1	.1	.3	.4	.3	.4	.4	.0	.0	.0	.1	.1
300.	.3	.6	.9	.6	.6	.5	.4	.1	.1	.1	.4	.4	.4	.4	.4	.0	.0	.0	.0	.0
305.	.3	.7	.9	.4	.4	.6	.5	.1	.1	.1	.4	.4	.4	.3	.4	.0	.0	.0	.0	.0
310.	.3	.5	.9	.4	.5	.6	.5	.1	.1	.1	.5	.4	.4	.3	.4	.0	.0	.0	.0	.0
315.	.2	.4	.8	.5	.6	.6	.4	.1	.1	.1	.5	.4	.4	.3	.4	.0	.0	.0	.0	.0
320.	.2	.4	.5	.5	.6	.5	.4	.1	.1	.1	.4	.5	.4	.4	.4	.0	.0	.0	.0	.0
325.	.1	.4	.6	.4	.6	.5	.4	.1	.1	.1	.4	.5	.5	.4	.5	.0	.0	.0	.0	.0
330.	.1	.3	.5	.4	.5	.5	.4	.1	.1	.1	.3	.5	.5	.5	.5	.0	.0	.0	.0	.0
335.	.1	.2	.5	.4	.5	.4	.3	.1	.1	.1	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
340.	.1	.1	.5	.4	.5	.4	.3	.1	.1	.2	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
345.	.1	.2	.6	.5	.5	.3	.3	.1	.1	.2	.3	.6	.5	.5	.7	.1	.0	.0	.0	.0
350.	.1	.2	.6	.6	.5	.3	.3	.1	.1	.3	.4	.5	.5	.5	.7	.2	.1	.0	.0	.0
355.	.1	.3	.4	.5	.5	.4	.3	.0	.1	.3	.5	.5	.5	.5	.9	.3	.1	.1	.0	.0
360.	.0	.3	.4	.5	.6	.4	.3	.0	.1	.3	.5	.6	.5	.4	1.0	.4	.2	.2	.0	.0
MAX	.5	.7	.9	.6	.6	.6	.5	.5	.7	.8	.7	.6	.6	.5	1.1	1.2	.9	.8	.7	.6
DEGR.	185	305	290	280	0	305	280	250	230	245	110	0	225	5	10	25	30	95	155	105

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.2	.3	.7	.5	.4	.3	.6
5.	.0	.2	.3	.7	.6	.4	.4	.6
10.	.0	.2	.4	.7	.7	.5	.4	.6
15.	.0	.2	.5	.8	.7	.5	.5	.6
20.	.0	.3	.5	.8	.7	.4	.4	.6
25.	.1	.3	.5	.8	.5	.4	.4	.6
30.	.1	.3	.6	.8	.5	.6	.5	.6
35.	.1	.3	.6	.7	.6	.6	.5	.6
40.	.1	.3	.6	.7	.5	.6	.5	.5
45.	.1	.3	.7	.7	.5	.6	.5	.4
50.	.1	.3	.7	.7	.4	.7	.6	.5
55.	.1	.3	.7	.7	.6	.8	.6	.4
60.	.1	.3	.6	.6	.6	.8	.6	.4
65.	.1	.2	.6	.7	.6	.6	.5	.5
70.	.2	.3	.6	.7	.6	.7	.3	.4
75.	.2	.3	.6	.7	.6	.8	.3	.4
80.	.1	.4	.5	.7	.7	.6	.3	.6
85.	.2	.4	.5	.5	.7	.6	.4	.6
90.	.2	.2	.4	.3	.4	.4	.5	.5
95.	.3	.2	.3	.3	.4	.5	.5	.6
100.	.4	.2	.3	.3	.4	.5	.5	.6
105.	.4	.0	.1	.2	.4	.5	.5	.6
110.	.4	.1	.1	.2	.3	.5	.5	.6
115.	.4	.1	.1	.2	.3	.4	.6	.6
120.	.4	.1	.1	.2	.4	.4	.5	.5
125.	.4	.1	.1	.2	.4	.5	.5	.5
130.	.4	.1	.1	.1	.4	.4	.5	.5
135.	.4	.0	.1	.1	.3	.5	.4	.4
140.	.3	.0	.1	.1	.3	.4	.4	.4
145.	.3	.0	.1	.1	.3	.4	.3	.4
150.	.3	.0	.0	.1	.3	.4	.2	.2
155.	.3	.0	.0	.0	.2	.3	.2	.2
160.	.3	.0	.0	.0	.2	.2	.1	.1
165.	.3	.0	.0	.0	.1	.0	.0	.1
170.	.3	.0	.0	.0	.0	.0	.0	.1
175.	.3	.0	.0	.0	.0	.0	.0	.0
180.	.3	.0	.0	.0	.0	.0	.0	.0
185.	.3	.0	.0	.0	.0	.0	.0	.0
190.	.3	.0	.0	.0	.0	.0	.0	.0
195.	.3	.0	.0	.0	.0	.0	.0	.0
200.	.3	.0	.0	.0	.0	.0	.0	.0
205.	.3	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.3	.0	.0	.0	.0	.0	.0	.0
215.	.3	.0	.0	.0	.0	.0	.0	.0
220.	.3	.0	.0	.0	.0	.0	.0	.0
225.	.3	.0	.0	.0	.0	.0	.0	.0
230.	.3	.0	.0	.0	.0	.0	.0	.0
235.	.3	.0	.0	.0	.0	.0	.0	.0
240.	.3	.0	.0	.0	.0	.0	.0	.0
245.	.4	.0	.0	.0	.0	.0	.0	.0
250.	.4	.0	.0	.0	.0	.0	.0	.0
255.	.4	.1	.0	.0	.0	.0	.0	.0
260.	.4	.1	.1	.0	.1	.0	.0	.0
265.	.4	.1	.1	.2	.2	.0	.0	.0
270.	.3	.1	.2	.4	.3	.0	.0	.0
275.	.2	.3	.2	.4	.5	.0	.0	.0
280.	.2	.3	.3	.5	.6	.0	.0	.0
285.	.1	.3	.3	.5	.5	.1	.0	.0
290.	.1	.3	.3	.6	.6	.1	.0	.0
295.	.1	.3	.3	.5	.6	.2	.0	.0
300.	.0	.3	.3	.5	.6	.2	.0	.0
305.	.0	.3	.3	.6	.6	.2	.1	.0
310.	.0	.3	.3	.6	.6	.3	.2	.1
315.	.0	.2	.3	.6	.5	.3	.1	.1
320.	.0	.2	.2	.6	.5	.3	.1	.1
325.	.0	.2	.2	.6	.5	.3	.2	.1
330.	.0	.2	.2	.6	.5	.3	.2	.2
335.	.0	.2	.2	.6	.4	.4	.2	.4
340.	.0	.2	.2	.6	.4	.4	.2	.5
345.	.0	.2	.2	.6	.3	.6	.2	.5
350.	.0	.2	.2	.6	.4	.5	.3	.5
355.	.0	.2	.2	.6	.5	.4	.3	.5
360.	.0	.2	.3	.7	.5	.4	.3	.6
MAX	.4	.4	.7	.8	.7	.8	.6	.6
DEGR.	100	80	45	15	10	55	50	0

THE HIGHEST CONCENTRATION IS 1.20 PPM AT 25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS 1.10 PPM AT 10 DEGREES FROM REC15.
THE 3RD HIGHEST CONCENTRATION IS .90 PPM AT 290 DEGREES FROM REC3 .

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Site 5 Olymp & La Br (S5EXWPPM.DAT)     60.0321.0.0000.000280.30480000
1    1
SE MID S                   873.      736.       5.0
SE 164 S                   771.      827.       5.0
SE 82 S                    719.      893.       5.0
SE CNR                     695.      985.       5.0
SE 82 E                    784.      990.       5.0
SE 164 E                   866.      989.       5.0
SE MID E                   986.      986.       5.0
NE MID E                   977.     1089.       5.0
NE 164 E                   844.     1094.       5.0
NE 82 E                    762.     1096.       5.0
NE CNR                     680.     1105.       5.0
NE 82 N                    683.     1199.       5.0
NE 164 N                   707.     1278.       5.0
NE MID N                   748.     1407.       5.0
NW MID N                   646.     1421.       5.0
NW 164 N                   592.     1268.       5.0
NW 82 N                    569.     1188.       5.0
NW CNR                     550.     1110.       5.0
NW 82 W                    462.     1106.       5.0
NW 164 W                   380.     1107.       5.0
NW MID W                   226.     1111.       5.0
SW MID W                   220.     1007.       5.0
SW 164 W                   395.     1000.       5.0
SW 82 W                    478.      998.       5.0
SW CNR                     560.      994.       5.0
SW 82 S                    594.      911.       5.0
SW 164 S                   626.      834.       5.0
SW MID S                   709.      731.       5.0
Site 5 Existing WITH PROJ PM            33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1744 3.3  0.  56
30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1744 3.3  0.  68
30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
      100        65       2.0 1744   20.5 1162 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1726 3.3  0.  56
30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1117 3.3  0.  56
30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1117 3.3  0.  68
30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
      100        54       2.0 1117   20.5 1092 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1120 3.3  0.  56
30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    1510 3.3  0.  56
30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    1510 3.3  0.  56
```

```
30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    1510 3.3  0.  56
30.
  1
NB        Brea T+R  AG   795.   760.   706.   856.    1455 3.3  0.  56
30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1455 3.3  0.  56
30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.       0.  36   3
       100        69       2.0 1455   20.5 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      55 3.3  0.  32
30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      55 3.3  0.  32
30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.       0.  12   1
       100        90       2.0   55   20.5 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    1683 3.3  0.  56
30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    1683 3.3  0.  56
30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    1683 3.3  0.  56
30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    1899 3.3  0.  56
30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    1759 3.3  0.  56
30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    1759 3.3  0.  56
30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.       0.  36   3
       100        65       2.0 1759   20.5 1410 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     140 3.3  0.  32
30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     140 3.3  0.  32
30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.       0.  12   1
       100        53       2.0  140   20.5  181 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    1741 3.3  0.  56
30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    1741 3.3  0.  56
30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    1741 3.3  0.  56
```

```
30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    1741 3.3  0.  56
30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    1741 3.3  0.  56
30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    1741 3.3  0.  56
30.
1.0   04 1000.   0Y  5  0 72
```

JOB: Site 5 Olymp & La Br (S5EXWPPM.DAT) RUN: Site 5 Existing WITH PROJ PM
DATE: 07/13/2011 TIME: 14:47:46.19

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

	LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	EB Oly AP	354.0	1033.0	-378.0	1053.0	732.	272.	AG	1744.	3.3	.0	56.0		
2.	EB Oly AP	353.0	1037.0	623.0	1030.0	270.	91.	AG	1744.	3.3	.0	68.0		
3.	EB Oly AP Q	544.0	1032.0	-470.7	1060.8	1015.	272.	AG	143.	100.0	.0	48.0	1.21	51.6
4.	EB Oly DP	624.0	1024.0	1617.0	1000.0	993.	91.	AG	1726.	3.3	.0	56.0		
5.	WB Oly AP	891.0	1065.0	1622.0	1047.0	731.	91.	AG	1117.	3.3	.0	56.0		
6.	WB Oly AP	890.0	1060.0	630.0	1066.0	260.	271.	AG	1117.	3.3	.0	68.0		
7.	WB Oly AP Q	695.0	1064.0	777.4	1062.0	82.	91.	AG	119.	100.0	.0	48.0	.61	4.2
8.	WB Oly DP	628.0	1073.0	-378.0	1100.0	1006.	272.	AG	1120.	3.3	.0	56.0		
9.	NB Brea AP	1230.0	261.0	1042.0	547.0	342.	327.	AG	1510.	3.3	.0	56.0		
10.	NB Brea AP	1042.0	547.0	981.0	616.0	92.	319.	AG	1510.	3.3	.0	56.0		
11.	NB Brea AP	981.0	616.0	795.0	761.0	236.	308.	AG	1510.	3.3	.0	56.0		
12.	NB Brea T+R	795.0	760.0	706.0	856.0	131.	317.	AG	1455.	3.3	.0	56.0		
13.	NB Brea T+R	706.0	856.0	653.0	980.0	135.	337.	AG	1455.	3.3	.0	56.0		
14.	NB Brea T+R Q	657.0	972.0	1161.6	-223.6	1298.	157.	AG	114.	100.0	.0	36.0	1.26	65.9
15.	NB Brea LT	777.0	742.0	686.0	845.0	137.	319.	AG	55.	3.3	.0	32.0		
16.	NB Brea LT	686.0	845.0	625.0	981.0	149.	336.	AG	55.	3.3	.0	32.0		
17.	NB Brea LT Q	628.0	973.0	640.1	946.0	30.	156.	AG	49.	100.0	.0	12.0	.62	1.5
18.	NB Brea DP	653.0	978.0	638.0	1130.0	153.	354.	AG	1683.	3.3	.0	56.0		
19.	NB Brea DP	638.0	1130.0	658.0	1238.0	110.	10.	AG	1683.	3.3	.0	56.0		
20.	NB Brea DP	658.0	1238.0	933.0	2002.0	812.	20.	AG	1683.	3.3	.0	56.0		
21.	SB Brea AP	644.0	1336.0	884.0	2016.0	721.	19.	AG	1899.	3.3	.0	56.0		
22.	SB Brea T+R	644.0	1337.0	606.0	1228.0	115.	199.	AG	1759.	3.3	.0	56.0		
23.	SB Brea T+R	606.0	1228.0	588.0	1103.0	126.	188.	AG	1759.	3.3	.0	56.0		
24.	SB Brea T+R Q	590.0	1120.0	848.6	2912.9	1811.	8.	AG	107.	100.0	.0	36.0	1.34	92.0
25.	SB Brea LT	665.0	1326.0	629.0	1221.0	111.	199.	AG	140.	3.3	.0	32.0		
26.	SB Brea LT	629.0	1221.0	612.0	1105.0	117.	188.	AG	140.	3.3	.0	32.0		
27.	SB Brea LT Q	614.0	1118.0	722.5	1848.9	739.	8.	AG	29.	100.0	.0	12.0	1.82	37.5
28.	SB Brea DP	588.0	1102.0	600.0	989.0	114.	174.	AG	1741.	3.3	.0	56.0		
29.	SB Brea DP	600.0	989.0	650.0	854.0	144.	160.	AG	1741.	3.3	.0	56.0		
30.	SB Brea DP	650.0	854.0	723.0	758.0	121.	143.	AG	1741.	3.3	.0	56.0		
31.	SB Brea DP	723.0	758.0	938.0	583.0	277.	129.	AG	1741.	3.3	.0	56.0		
32.	SB Brea DP	938.0	583.0	1029.0	479.0	138.	139.	AG	1741.	3.3	.0	56.0		
33.	SB Brea DP	1029.0	479.0	1184.0	227.0	296.	148.	AG	1741.	3.3	.0	56.0		

JOB: Site 5 Olymp & La Br (S5EXWPPM.DAT) RUN: Site 5 Existing WITH PROJ PM
DATE: 07/13/2011 TIME: 14:47:46.19

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
3.	EB Oly AP Q	100	65	2.0	1744	1162	20.50	1	3
7.	WB Oly AP Q	100	54	2.0	1117	1092	20.50	1	3
14.	NB Brea T+R Q	100	69	2.0	1455	1423	20.50	1	3
17.	NB Brea LT Q	100	90	2.0	55	1490	20.50	1	3
24.	SB Brea T+R Q	100	65	2.0	1759	1410	20.50	1	3
27.	SB Brea LT Q	100	53	2.0	140	181	20.50	1	3

RECEPTOR LOCATIONS

	RECEPTOR	COORDINATES (FT) X	Y	Z
1.	SE MID S	873.0	736.0	5.0
2.	SE 164 S	771.0	827.0	5.0
3.	SE 82 S	719.0	893.0	5.0
4.	SE CNR	695.0	985.0	5.0
5.	SE 82 E	784.0	990.0	5.0
6.	SE 164 E	866.0	989.0	5.0
7.	SE MID E	986.0	986.0	5.0
8.	NE MID E	977.0	1089.0	5.0
9.	NE 164 E	844.0	1094.0	5.0
10.	NE 82 E	762.0	1096.0	5.0
11.	NE CNR	680.0	1105.0	5.0
12.	NE 82 N	683.0	1199.0	5.0
13.	NE 164 N	707.0	1278.0	5.0
14.	NE MID N	748.0	1407.0	5.0
15.	NW MID N	646.0	1421.0	5.0
16.	NW 164 N	592.0	1268.0	5.0
17.	NW 82 N	569.0	1188.0	5.0
18.	NW CNR	550.0	1110.0	5.0
19.	NW 82 W	462.0	1106.0	5.0
20.	NW 164 W	380.0	1107.0	5.0
21.	NW MID W	226.0	1111.0	5.0
22.	SW MID W	220.0	1007.0	5.0
23.	SW 164 W	395.0	1000.0	5.0
24.	SW 82 W	478.0	998.0	5.0
25.	SW CNR	560.0	994.0	5.0
26.	SW 82 S	594.0	911.0	5.0
27.	SW 164 S	626.0	834.0	5.0
28.	SW MID S	709.0	731.0	5.0

JOB: Site 5 Olymp & La Br (S5EXWPPM.DAT) RUN: Site 5 Existing WITH PROJ PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .0	.2	.3	.7	.6	.4	.3	.0	.1	.3	.5	.6	.6	.5	1.0	.5	.2	.2	.0	.0
5.	* .0	.2	.3	.7	.5	.3	.3	.0	.0	.2	.4	.6	.5	.5	1.0	.7	.4	.3	.1	.0
10.	* .0	.1	.3	.6	.3	.3	.3	.0	.0	.1	.3	.4	.5	.5	1.0	.8	.7	.5	.1	.1
15.	* .0	.1	.2	.5	.3	.2	.3	.0	.0	.0	.3	.4	.4	.4	.9	.9	.8	.6	.1	.1
20.	* .0	.1	.2	.5	.3	.2	.3	.0	.0	.0	.1	.3	.3	.3	1.0	1.2	.9	.8	.1	.1
25.	* .0	.1	.1	.5	.3	.2	.3	.0	.0	.0	.1	.1	.2	.2	.9	1.2	.9	.8	.3	.1
30.	* .0	.1	.1	.5	.3	.2	.3	.0	.0	.0	.0	.1	.1	.1	.8	1.2	.8	.7	.4	.1
35.	* .0	.1	.1	.5	.3	.3	.3	.0	.0	.0	.0	.0	.1	.1	.7	1.0	.8	.6	.4	.2
40.	* .0	.1	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.1	.7	1.0	.8	.7	.2	.1
45.	* .0	.1	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	1.0	.7	.7	.2	.1
50.	* .0	.1	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	1.0	.7	.6	.1	.1
55.	* .0	.1	.1	.4	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.6	.7	.7	.5	.2	.1
60.	* .0	.1	.1	.4	.2	.3	.3	.0	.0	.0	.0	.0	.0	.0	.5	.7	.7	.5	.2	.1
65.	* .0	.1	.1	.3	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.5	.2	.1
70.	* .0	.1	.1	.2	.4	.4	.4	.0	.0	.0	.0	.0	.0	.0	.5	.7	.6	.4	.2	.1
75.	* .0	.0	.1	.2	.4	.4	.4	.1	.0	.0	.0	.0	.0	.0	.4	.7	.6	.3	.2	.2
80.	* .0	.0	.1	.2	.4	.4	.4	.1	.1	.0	.0	.0	.0	.0	.4	.7	.6	.3	.3	.2
85.	* .0	.0	.1	.2	.4	.4	.4	.1	.1	.2	.1	.0	.0	.0	.4	.7	.6	.3	.2	.1
90.	* .0	.0	.0	.2	.2	.3	.2	.3	.3	.3	.3	.0	.0	.0	.4	.7	.6	.4	.2	.2
95.	* .0	.0	.0	.1	.2	.2	.2	.3	.3	.3	.3	.0	.0	.0	.4	.7	.6	.7	.2	.2
100.	* .0	.0	.0	.1	.1	.2	.2	.3	.3	.3	.3	.0	.0	.0	.4	.7	.6	.7	.3	.5
105.	* .0	.0	.0	.1	.1	.1	.1	.3	.3	.3	.4	.0	.0	.0	.4	.7	.7	.7	.3	.5
110.	* .1	.0	.0	.0	.1	.1	.1	.3	.3	.3	.4	.1	.0	.0	.4	.7	.7	.7	.5	.5
115.	* .1	.0	.0	.0	.0	.0	.0	.3	.3	.2	.4	.1	.0	.0	.4	.8	.7	.6	.6	.5
120.	* .1	.0	.0	.0	.0	.0	.0	.3	.3	.3	.4	.1	.0	.0	.4	.8	.8	.4	.5	.6
125.	* .1	.1	.0	.0	.0	.0	.0	.3	.3	.3	.5	.1	.0	.0	.5	.8	.8	.4	.4	.6
130.	* .2	.2	.0	.0	.0	.0	.0	.3	.2	.3	.5	.1	.0	.0	.5	.8	.9	.6	.4	.6
135.	* .2	.2	.3	.0	.0	.0	.0	.2	.2	.3	.5	.1	.0	.0	.5	.8	.8	.7	.5	.6
140.	* .2	.3	.3	.1	.0	.0	.0	.2	.2	.3	.4	.2	.0	.0	.5	.8	.8	.6	.5	.6
145.	* .2	.4	.5	.1	.0	.0	.0	.2	.2	.3	.4	.2	.0	.0	.5	.8	.8	.6	.5	.6
150.	* .2	.4	.5	.2	.0	.0	.0	.2	.2	.4	.5	.2	.0	.0	.5	1.0	.7	.7	.5	.6
155.	* .4	.5	.7	.2	.1	.0	.0	.2	.2	.5	.5	.3	.0	.0	.5	.9	.9	.6	.5	.5
160.	* .4	.5	.8	.4	.1	.0	.0	.2	.2	.5	.6	.3	.1	.0	.7	1.0	.8	.6	.6	.5
165.	* .4	.6	.8	.4	.1	.1	.0	.2	.3	.5	.5	.3	.1	.1	.7	1.0	.7	.5	.5	.5
170.	* .5	.6	.8	.5	.1	.1	.0	.2	.3	.6	.5	.3	.2	.1	.9	.9	.6	.4	.5	.5
175.	* .5	.6	.9	.5	.2	.1	.1	.3	.3	.6	.6	.3	.2	.1	1.0	.8	.5	.4	.5	.5
180.	* .5	.6	.8	.6	.2	.1	.1	.3	.3	.6	.5	.4	.1	.2	1.1	.7	.4	.3	.5	.5
185.	* .5	.6	.8	.5	.2	.1	.1	.3	.3	.6	.4	.3	.1	.2	1.0	.6	.6	.3	.5	.5
190.	* .5	.6	.7	.4	.2	.1	.1	.3	.3	.6	.4	.3	.1	.2	1.1	.6	.4	.4	.5	.5
195.	* .5	.5	.7	.4	.1	.1	.1	.3	.3	.6	.5	.2	.1	.1	1.1	.6	.4	.4	.5	.5
200.	* .4	.5	.7	.5	.1	.1	.1	.3	.3	.6	.6	.2	.2	.2	1.0	.5	.3	.4	.5	.6
205.	* .5	.5	.7	.5	.1	.1	.1	.3	.3	.6	.5	.2	.2	.3	1.0	.4	.3	.4	.5	.5

1

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	* .4	.5	.6	.5	.1	.1	.1	.3	.3	.6	.4	.3	.3	.3	.8	.3	.3	.4	.5	.5
215.	* .4	.4	.6	.5	.1	.1	.1	.3	.3	.6	.5	.5	.5	.4	.8	.2	.3	.4	.5	.5
220.	* .4	.5	.5	.5	.1	.1	.1	.3	.3	.6	.5	.6	.5	.5	.8	.2	.4	.4	.5	.5
225.	* .4	.5	.5	.5	.2	.1	.1	.3	.4	.5	.5	.6	.5	.5	.6	.1	.4	.5	.5	.5
230.	* .4	.5	.5	.4	.2	.1	.1	.3	.4	.6	.6	.6	.5	.6	.6	.1	.3	.5	.5	.5
235.	* .3	.5	.6	.4	.2	.1	.1	.3	.3	.6	.7	.7	.5	.5	.5	.1	.3	.5	.6	.6
240.	* .3	.4	.7	.4	.2	.1	.1	.2	.3	.7	.7	.7	.4	.5	.5	.1	.3	.5	.7	.6
245.	* .4	.4	.6	.4	.3	.1	.1	.2	.4	.8	.7	.7	.5	.5	.5	.1	.4	.5	.7	.6
250.	* .4	.4	.6	.3	.3	.1	.2	.3	.4	.6	.7	.7	.5	.5	.5	.1	.4	.7	.6	.6
255.	* .4	.4	.6	.5	.3	.2	.2	.4	.5	.8	.6	.8	.5	.5	.4	.1	.4	.7	.6	.6
260.	* .4	.4	.6	.5	.3	.3	.2	.4	.3	.8	.8	.6	.5	.4	.4	.1	.2	.6	.6	.6
265.	* .4	.5	.5	.7	.3	.2	.3	.4	.5	.7	.8	.6	.5	.4	.4	.1	.1	.5	.6	.6
270.	* .4	.5	.7	.6	.4	.3	.3	.3	.4	.6	.5	.6	.4	.4	.4	.0	.1	.4	.5	.5
275.	* .4	.6	.7	.9	.7	.3	.3	.3	.3	.5	.5	.5	.4	.4	.4	.0	.0	.2	.3	.2
280.	* .5	.6	.8	.8	.7	.3	.4	.2	.3	.4	.5	.5	.4	.4	.4	.0	.0	.2	.2	.2
285.	* .5	.6	.9	.7	.6	.4	.5	.0	.2	.1	.3	.5	.4	.4	.4	.0	.0	.0	.1	.1
290.	* .5	.6	.9	.7	.6	.6	.4	.0	.1	.1	.3	.5	.4	.4	.4	.0	.0	.0	.1	.1
295.	* .5	.7	1.0	.6	.5	.4	.4	.1	.1	.1	.4	.5	.4	.4	.4	.0	.0	.0	.0	.0
300.	* .4	.7	.9	.6	.5	.4	.2	.1	.1	.2	.4	.5	.4	.4	.4	.0	.0	.0	.0	.0
305.	* .4	.7	.9	.7	.5	.5	.2	.1	.1	.2	.4	.4	.4	.4	.4	.0	.0	.0	.0	.0
310.	* .4	.6	.9	.7	.5	.5	.3	.1	.1	.2	.4	.4	.5	.4	.4	.0	.0	.0	.0	.0
315.	* .3	.5	.8	.5	.5	.5	.3	.1	.1	.2	.5	.4	.5	.4	.4	.0	.0	.0	.0	.0
320.	* .2	.4	.6	.5	.6	.5	.4	.1	.1	.1	.5	.5	.5	.4	.4	.0	.0	.0	.0	.0
325.	* .1	.4	.6	.5	.6	.4	.4	.1	.1	.1	.4	.5	.5	.4	.5	.0	.0	.0	.0	.0
330.	* .0	.3	.6	.6	.6	.4	.4	.1	.1	.1	.4	.5	.5	.4	.5	.0	.0	.0	.0	.0
335.	* .1	.2	.6	.5	.6	.4	.4	.1	.2	.2	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
340.	* .1	.1	.5	.5	.6	.4	.4	.1	.2	.2	.3	.5	.5	.5	.6	.1	.0	.0	.0	.0
345.	* .1	.2	.5	.5	.5	.4	.4	.1	.2	.3	.3	.6	.5	.5	.6	.1	.0	.0	.0	.0
350.	* .1	.2	.5	.7	.6	.4	.4	.1	.2	.3	.4	.6	.5	.5	.7	.2	.1	.0	.0	.0
355.	* .1	.2	.4	.7	.6	.4	.3	.0	.1	.3	.5	.6	.5	.6	.9	.3	.1	.1	.0	.0
360.	* .0	.2	.3	.7	.6	.4	.3	.0	.1	.3	.5	.6	.6	.5	1.0	.5	.2	.2	.0	.0
MAX	* .5	.7	1.0	.9	.7	.6	.5	.4	.5	.8	.8	.8	.6	.6	1.1	1.2	.9	.8	.7	.6
DEGR.	* 170	295	295	275	275	290	285	255	255	245	260	255	0	230	180	20	130	20	240	120

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MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
0.	.0	.7	.7	.8	.6	.5	.3	.7
5.	.0	.7	.7	.8	.7	.6	.5	.7
10.	.0	.7	.8	.8	.7	.6	.6	.6
15.	.0	.7	.8	.9	.9	.6	.5	.6
20.	.0	.8	.8	.9	1.0	.4	.4	.6
25.	.1	.8	.8	1.1	.7	.4	.5	.6
30.	.1	.8	.8	.9	.8	.4	.5	.6
35.	.1	.8	.8	.9	.6	.5	.5	.6
40.	.1	.8	.8	.8	.5	.6	.6	.6
45.	.1	.9	.8	.8	.5	.6	.6	.5
50.	.1	.9	.8	.8	.4	.6	.6	.6
55.	.1	.9	.9	.8	.6	.5	.6	.6
60.	.1	.9	.8	.6	.6	.5	.6	.6
65.	.1	.8	.7	.6	.6	.5	.5	.5
70.	.1	.9	.7	.8	.6	.6	.5	.4
75.	.2	.9	.7	.7	.7	.6	.4	.5
80.	.1	.9	.6	.6	.6	.6	.5	.6
85.	.1	.7	.6	.5	.5	.6	.5	.6
90.	.2	.7	.5	.3	.6	.5	.5	.6
95.	.4	.5	.3	.3	.6	.5	.5	.6
100.	.5	.3	.4	.3	.4	.5	.5	.6
105.	.5	.2	.3	.3	.4	.5	.5	.6
110.	.5	.2	.1	.2	.3	.5	.5	.7
115.	.8	.1	.1	.2	.3	.5	.6	.7
120.	.8	.1	.1	.2	.4	.5	.5	.5
125.	.7	.1	.1	.2	.4	.5	.5	.5
130.	.6	.1	.1	.1	.5	.6	.5	.5
135.	.6	.1	.1	.1	.5	.6	.5	.4
140.	.6	.0	.1	.1	.4	.5	.4	.4
145.	.5	.0	.1	.1	.3	.4	.4	.4
150.	.5	.0	.1	.1	.3	.4	.3	.3
155.	.5	.0	.0	.1	.3	.3	.2	.2
160.	.5	.0	.0	.0	.2	.2	.1	.2
165.	.5	.0	.0	.0	.2	.2	.1	.1
170.	.5	.0	.0	.0	.0	.0	.0	.1
175.	.5	.0	.0	.0	.0	.0	.0	.0
180.	.5	.0	.0	.0	.0	.0	.0	.0
185.	.5	.0	.0	.0	.0	.0	.0	.0
190.	.5	.0	.0	.0	.0	.0	.0	.0
195.	.5	.0	.0	.0	.0	.0	.0	.0
200.	.5	.0	.0	.0	.0	.0	.0	.0
205.	.5	.0	.0	.0	.0	.0	.0	.0

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WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28
210.	.5	.0	.0	.0	.0	.0	.0	.0
215.	.5	.0	.0	.0	.0	.0	.0	.0
220.	.5	.0	.0	.0	.0	.0	.0	.0
225.	.5	.0	.0	.0	.0	.0	.0	.0
230.	.5	.0	.0	.0	.0	.0	.0	.0
235.	.6	.0	.0	.0	.0	.0	.0	.0
240.	.6	.0	.0	.0	.0	.0	.0	.0
245.	.6	.0	.0	.0	.0	.0	.0	.0
250.	.6	.2	.1	.1	.0	.0	.0	.0
255.	.6	.2	.1	.1	.1	.0	.0	.0
260.	.6	.3	.3	.4	.3	.0	.0	.0
265.	.5	.5	.4	.5	.5	.0	.0	.0
270.	.5	.6	.7	.6	.6	.1	.0	.0
275.	.2	.8	.8	.8	.9	.1	.1	.0
280.	.2	1.0	.9	1.0	.9	.3	.1	.0
285.	.1	1.0	1.0	1.0	.9	.3	.1	.1
290.	.1	1.0	1.0	1.0	.8	.3	.1	.1
295.	.0	1.0	1.0	1.0	.8	.2	.1	.1
300.	.0	.8	.8	.8	.8	.3	.1	.1
305.	.0	.8	.8	.8	.7	.3	.1	.1
310.	.0	.8	.8	.8	.7	.3	.1	.2
315.	.0	.8	.8	.8	.6	.3	.1	.2
320.	.0	.8	.7	.7	.6	.3	.2	.2
325.	.0	.7	.6	.7	.6	.2	.3	.2
330.	.0	.7	.6	.7	.5	.2	.3	.5
335.	.0	.7	.7	.7	.5	.3	.3	.4
340.	.0	.7	.7	.7	.5	.3	.3	.4
345.	.0	.7	.7	.7	.4	.5	.3	.5
350.	.0	.7	.7	.7	.5	.4	.3	.5
355.	.0	.7	.7	.7	.6	.4	.3	.5
360.	.0	.7	.7	.8	.6	.5	.3	.7
MAX DEGR.	.8 115	1.0 280	1.0 285	1.1 25	1.0 20	.6 5	.6 10	.7 110

THE HIGHEST CONCENTRATION IS 1.20 PPM AT 20 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS 1.10 PPM AT 25 DEGREES FROM REC24.
THE 3RD HIGHEST CONCENTRATION IS 1.10 PPM AT 180 DEGREES FROM REC15.